

Reconciling Fugitive Dust Emissions with Ambient Measurements: Along the Unpaved Road

V. Etyemezian*, J. Gillies, H. Kuhns, D. Nikolic

Division of Atmospheric Sciences
Desert Research Institute
Las Vegas, NV

and

G. Seshadri, J. Veranth

University of Utah
SLC, UT

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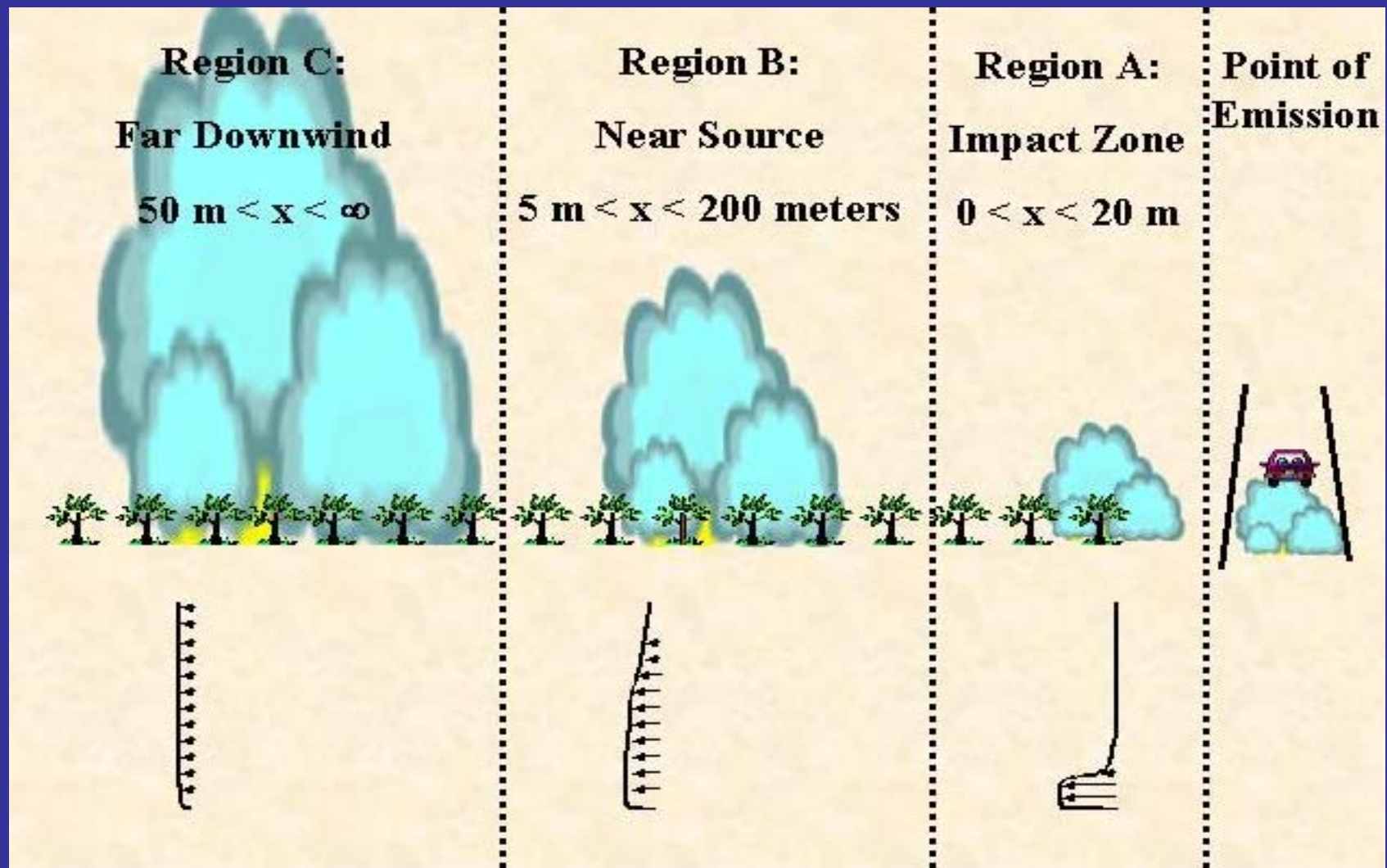
Outline

- Background
 - What is the phenomenon being examined?
 - Why is it important?
- Modeling approaches
 - Gaussian plume model (ISC style)
 - Box Model (Gillette style)
 - Deposition velocity
- Model results
 - What do initial results tell us?
 - How does this compare with measurements?
 - Where do we need improvements?
- Conclusions and Future Work

Relevance to Fug Dust Emissions

- Not accounting for near-field deposition \Rightarrow
 - Overestimate fug dust regional contribution (e.g. Chow and Watson, 2000; Countess, 2001)
 - Erroneous estimate of size distribution of regionally transportable fraction (important for visibility)
 - Cannot resolve PM_{10} contributions from varying fug dust sources
 - Is it the nearby unpaved road, the farm 5 km upwind, or China?
- Over-accounting for deposition \Rightarrow
 - Similar problems

Downwind of Dust Source



Downwind Regimes

Removal of PM_{10} dust by vegetation/land cover

- Region “A”:
 - Plume height \sim vegetation height
 - Work in progress
- Region “B”:
 - Mixed height $>$ Plume height $>$ vegetation height
 - Addressed in this study
- Region “C”:
 - $PM_{10} \sim$ constant with height
 - Addressed in regional scale models

Gaussian Plume Approach

- **Use Gaussian plume model to simulate dispersion**
- **Assumptions:**
 - **Gaussian profile is reasonable**
 - **Deposition is “slow” compared to dispersion. I.e. can distribute removal over entire plume**
 - **Can use bulk deposition models even though concentration gradients high very near the source**

Gaussian Approach Cont.

- Basic equation similar to ISC3:

$$C = (1 \times 10^{-6}) \frac{QVD}{2\pi u_s \sigma_y \sigma_z} \exp \left[-0.5 \left(\frac{y}{\sigma_y} \right)^2 \right]$$

Q = pollutant emission rate (g/s)

V = a vertical term that includes reflection, deposition, and mixing

D = chemical decay term (equal to 1 since dust non-reactive)

σ_y, σ_z = standard deviation of vertical and lateral concentration

u_s = mean wind speed at release height.

Gaussian Approach Cont.

Assume line source \Rightarrow Integrate crosswind:

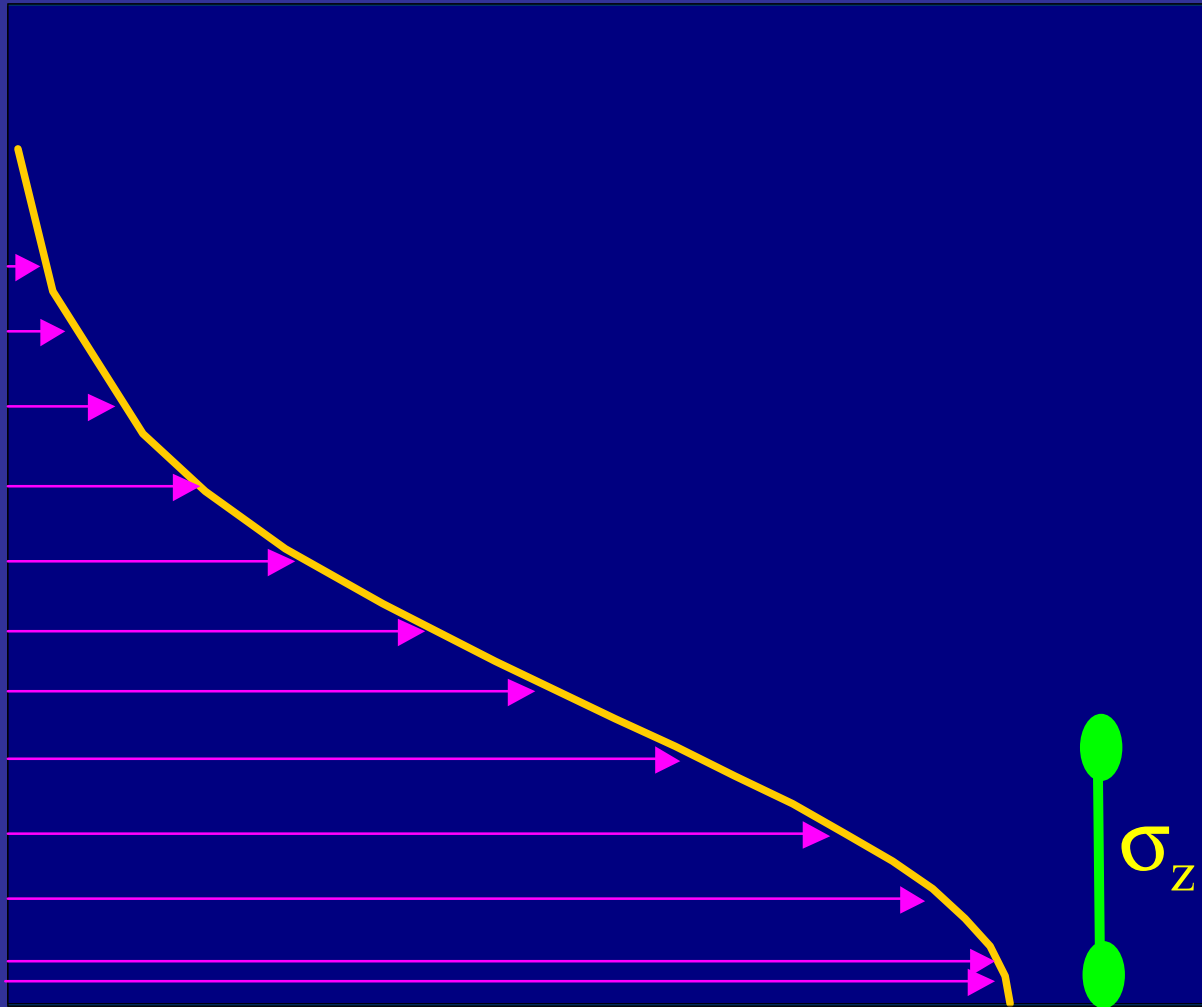
$$C = (1 \times 10^{-6}) \frac{\dot{Q}V}{\sqrt{2\pi} u_s \sigma_z}$$

Vertical term:

$$V = \exp\left[-0.5\left(\frac{z_r - h}{\sigma_z}\right)^2\right] + \exp\left[-0.5\left(\frac{z_r + h}{\sigma_z}\right)^2\right] + [\dots]$$

If $h = 0, z = 0, V=2$

Gaussian Approach Cont.



Gaussian Approach Cont.

Vertical Standard Deviation:

$$\sigma_z = ax^b$$

Constants a, b from Turner (1970) dependent on atmospheric stability and distance downwind

Guassain Approach Cont.

Additional Considerations:

- Initial height $\Rightarrow + x'$ to downwind distance

$$\sigma_z = a(x + x')^b = IH \approx H_{vehicle}$$

- Assume WS uniform with height. I.e. WS \times Time=Distance
- Limited accuracy near ground and near source

Box Model Approach

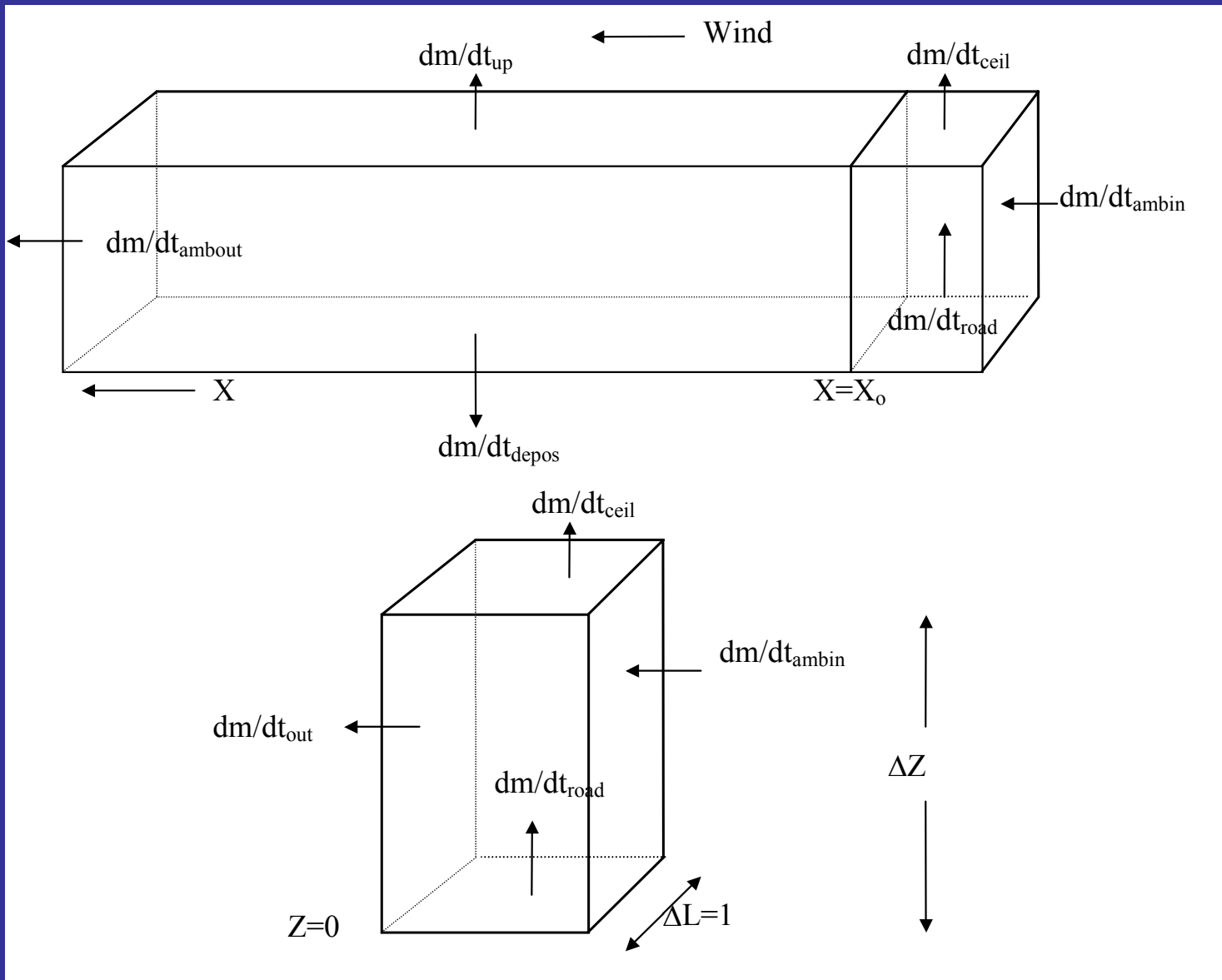
- Proposed by Gillette (2002)
- Mass balance on long box downwind of unpaved road. Particle flux only at entrance, top, and bottom
- Dispersion through top \propto Concentration

$$\frac{dm}{dt}_{top} = K * C$$

$$K = Au_*$$

- Deposition at ground \propto Concentration

$$\frac{dm}{dt}_{depos} = V_d * C$$



Box Model Cont

- Resultant Equation for Transportable Fraction

$$\Phi = \frac{\frac{dm_{up}}{dt}}{\frac{dm_{road}}{dt}} = \left[1 - \frac{V_d}{(V_d + K)} \right] = \frac{K}{(V_d + K)}$$

where V_d and K ($= 0.06 u^*$) are constant

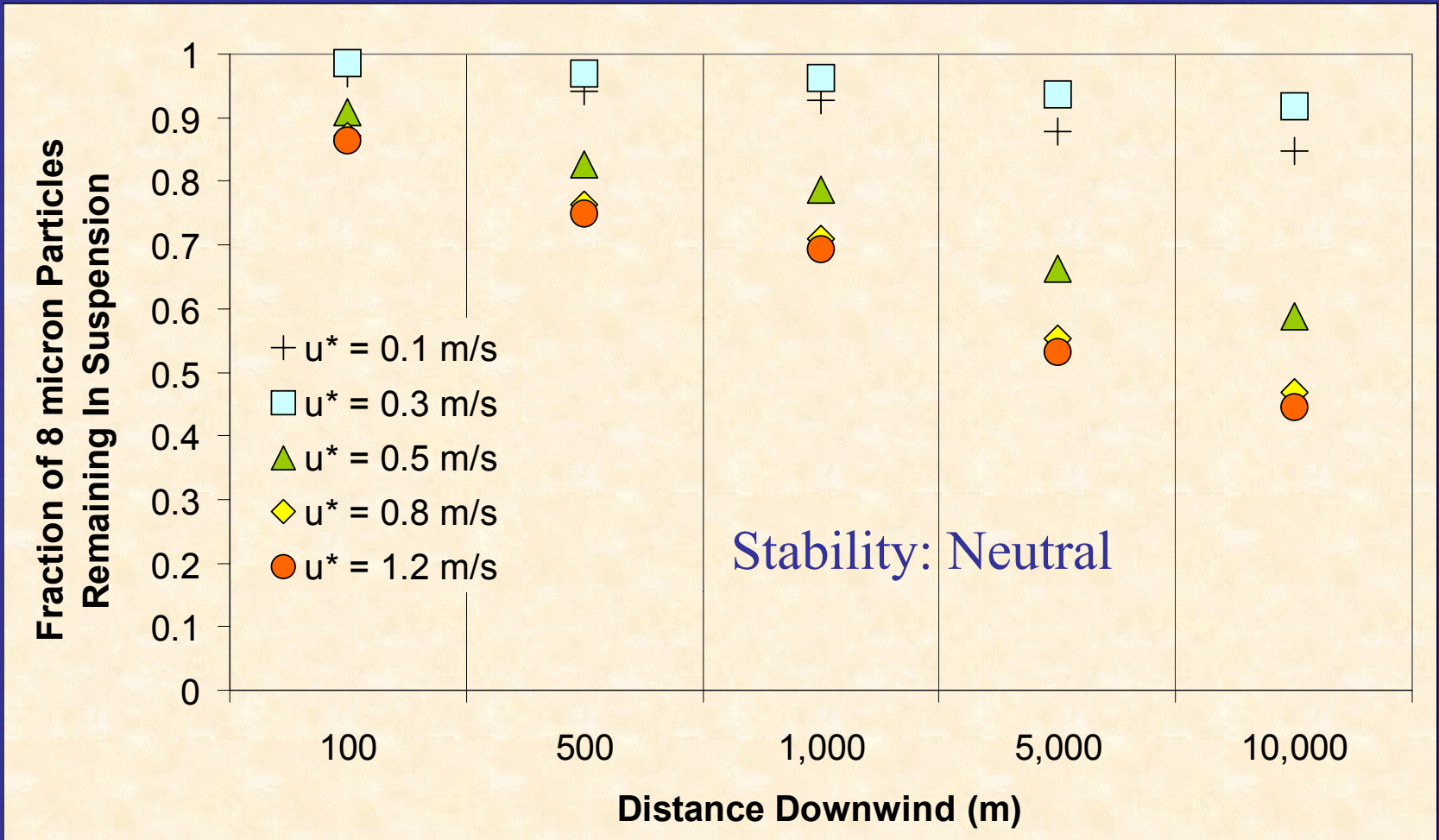
Dry Deposition

- Flux to Ground \propto Concentration

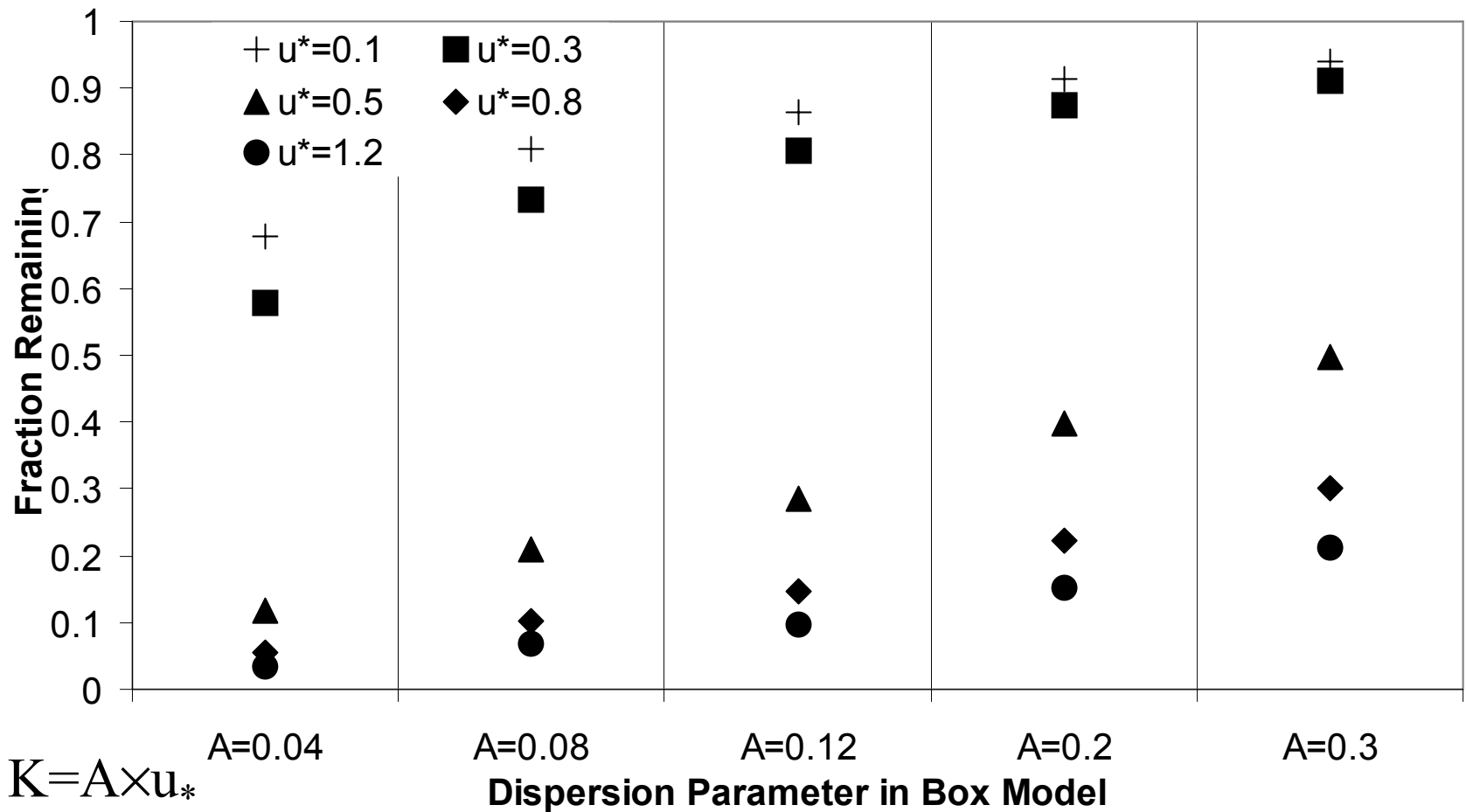
$$F_{dep} = V_d * C \quad V_d \equiv \text{Deposition velocity}$$

- Framed for removal from uniform concentration in bulk medium (e.g. Slinn, 1982)
 - Ground release is opposite situation
 - Roughness elements $<$ concentration profile
 - Assumptions may apply ~ 10 's m downwind
- Assume removal due to impaction mostly

Results: ISC Fraction in Suspension vs. distance



Results: Box Model Prediction



$$K = A \times u_*$$

Results: Box Model Difficulties

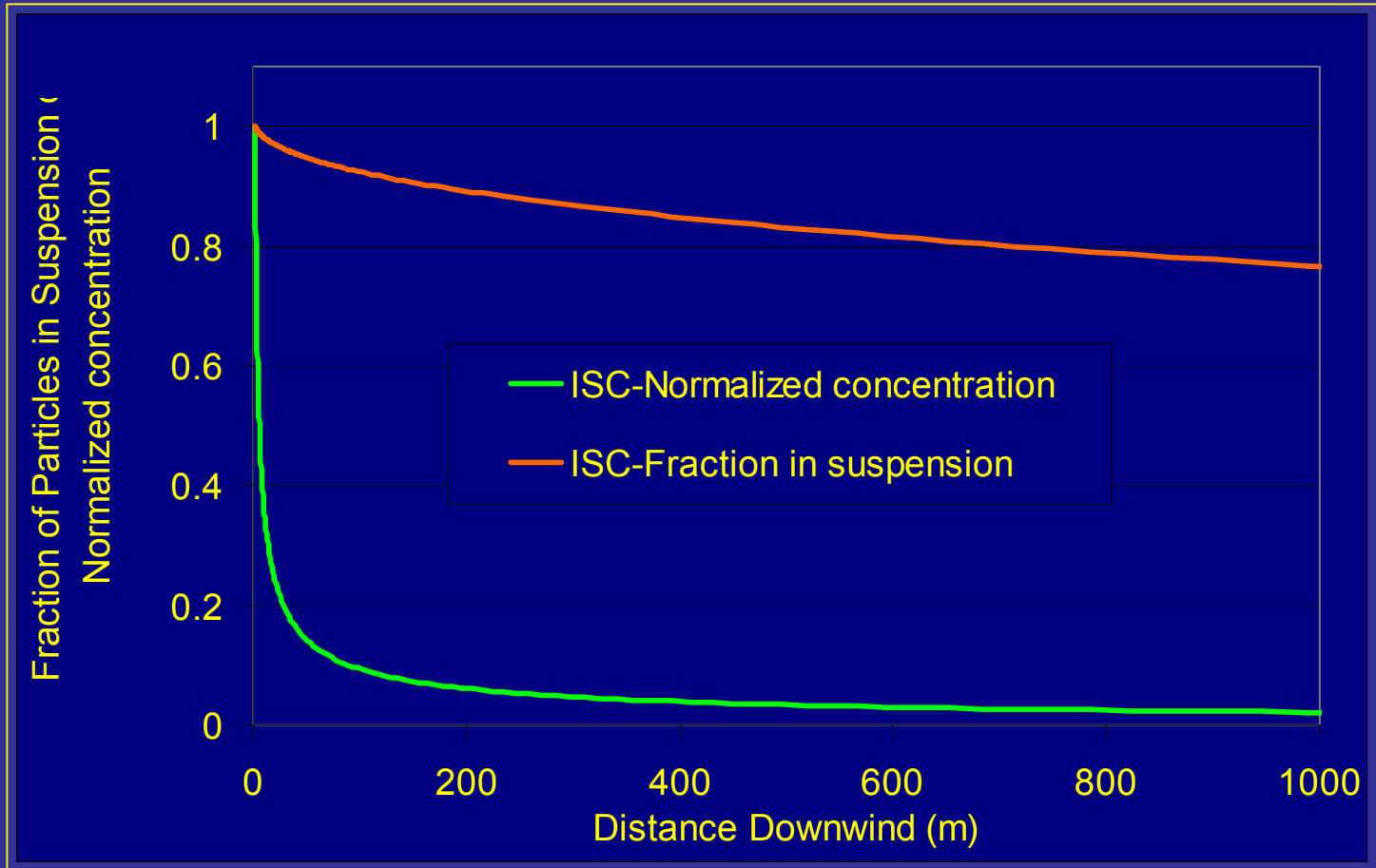
- Deposition O.K.
- For first order dispersion, I.e. $\frac{dm}{dt_{top}} = K * C$
Limited applicability
- To specify K correctly, require specification of distance downwind

Results: Stability and Transportable Fraction

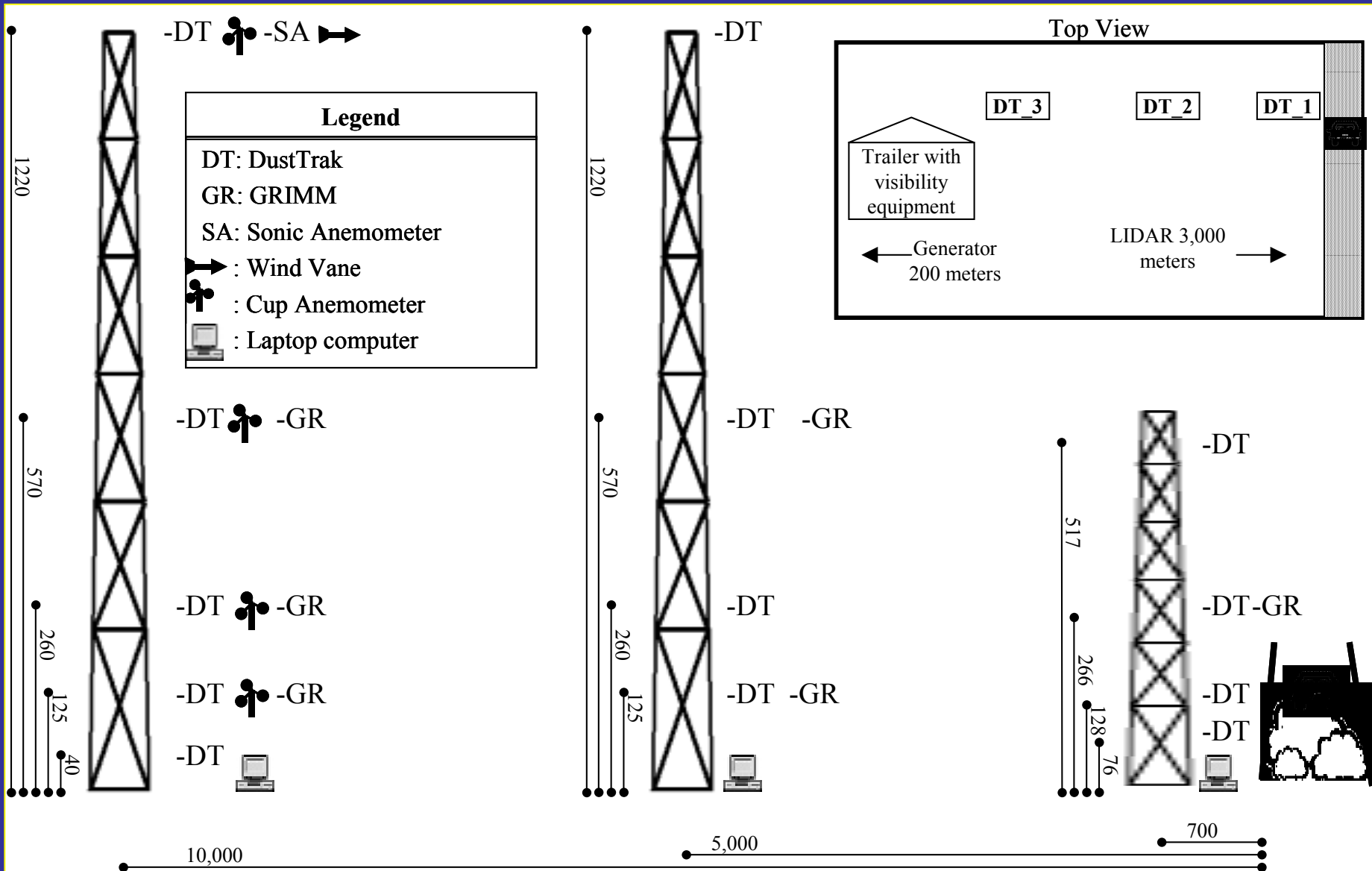
Stability	<u>$u^* = 0.3$ m/s</u>		<u>$u^* = 0.5$ m/s</u>	
	<i>500 m</i>	<i>5,000 m</i>	<i>500 m</i>	<i>5,000 m</i>
Very Stable	0.95	0.87	0.72	0.43
Stable	0.96	0.91	0.79	0.57
Neutral	0.97	0.94	0.83	0.66
Moderately Unstable	0.98	0.98	0.91	0.86
Very Unstable	0.99	0.99	0.93	0.92

Note: Particle size differences similar to u^* differences

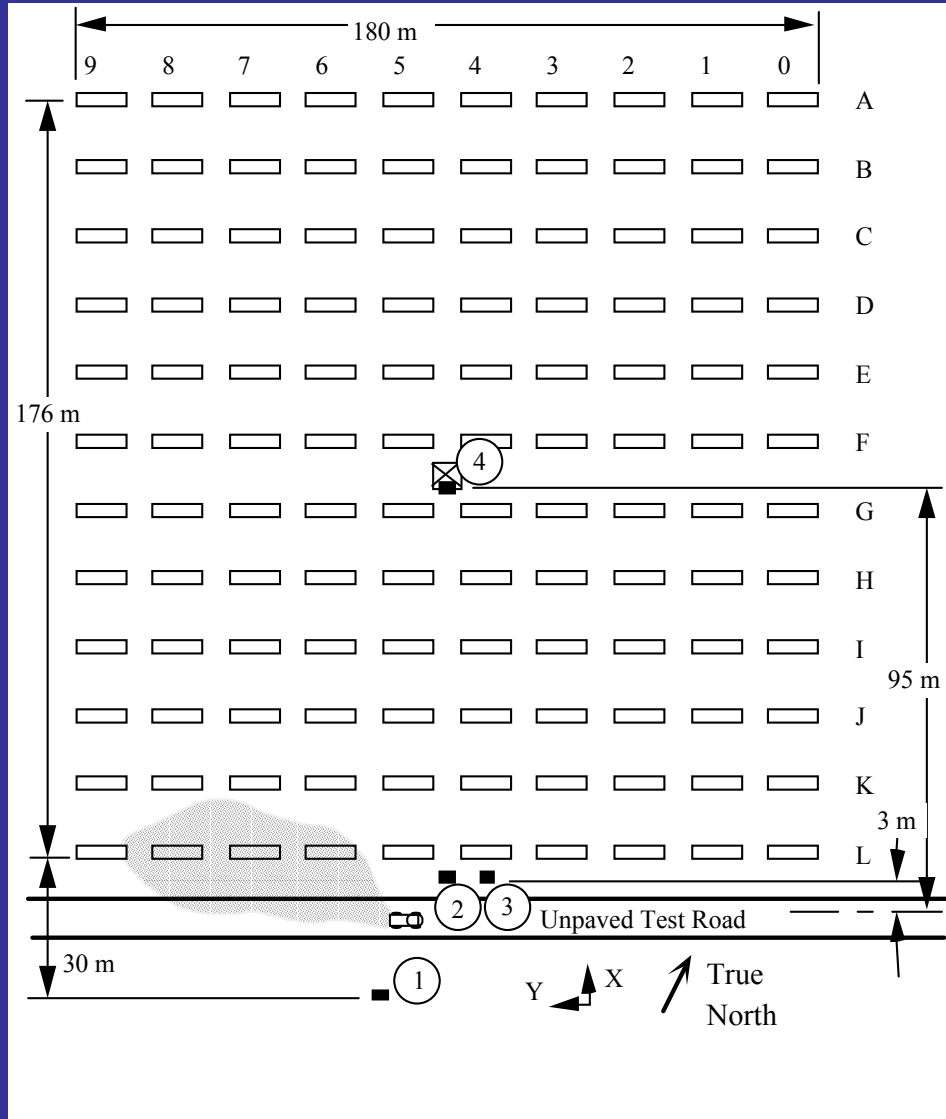
Results: Concentration not indicator of removal



Measurements: Daytime desert



Measurements: Nighttime urban?



Array of cargo containers.

Dimensions (m):
 $2.5 \times 2.4 \times 12.2$

Effective z_0 : 0.1 m

Effective u_* : 0.4 m/s

Results: Measurement vs. model

- Daytime Desert fraction PM_{10} removed:
 - Measured: 0%
 - Modeled: 3%
- Nighttime urban fraction PM_{10} removed:
 - Measured: 85%
 - Modeled: 30%

Conclusions

- Fraction of PM_{10} removed near source
 - Decreases with WS initially, increases at higher WS
 - Minimum for unstable conditions
 - Minimum for small roughness height
 - Not proportional to concentration
- Box model has limitation in dispersion

Future Work

- Gaussian model simple and holds promise
- Essential to have field data
 - Multiple atmospheric conditions
 - Multiple roughness (vegetative/land cover type and density)
- Examine “Region A” removal

