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PKL
EUGENE F. MOONEY
SECRETARY



AP-42 Section 11.30
Reference 11
Report Sect. 4
Reference 8

COMMONWEALTH OF KENTUCKY
DEPARTMENT FOR NATURAL RESOURCES AND ENVIRONMENTAL PROTECTION
BUREAU OF ENVIRONMENTAL PROTECTION

A. L. ROARK
COMMISSIONER

FRANKFORT, KENTUCKY 40601
January 9, 1979

Mr. Robert R. Lancaster, Plant Manager
Grefco, Inc.
P.O. Box 35
Florence, Kentucky 41042

RECEIVED
JAN 11 1979
New Products

ID: 079-0280-0021

Dear Mr. Lancaster:

This is to inform you the results of a review of your stack test report submitted to this Division on October 23, 1978.

On October 3, 4, and 5, 1978, compliance testing was performed on the perlite expanding furnace cyclone. These tests indicated an average particulate emission rate of 10.26 lb/hr, whereas the allowable rate, as specified by 401 KAR 3:060, Section 4 is 12.88 lb/hr. Therefore, this emission point was in compliance with the above regulation at the time of the test. A copy of the stack test evaluation report is enclosed for your review.

Sincerely,


William S. Coakley, Director
Enforcement and Surveillance Program
Division of Air Pollution Control

WSC:dh

cc: John T. Smither
Hisham M. Sa'aid
James W. Dills
Florence Regional Office
Case Preparation

pc: J. Carver
H. Baker
P. Mehta ✓

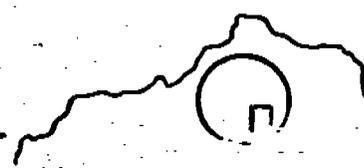
emission report

Sampling Observation and Report Review

Grefco, Incorporated
Perlite Insulation Board Plant
Florence, Kentucky
October 17, 1978

Sampling Performed by
Grefco, Incorporated
Engineering Department
Torrence, California

Observed and Reviewed by
Kentucky Division of Air Pollution Control

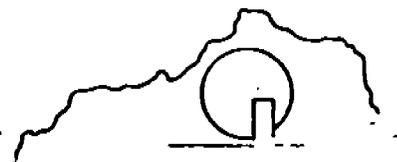


Sampling Observation and Report Review

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Florence, Kentucky
October 17, 1978

Sampling Performed by
Grefco, Incorporated
Engineering Department
Torrence, California

Observed and Reviewed by
Kentucky Division of Air Pollution Control



Report Certification

As observer and author I hereby certify that the sampling procedures were performed during my direct observation and general guidance and all data and conclusions in this report are authentic and accurate.

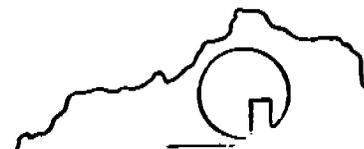
Date 12-18-78

Gerald H. Slucher
Gerald H. Slucher, Chief
Source Test Section
Division of Air Pollution
Control

As observer and author I hereby certify that the facility was operated during the testing according to my instructions.

Date 12/22/78

Samuel H. Bruntz
Samuel Bruntz
Engineering & Permits Program
Division of Air Pollution Control



INTRODUCTION

On October 3, 4 and 5, 1978, Kentucky Division of Air Pollution Control personnel were present at Grefco, Incorporated, Florence, Kentucky, to observe and provide general guidance during the compliance testing of the perlite expander cyclone stack in accordance with Kentucky Air Pollution Control Regulations 401 KAR 3:060, Section 4 applicable to standards of performance for existing process operations.

Representativeness of the compliance test data was based on Methods 1, 2, 3, and 5 in the August 18, 1977 Federal Register for the sampling procedures. The baseline process conditions were set by the Kentucky Division of Air Pollution Control. All compliance test conditions and procedures were agreed upon by Grefco and the Division at a pre-test meeting prior to the compliance testing field tests.

Present during the compliance test, as shown in Figure 1, were Sam Bruntz to monitor the process operations, Chris Finley to make visible emission evaluations, and Gerald Slucher to observe sampling procedures, all with the Kentucky Division of Air Pollution Control.

The following sections of this report treat the summary of representativeness of the compliance test, facility operations, sampling and analytical procedures, and review of compliance test report.

Process Description

The Grefco plant in Florence is engaged in the manufacture of fiberboard insulation. Perlite ore is shipped in by rail and pneumatically fed to a storage silo. Then, as required, ore is transferred by elevator to one of three perlite expanding furnaces. As the ore falls through the furnace, heat causes thermal expansion and the resultant expanded ore is then pneumatically blown through a series of cyclones, then mixed with a newspaper pulp and spread into a mat. The mat is fed through a series of rollers and, in the presence of a vacuum, is partially dehydrated. The mat is then blown with asphalt and baked in a drying oven. The completed mat is cut to customer specified board sizes, then shipped.

The perlite expanding furnaces are ducted to a wet cyclone which, in the past, has not been effective in reducing particulates emissions and opacity to the levels specified by regulation 401 KAR 3:060, Section 4. Grefco has therefore made modifications to the water spray system of the wet cyclone, such as the use of fresh city water rather than recycle process water and the addition of furnace shutdown mechanisms activated by items such as loss of water pressure.

The purpose of the stack test, therefore, was to determine the effectiveness of the modifications. During the test, the water spray pressure was observed to be 60 psig, and the process weight rates and allowables were as follows:

	<u>Process Weight Rate, TPH</u>	<u>Allowable (3:060(4) lbs/hr.</u>
	5.46	12.79
	5.55	12.93
	5.55	12.93
	<hr/>	<hr/>
Ave.	5.52	12.88



Summary of Representativeness of Data

All facility operating conditions and sampling procedures were discussed and agreed upon at the pre-test meeting on September 12, 1978, by Grefco representatives Praful Mehta, Gary Lockhart and Bill Eilau, and Division Representatives Sam Bruntz, Samuel Murphy, Steve Brown, and John Jayne.

The sampling and recovery procedures followed the August 18, 1977, Federal Register Methods 1, 2, 3, and 5. All sampling procedures were representative of the prescribed methods.

The analysis of the sample was conducted in the laboratory at the plant. The filters were desiccated and pre-weighed and final weights measured on the analytical balance at the plant. The procedures observed were acceptable.

No visible emissions evaluation was performed, but the regional inspector, Chris Finley, did file a report on 10/3/78 stating that there were no visible emissions.

All three test runs were observed and evaluated to have no significant biases.

Sampling and Analytical Procedures

Sampling and analytical procedures followed the August 18, 1977, Federal Register Methods 1, 2, 3, and 5.

The sample site checklist is presented in Figure 2. The sample site met the specified requirements to allow the sample to be withdrawn from the stack at 32 sample points. Very little buildup was present on the inner stack walls.

The sample train component and calibration checklist is presented in Figure 3. Calibration data was presented at the test and found to be acceptable. The meter box was calibrated by Pedco Environmental. All sample train components met guidelines set forth by EPA methods.

The sample train assembly and final preparation check list is presented in Figure 4. All train components were prepared and assembled properly. The leak rate was within the acceptable limits of each test.

The sample collection checklist is presented in Figure 5. The sample train was operated in the prescribed manner.

The sample recovery checklist is presented in Figure 6. The drying and weighing of the sample was done according to the prescribed procedures.

The sample residues and filters from the sample analysis were not requested to be shipped to the Division after the review of the compliance test report.

GENERAL/SAMPLING SITE

Stack/Duct Cross Section Dimensions 42" Equivalent Diameter _____
 Material of Construction steel Corroded? no Leaks no
 Internal Appearance - Corroded? _____ Caked Particulate? Thickness _____
 Insulation? no Thickness _____ Lining? no Thickness _____
 Nipple? I.D. 3" Length 6" Flush with Inside Wall? _____
 Straight Run Before Ports _____ Diameters 5 diam
 Straight Run After Ports _____ Diameters 2 diam
 Photos Taken? _____ of what _____

Drawing of Sampling Location:

Minimum information on drawing: stack/duct dimensions, location and description of major disturbances and all minor disturbances (dampers, transmissometers, etc.), and cross sectional view showing dimensions and port locations.

Table 4. (continued). OBSERVATION CHECKLIST

DPAC-110(Rev. 5-27-77)

GENERAL/SAMPLING SYSTEMSampling Method (e.g., EPA5) _____

Sampling Train Schematic Drawing: _____

Modifications to Standard Method _____

Pump Type: Fibervane with In-Line Oiler Carbon Vane Diaphragm Probe Liner Material SS Heated? Entire Length? Type "S" Pitot Tube? Other _____Pitot Tube Connected To: Inclined Manometer _____ Or Magnehelic Gauge Range 0-1" Approx. Scale Length _____ Divisions .02"Orifice Meter Connected To: Inclined Manometer _____ Or Magnehelic Gauge Range 0-3" Approx. Scale Length _____ Divisions .1"Meter Box Brand JOY Sample Box Brand JOY

Recent Calibration of Orifice Meter-Dry Gas Meter? _____ Pitot Tubes? _____

Nozzles _____ Thermometers or Thermocouples? _____ Magnehelic Gauges? _____

Numbers of Sampling Points/Traverse From Fed.Reg. _____ Number to be Used _____

Length of Sampling Time/Point Desired _____ Time to be Used _____

X - not required by regulations

Table 4 (continued). OBSERVATION CHECKLIST

DAPC-110(Rev.5-27-77)

TRAIN ASSEMBLY/FINAL PREPARATIONS

RUN # _____

(Use One Sheet Per Run if Necessary)

Filter Holder Clean Before Test? Filter Holder Assembled _____Correctly? Filter Media Type Fluorid Filter Clearly Identified? Filter Intact? Probe Liner Clean Before Test? Nozzle Clean? Nozzle Undamaged? Impingers Clean Before Test? Impingers Charged Correctly? Ball Joints or Screw Joints? ball Grease used? Kind of Grease silicone Pitot Tube Tip Undamaged?

Pitot Lines Checked for Leaks? _____ Plugging? _____

Meter Box Leveled? Pitot Manometer Zeroed? Orifice Manometer Zeroed? Probe Markings Correct? Probe Hot Along Entire Length? Filter Compartment Hot? Temperature Information Available? Impingers Iced Down? Thermometer Reading Properly? Barometric Pressure Measured? _____If Not, What is Source of Data _____ $\Delta H_{@}$ From Most Recent Calibration
_____ $\Delta H_{@}$ From Check Against Dry Gas Meter _____

Nomograph Check:

If $\Delta H_{@} = 1.80$, $TM = 100^{\circ} F$, $\% H_2O = 10\%$, $P_s/P_m = 1.00$, $C = \underline{X}$ (0.95)If $C = 0.95$, $TS = 200^{\circ} F$, $DN = 0.375$, Δp Reference = X (0.118)Align $\Delta p = 1.0$ with $\Delta H = 10$; @ $\Delta p = 0.01$, $\Delta H = \underline{X}$ (0.1)

For Nomograph Set-Up:

Estimated Meter Temperature X °F Estimated Value of P_s/P_m XEstimated Moisture Content X % How Estimated? _____C Factor X Estimated Stack Temperature X °F Desired NozzleDiameter X

Stack Thermometer Checked Against Ambient Temperature? _____

Leak Test Performed Before Start if Sampling? _____ Rate _____ CFM @ _____

SAMPLING (Use One Sheet For Each Run if Necessary)

Run # _____

Probe-Sample Box Movement Technique:

Is Nozzle Sealed When Probe is in Stack with Pump Turned Off? CKIs Care Taken to Avoid Scraping Nipple or Stack Wall? ✓Is an Effective Seal Made Around Probe at Port Opening? ✓Is Probe Seal Made Without Disrupting Flow Inside Stack? ✓Is Probe Marking System Adequate to Properly Locate Each Point? ✓Are Nozzle and Pitot Tube Kept Parallel to Stack Wall At Each Point? ✓If Probe is Disconnected From Filter Holder with Probe in the Stack on a Negative Pressure Source, How is Particulate Matter in the Probe Prevented From Being Sucked Back into the Stack? NAIf Filters are Changed During a Run, Was any Particulate Lost? NA

Meterbox Operation:

Is Data Recorded in a Permanent Manner? ✓ Are Data Sheets Complete? ✓Average Time to Reach Isokinetic Rate at Each Point 30 secIs Nomograph Setting Changed When Stack Temperature Changes Significantly? —Are Velocity Pressures (Δp) Read and Recorded Accurately? ✓Is Leak Test Performed at Completion of Run? < .02 cfm @ 7.5 In Hg.

General Comment on Sampling Techniques _____

If Orsat Analysis is Done, Was It: From Stack _____ From Integrated Bag _____

Was Bag System Leak Tested? _____ Was Orsat Leak Tested? _____
Check Against Air? _____

If Data Sheets Cannot Be Copied, Record: Approximate Stack Temperature _____ °F

Nozzle Dia. _____ In. Volume Metered _____ ACF

First 8 Δp Readings _____

Table 4 (continued). OBSERVATION CHECKLIST

SAMPLE RECOVERY

General Environment-Clean Up Area in Lab

Wash Bottles Clean? Brushes Clean? Brushes Rusty? NO

Jars Clean? Acetone Grade _____ Residue on Evap. Spec. _____

Filter Handled OK? Probe Handled OK? Impingers Handled OK?

After Cleanup: Filter Holder Clean? Probe Liner Clean?

Nozzle Clean? Impingers Clean? Blanks Taken? NO

Description of Collected Particulate light brown dust

Silica Gel All Pink? Run 1 NO Run 2 NO Run 3 NO

Jars Adequately Labeled? NA Jars Sealed Tightly? NA

Liquid Level Marked on Jars? NA Jars Locked Up? NA

General Comments on Entire Sampling Project:

Was the Test Team Supervisor Given the Opportunity to Read Over This Checklist? Yes Did He Do So? _____

Observer's Name Elizabeth W. ... Title Lead Source Test Technician

Affiliation ADAPC Signature Elizabeth W. ...

Table 5. SAMPLE RECOVERY CHECKLIST

Review of Compliance Test Report

The compliance test report followed the reporting format required by the Division. The reporting requirement checklist is presented in Figure 7. A review of the report and all calculations showed the data presentation to be representative and accurate. Figure 8, 9, and 10 present the data and calculations as verified with a Hewlett-Packard Model 10 programmable calculator.

The emission standard is 12.88 lbs/hr. The reported emission rate is 10.26 lbs/hr.

Based on the data and the discussions in the report and this review, it does not seem that any errors occurred which would have biased the results. It is recommended that this test report be accepted.



STACK TEST REVIEW

NAME GRFFCO

TEST NO. 1

SOURCE TYPE Portable Equipment

RUN NO. 1

MODEL OR NAME _____

DATE OF TEST 10-3-78

TEST PERFORMED BY GRFFCO

DATA REQUIRED	RESULTS
<p>T_s, Stack temperature <u>138.9</u> °F</p> <p>P_s, Stack pressure <u>29.97</u> in. Hg.</p> <p>T_m, Meter temperature <u>76.80</u> °F</p> <p>P_m, Meter pressure <u>29.99</u> in. Hg.</p> <p>M_w, Condensed water <u>225.5</u> gm</p> <p>V_{DGM}, Volume of sample (meter conditions) <u>401.30</u> cf</p>	<p>V_{H2O}, Volume of water <u>10.57</u> cf</p> <p>B_w, Moisture of content <u>12.70</u></p> <p>V_{ne}, Volume of sample at stack cond. <u>241.47</u> cf</p> <p>M_{dry}, Molecular wt dry _____</p> <p>M_{wet}, Molecular wt wet <u>21.55</u></p> <p>Velocity <u>31.27</u> fps</p>
<p>CO₂ _____ % <u>0</u></p> <p>O₂ _____ % <u>71</u></p> <p>CO₂ _____ % <u>0</u></p> <p>N₂ _____ % <u>71</u></p>	<p>Isokinetic Ratio <u>101.1</u></p> <p>gr/scf @ 12% CO₂ _____</p>
<p>ΔP, Velocity head <u>.24713</u> in. H₂O (traverse points)</p> <p>C_p, Pitot tube coeff. _____</p>	<p>Lb/Hr <u>9.6</u></p> <p>Lb/mm BTU _____</p>
<p><u>90</u> min x 60</p> <p>θ, Sampling time <u>90</u> min <u>sec</u></p> <p>A_n, area of nozzle D= " <u>0.0037409</u> ft²</p> <p>D² x 0.005454</p>	<p>REQUESTED BY _____</p> <p>REVIEWED BY _____</p> <p>DATE _____</p> <p>RECOMMENDATION _____</p>
<p>Weight of collected pollutant <u>2290</u> gm</p> <p>CO₂, Waste only _____ %</p>	
<p>A_s, Area of stack D= ft $\frac{D^2}{4} \pi$ <u>9.62</u> ft²</p>	
<p>Boiler Heat Capacity _____ mmBTU/Hr.</p>	

REMARKS

U

ENTER
 TS+X
 TN+Y
 ENTER
 PS-X
 PN+Y
 ENTER
 UL+X
 UN+Y
 ENTER
 OQ2+X
 OQ2+Y
 ENTER
 CO+X
 N2+Y
 ENTER
 DEL P.
 AVG P DEL P
 0.492858

ENTER
 CP+X
 THETA+Y
 ENTER
 AN+X
 MN+Y
 ENTER
 AS+X
 VMSTD
 39.870784

VMSTD
 10.688789

BW0
 0.211396

NS
 26.848403

MS
 31.272929

ISOKIN
 101.092105

CGMC
 LBS/FT3
 0.000000

ENTER

STACK TEST REVIEW

NAME GREFCO

TEST NO. _____

SOURCE TYPE Roller Exhauster

RUN NO. 2

MODEL OR NAME _____

DATE OF TEST 10-4-79

TEST PERFORMED BY GREFCO

DATA REQUIRED	RESULTS
<p>T_s, Stack temperature <u>128.75</u> °F</p> <p>P_s, Stack pressure <u>29.99</u> in.Hg.</p> <p>T_m, Meter temperature <u>76.8</u> °F</p> <p>P_m, Meter pressure <u>30.08</u> in.Hg.</p> <p>M_w, Condensed water <u>469.5</u> gm</p> <p>V_{DGM}, Volume of sample (meter conditions) <u>83.46</u> cf</p>	<p>V_{H_2O}, Volume of water <u>22.25</u> cf</p> <p>B_{wo}, Moisture of content <u>2.21</u></p> <p>V_{ne}, Volume of sample at stack cond. <u>82.825</u> cf</p> <p>M_{dry}, Molecular wt dry _____</p> <p>M_{wet}, Molecular wt wet <u>26.5</u></p> <p>Velocity <u>30.18</u> fps</p>
<p>CO₂ _____ % <u>0</u></p> <p>O₂ _____ % <u>21</u></p> <p>CO₂ _____ % <u>1</u></p> <p>N₂ _____ % <u>79</u></p>	<p>Isokinetic Ratio <u>101.3</u></p> <p>gr/scf @ 12% CO₂ _____</p>
<p>AP, Velocity head <u>225.71</u> in.H₂O (traverse points)</p> <p>C_p, Pitot tube coeff. <u>0.857</u></p>	<p>Lb/Hr <u>11.25</u></p> <p>Lb/mm BTU _____</p>
<p>_____ min x 60</p> <p>θ, Sampling time <u>90 min sec.</u></p> <p>A_n, area of nozzle D= " <u>0.00717</u> ft²</p> <p>D² x 0.005454</p>	
<p>Weight of collected pollutant <u>575.1 mg</u> gm</p> <p>CO₂, Waste only _____ %</p>	<p>REQUESTED BY _____</p> <p>REVIEWED BY _____</p> <p>DATE _____</p> <p>RECOMMENDATION _____</p>
<p>A_s, Area of stack D= ft $\frac{D^2}{4} \pi$ <u>9.62</u> ft²</p>	
<p>Boiler Heat Capacity _____ mmBTU/Hr.</p>	

REMARKS

ENTER
TS+X
TM+Y
ENTER
PS+X
PM+Y
ENTER
VL+X
VM+Y
ENTER
CD2+X
CD+Y
ENTER
CD+X
N2+Y
ENTER
DEL P
AVG P DEL P
0.475048

ENTER
CP+X
THETA+Y
ENTER
AN+X
MN+Y
ENTER
AS+X
VMSTD
82.825157

VMSTD
22.254300

BUO
0.211785

MS
26.544246

VS
30.180925

ISOKIN
101.341623

CONC
LBS/FT3
0.000015

EMISSIONS
LBS/HR
11.850977

STACK TEST REVIEW

NAME GREFLO

TEST NO. _____

SOURCE TYPE Waste Exports

RUN NO. 3

MODEL OR NAME _____

DATE OF TEST 10-5-78

TEST PERFORMED BY GREFLO

DATA REQUIRED	RESULTS
<p>T_s, Stack temperature <u>138.44</u> °F</p> <p>P_s, Stack pressure <u>30.00</u> in.Hg</p> <p>T_m, Meter temperature <u>75.23</u> °F</p> <p>P_m, Meter pressure <u>30.07</u> in.Hg</p> <p>M_w, Condensed water <u>485.5</u> gm</p> <p>V_{DGM}, Volume of sample (meter conditions) <u>46.46</u> cf</p>	<p>V_{H_2O}, Volume of water <u>23.01</u> cf</p> <p>B_{wo}, Moisture of content <u>2.211</u></p> <p>V_{ne}, Volume of sample at stack cond. <u>86.65</u> cf</p> <p>M_{dry}, Molecular wt dry _____</p> <p>M_{wet}, Molecular wt wet <u>76.55</u></p> <p>Velocity <u>30.6</u> fps</p>
<p>CO₂ _____ % <u>0</u></p> <p>O₂ _____ % <u>21</u></p> <p>CO₂ _____ % <u>0</u></p> <p>N₂ _____ % <u>79</u></p>	<p>Isokinetic Ratio <u>103.7</u></p> <p>gr/scf @ 12% CO₂ _____</p>
<p>ΔP, Velocity head <u>232188</u> in.H₂O (traverse points)</p> <p>C_p, Pitot tube coeff. <u>.857</u></p>	<p>Lb/Hr <u>9.97</u></p> <p>Lb/mm BTU _____</p>
<p>_____ min x 60</p> <p>θ, Sampling time <u>90</u> min sec</p> <p>A_D, area of nozzle D= <u>0.005454</u> ft²</p> <p>$D^2 \times 0.005454$ <u>0.00717</u></p>	
<p>Weight of collected pollutant <u>521.1 mg</u> gm</p> <p>CO₂, Waste only _____ %</p>	<p>REQUESTED BY _____</p> <p>REVIEWED BY _____</p> <p>DATE _____</p> <p>RECOMMENDATION _____</p>
<p>A_s, Area of stack D= ft $\frac{D^2}{4} \pi$ <u>9.62</u> ft²</p>	
<p>Boiler Heat Capacity _____ mmBTU/Hr.</p>	

REMARKS

3

ENTER
 TR+X
 TR-Y
 ENTER
 PS-X
 PR-Y
 ENTER
 VL-X
 VH-Y
 ENTER
 COZ+X
 UL-Y
 ENTER
 CO+X
 N2-Y
 ENTER
 DEL P
 AVG P DEL P
 0.481859

ENTER
 CP+X
 THETA+Y
 ENTER
 AN+X
 MH+Y
 ENTER
 AS+X
 VMSTD
 86.054023

VMSTD
 20.012700

BMD
 0.210997

MS
 22.552736

VC
 30.595655

ISOKIN
 103.673131

CGHC
 LBS/FTS
 4.000000

EMIS

GREFCO, INC.
ENGINEERING DEPARTMENT
TORRANCE, CALIFORNIA

Project No. : 384-FL

STACK EMISSION MEASUREMENT AT GREFCO's
PERMALITE INSULATION BOARD PLANT
FLORENCE, KENTUCKY

A report prepared for Kentucky Division of
Air Pollution Control, Frankfort, Kentucky

October 17, 1978

Prepared and submitted by:
P. A. Mehta, Sr. Process Engineer

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INTRODUCTION

Three sets of particulate emission measurements were made on the perlite expanders cyclone stack at the Florence plant during the week of October 2, 1978. These tests were conducted to demonstrate to the Kentucky Division of Air Pollution control that the particulate emissions from the perlite expander stack are within the allowable rate as set forth in the most recent Kentucky Air Pollution control regulations, Section 401-KAR 3:060, Standards of Performance for Existing Source, Section 5, Table 3, Page 16-17.

Representatives of the Kentucky Division of Air Pollution Control, Messers Gerald H. Slucher, Chief, Source Test Section; and Samuel Bruntz, Environmental Engineer were present to witness the first test on October 3. Mr. Chris Finley, Divisional Air Pollution Control Inspector joined the later part of the test on October 3. Mr. Slucher was present during the next two tests conducted on October 4 and 5, 1978. Florence Plant Quality Control Laboratory Supervisor, Mr. Donald Black assisted the writer in successfully conducting the tests.

During the last labor day weekend, a new, larger furnace exhauster was installed to replace two smaller blowers. Water is introduced through eight nozzles, equally divided before and after the blower to control and maintain stack emissions within allowable limits. Introduction of fresh water ahead of blower did not pose any mechanical or operational problems. Each of the eight sprays is equipped with a flow switch connected to an alarm. Decrease in the water pressure or in the water flow from a set point will activate the alarm, and also will shut off the perlite feed to the furnaces, and subsequently the plant operation.

The tests were conducted under normal plant operation, and in accordance with the

EPA Method 5, outlined in the Federal Register, Vol. 42, No. 160, August 18, 1977; Pages 41776-41782.

RESULTS AND CONCLUSIONS

Results of the three tests are summarized below. Detailed summary of the results are attached to this report.

<u>Test No.</u>	<u>I</u>	<u>II</u>	<u>III</u>	<u>Average</u>
Date	Oct.3, 78	Oct.4, 78	Oct.5, 78	
Process Weight - TPA	5.46	5.55	5.55	5.52
Allowable Emissions(lbs/Hr)*	12.785	12.926	12.926	12.879
Actual Emissions(lbs/Hr)	9.387	10.930	9.693	10.00
Air Flow - Actual CFM	17,990	17,225	17,556	17,590
Isokinetic Variations - %	96.4	97.8	99.4	98.4

* The allowable emissions are based on the Formula:

$$E = 4.10 \times P^{0.67}$$

E = Emissions (lbs/Hr)

P = Process Weight -(Tons/Hr)

Results of each test indicate that the emissions from the expanders cyclone stack are within the allowable limits and hence in compliance with the Kentucky State Air Pollution Regulations, 401-KAR, 3:060.

Mr. Chris Finley's Inspection Report is also attached. His findings indicate that there were no visible emissions from the stack.

4
DIVISION OF AIR POLLUTION

INSPECTION REPORT

REFERS TO COMPLAINT NO. _____	FILE NO. <u>0790280</u>
DATE <u>10/3/79</u>	TIME <u>am</u> to <u>am</u> pm
INSPECTION TYPE: S SI <u>CS</u> F E C	
A. GENERAL:	
FACILITY NAME <u>GREFCO</u>	Phone _____ (area code)
Location <u>7125 INDUSTRIAL RD</u>	_____
<u>FLORENCE KY</u>	_____
PERSON CONTACTED <u>DON BLACK</u>	Title <u>LAB SUPER</u>
WEATHER <u>SHOWERS</u>	TERRAIN CONDITIONS <u>INDUSTRIAL PARK</u>
B. EQUIPMENT & PROCESS DESCRIPTION	
<u>INSULATION BOARD MANUFACTURE</u> <u>COMPANY'S OWN STACK TEST TEAM</u>	
C. CONTROL EQUIPMENT	
<u>WET CYCLONE</u> <u>ALARM SYSTEM</u> <u>CYCLONE USED IN PROCESS)</u>	
D. FINDINGS	
<u>STACK TEST - PARTICULATES</u> <u>4 TONS/HR OUTPUT → 12 LBS/HR ALLOWABLE</u> <u>EMISSIONS</u> <u>NO VISIBLE EMISSIONS - STEAM ONLY</u>	
REGULATIONS VIOLATED:	
E. RECOMMENDED CORRECTIVE ACTION:	
<u>2 ADDITIONAL TESTS SCHEDULED FOR</u> <u>10/4/78</u> <u>LBS/min - PROCESS RATE; 1% = 1 LB.</u>	
INVESTIGATOR'S SIGNATURE _____	Title _____
I hereby acknowledge receipt of a copy of this report and do further acknowledge that I have been apprised of the discrepancies and alleged violations noted during the inspection.	
SIGNED _____	Title _____
F. OFFICE USE ONLY	
cc: <u>G. Carcich</u> <u>G. Lockard</u> <u>P. Baker</u> <u>P. Mehta</u>	
LOG NO. _____	

4.

DIVISION OF AIR POLLUTION
INSPECTION REPORT

REFERS TO COMPLAINT NO. _____	FILE NO. <u>0790280</u>
DATE <u>10/3/79</u>	TIME _____ am pm to am pm
INSPECTION TYPE: S SI <u>(S)</u> P E C	
A. GENERAL:	
FACILITY NAME <u>GREFCO</u>	Phone _____ (area code)
Location <u>7125 INDUSTRIAL RD</u> <u>FLORENCE KY</u>	_____
PERSON CONTACTED <u>DON BLACK</u>	Title <u>LAB SUPER</u>
WEATHER <u>SHOWERS</u>	TERRAIN CONDITIONS <u>INDUSTRIAL PARK</u>
B. EQUIPMENT & PROCESS DESCRIPTION <u>INSULATION BOARD MANUFACTURE</u> <u>COMPANY'S OWN STACK TEST TEAM</u>	
C. CONTROL EQUIPMENT <u>WET CYCLONE</u> <u>ALARM SYSTEM</u> <u>COYCLONE USED IN PROCESS)</u>	
D. FINDINGS <u>STACK TEST - PARTICULATES</u> <u>4 TONS/HR OUTPUT → 12 LBS/HR ALLOWABLE</u> <u>EMISSIONS</u> <u>NO VISIBLE EMISSIONS - STEAM ONLY</u>	
REGULATIONS VIOLATED:	
E. RECOMMENDED CORRECTIVE ACTION: <u>2 ADDITIONAL TESTS SCHEDULED FOR</u> <u>10/4/78</u> <u>LBS/MIN - PROCESS RATE; 1% = 1 LB.</u>	
INVESTIGATOR'S SIGNATURE _____	Title <u>INSPECTION</u>
I hereby acknowledge receipt of a copy of this report and do further acknowledge that I have been apprised of the discrepancies and alleged violations noted during the inspection.	
SIGNED <u>Don Black</u>	Title <u>LAB SUPER</u>
F. OFFICE USE ONLY <u>DATE 10/3/79</u> <u>BY [Signature]</u> <u>DIVISION REPS</u>	
LOG NO. _____	

cc: G. Carcich
J. Lockard
M. Baker
P. Mehta

PLANT: FLORENCE "PSRI" BOARD PLANT

STACK TESTED: PERLITE EXPANDER CYCLONE (WET) STACK

SUMMARY OF DATA AND RESULTS

TEST NUMBER		1	2	3	Average
DATE		Oct. 3, '78	Oct. 4, '78	Oct. 5, '78	
GAS COMPOSITION	CO ₂ %	5.2	5.0	4.7	5.0
	O ₂ %	14.5	14.8	15.2	14.8
	N ₂ %	80.3	80.3	80.1	80.2
A _n Nozzle Area	Ft ²	0.0003342	0.0007167	0.0007167	-----
A _s Stack Area	Ft ²	9.62	9.62	9.62	9.62
ACFM Air Volume @ Stack Cond.	CF ³ /Min.	17,990	17,225	17,556	17,590
C Particulate Conc.	Grain/SCF*	0.08724	0.10597	0.0922	0.09514
dH Pressure Drop Across Orifice	"w.c.	0.284	1.300	1.330	0.971
D _n Nozzle Diameter	In.	0.2475	0.3625	0.3625	-----
D _s Stack Diameter	In.	42	42	42	42
E Emission Rate	lbs/hr.	9.387	10.930	9.693	10.00
F _w Mole Fraction Water		0.208	0.208	0.208	0.208
I Isokinetic	%	96.74	97.83	99.40	98.0
M _d Molecular Wt. -Dry	lb/lb mole	29.41	29.39	29.36	29.39
M _s Molecular Wt. -Wet	lb/lb mole	27.038	27.019	26.997	27.02
√P Pitot Reading Sq. Average	"w.c.	0.4943	0.4735	0.4823	0.4834
P _h Barometric Pressure	" Hg	29.96	29.99	29.98	29.98
P _s Stack Pressure Absolute	" Hg	29.97	30.00	29.99	29.99
SCFM (wet) 68 °F & 29.92" Hg	SCF/Min.				
SCFM (dry) 68 °F & 29.92" Hg	FT ³ /Min.	12,554	12,033	12,263	12,283
SG Specific Gravity (stack conditions)					
T _m Gas Temp. @ Meter **	°R	530**	530**	530**	530**
T _s Stack gas temp.	°R	600	600	600	600
V _{ic} Condensate	Gms.	225.5	469.5	485.5	393.5
V _m Dry Gas Sampled	Ft ³	40.58	84.04	87.07	69.56
V _s Average Stack Gas Velocity	Ft/Sec.	31.17	29.84	30.42	30.48
V _s " " " "	Ft/Min.	1870	1790	1825	1829
W _t Sample Weight	Grams	0.2290	0.5781	0.5211	0.4427
θ Sampling Time	Minutes	96	96	96	96
K Pitot Coefficient		0.857	0.857	0.857	0.857
Process Weight Rate	lbs./Hr.	10,920	11,100	11,100	11,040
Allowable Emission Rate	lbs./Hr.	12.785	12.926	12.926	12.879
Actual Emission Rate	lbs./Hr.	9.387	10.930	9.693	10.00
** Gas Meter Compensated @ 70 °F					
* Dry SCF @ 68 °F & 29.92" Hg					

EQUIPMENT & TEST PROCEDURE

Western Precipitation Division/Joy Manufacturing Co. (Los Angeles, California) Emission Parameter Analyzer (EPA II) was used for sampling the stack. This EPA sampling train is essentially the same as the one recommended and shown on Page 41777 of Federal Register, Vol. 42, No. 160, August 18, 1977.

Test procedure, equipment, and data sheet to be used were discussed and agreed upon in the meeting held on September 12, 1978 with the Grefco personnel and the members of the Kentucky Division of Air Pollution Control at Frankfort, Kentucky.

The dry gas meter was calibrated against wet test meter before and after the testing by an independent testing laboratory. The dry gas meter was within the tolerance. Their results are attached in the appendix. Each sampling nozzle was accurately measured to the nearest 0.001 inch and the S-type pitot tube was calibrated and its coefficient was determined.

Prior to each test, the equipment was tested for leaks and it was maintained below 0.02 CFM at about 15-20 inches of Hg vacuum. Nominal 0.25" diameter was used for the first test, and later was changed to 3/8" diameter nozzle at the request of Mr. Slucher.

Carbon dioxide and oxygen in the flue gases were determined with the Fyrites. Reagent grade acetone was used for washing sampling nozzle, probe, and particulate contaminated glasswares. All weight, other than that of silica gel were recorded to the nearest 0.1 milligram. The weight of silica gel was recorded to the nearest 0.5 gram. The condensate from each impinger was measured to the nearest 1 ml.

All samplings were done isokinetically. Prior to each test, a complete velocity traverse were taken using caliberated S-type pitot tube. Both, velocity traverse points and particulate traverse points were determined from figure 1-1 of Federal Register, Vol. 42, No. 160, Aug. 18, 1977, Page 41756. A sketch (DWG. NO. FL 384-A-29) showing sampling points location and a sketch (DWG. NO. FL 384-A-26) showing sampling port location are attached.

DISCUSSION:

This report covers the results of three tests conducted on the expander cyclone stack during the Florence Board Plant normal operation.

Water was introduced before and after the furnace exhauster to reduce stack emissions. This technique has been in use to reduce particulate emissions at several Grefco plants and they are in compliance with their respective state air pollution codes.

Several tests taken at the Florence Board Plant since the larger blower installation, including the three tests discussed in this report have indicated that the emissions from the perlite expander stack are lower by about 25% than allowable rate.

It is the writers opinion that excess of water before the blower may show high emissions in a stack test because excess water may cause free droplets, containing particulates to escape through the stack. However, as long as the stack gases are not supersaturated, the emissions from the stack will be lower than allowable rate.

It should be noted that the formula used in calculating the emission rates are the same as given in the Federal Register, Pg. 41776-41782 except the nomenclature and the formats are different.

A P P E N D I X

DATA, CALCULATIONS, AND RESULTS

FIELD DATA

PLANT Grefco - Florence, Ky
 DATE 10-3-78
 SAMPLING LOCATION EXP CYC
 SAMPLE TYPE Particulate
 RUN NUMBER 2
 OPERATOR PAM & D. Black
 AMBIENT TEMPERATURE 60°F
 BAROMETRIC PRESSURE 29.98
 STATIC PRESSURE, (P_s) +0.02"
 FILTER NUMBER(s) A

PROBE LENGTH AND TYPE 4' S.S.
 NOZZLE I.D. 0.2475
 ASSUMED MOISTURE 21%
 SAMPLE BOX NUMBER _____
 METER BOX NUMBER _____
 METER AND _____
 C FACTOR _____
 PROBE HEATER SETTING @ 250°F
 HEATER BOX SETTING 250°F
 REFERENCE Δp _____

Test #1

SCHEMATIC OF TRAVERSE POINT LAYOUT
 READ AND RECORD ALL DATA 3 MINUTES

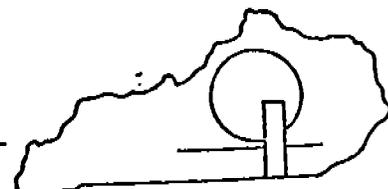
Probe = 250 ± 10

10:25 AM

TRAVERSE POINT NUMBER	SAMPLING Time, min	CLOCK TIME (24 hr CLOCK)	GAS METER READING (V _m) ft ³	VELOCITY HEAD (A _{ps}), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPINER TEMPERATURE °F
					DESIRED	ACTUAL		INLET (T _{m_in}), °F	OUTLET (T _{m_out}), °F			
			2950.0				1	4	6		3	5
1	0		2950	0.16	0.17	0.17	120	65	70	1.5	245	110
2	3		2951.05	0.21	0.23	0.23	140	60	75	1.5	275	160
3	6		2952.27	0.21	0.23	0.23	140	60	75	1.5	275	160
4	9		2953.46	0.17	0.19	0.19	140	60	75	1.5	265	180
5	12		2954.48	0.17	0.19	0.19	140	60	75	1.5	265	180
6	15		2955.51	0.17	0.19	0.19	110	60	80	1.5	255	180
7	18		2956.55	0.19	0.21	0.21	140	60	80	2.0	255	180
8	21		2957.71	0.19	0.21	0.21	140	60	85	2.0	255	180
9	24		2958.86	0.22	0.24	0.25	140	60	90	2.0	245	185
10	27		2960.09	0.25	0.27	0.27	140	60	90	3.0	245	185
11	30		2961.39	0.26	0.28	0.28	140	60	90	3.0	245	190
12	33		2962.65	0.30	0.33	0.35	140	60	95	3.5	245	190
13	36		2964.11	0.32	0.35	0.35	140	60	95	3.5	250	195
14	39		2965.55	0.36	0.39	0.40	140	60	95	3.5	250	195
15	42		2967.10	0.37	0.41	0.41	140	60	100	4.0	255	200
16	45		2969.18	0.40	0.44	0.45	140	65	100	4.0	260	205
			END @ 44 2970.23									
				Ave	ΔH = 0.274							
			V _H	0.41911			140°F					

CONDITIONS:

2970.23 - 2950 = 20.23 CFM



FACILITY GREFCO, INC.
LOCATION FLORENCE, KY
DATE _____

SAMPLE ID NUMBER A
TEST TEAM P.A. Mehta & D. Black
ANALYST P.A. Mehta

FRONT HALF

FILTER TARE WT. A

WEIGHING NO. 1 0.7832 g.
WEIGHING NO. 2 0.7831 g.
WEIGHING NO. 3 0.7834 g.

FILTER FINAL WT.

WEIGHING NO. 1 0.9404 g.
WEIGHING NO. 2 0.9401 g.
WEIGHING NO. 3 0.9403 g.

FILTER NET WT.

FINAL WT. 0.9403 g.
TARE WT. 0.7834 g.
NET WT. 0.1569 g.

BEAKER TARE WT. A

WEIGHING NO. 1 50.4682 g.
WEIGHING NO. 2 50.4680 g.
WEIGHING NO. 3 50.4683 g.

BEAKER FINAL WT.

WEIGHING NO. 1 50.5406 g.
WEIGHING NO. 2 50.5404 g.
WEIGHING NO. 3 50.5404 g.

FRONT WASHINGS NET WT.

FINAL WT. 50.5404 g.
TARE WT. 50.4683 g.
NET WT. 0.0721 g.

VOLUME OF WASHINGS 95 ml.

FILTER NET WT. 0.1569 g.
WASHINGS NET WT. 0.0721 g.

FRONT HALF SUBTOTAL 0.2290 g.

BACK HALF

BEAKER TARE WT.

WEIGHING NO. 1 ~~_____~~ g.
WEIGHING NO. 2 ~~_____~~ g.
WEIGHING NO. 3 ~~_____~~ g.

BEAKER FINAL WT.

WEIGHING NO. 1 ~~_____~~ g.
WEIGHING NO. 2 ~~_____~~ g.
WEIGHING NO. 3 ~~_____~~ g.

BACK WASHINGS NET WT.

FINAL WT. ~~_____~~ g.
TARE WT. ~~_____~~ g.
NET WT. ~~_____~~ g.

VOLUME OF WASHINGS _____ ml.

BACK HALF SUBTOTAL _____ g.

TOTAL PARTICULATE _____ g.

ACETONE BLANK

BEAKER TARE WT.

WEIGHING NO. 1 _____ g.
WEIGHING NO. 2 _____ g.
WEIGHING NO. 3 _____ g.

BEAKER FINAL WT.

WEIGHING NO. 1 _____ g.
WEIGHING NO. 2 _____ g.
WEIGHING NO. 3 _____ g.

VOLUME OF ACETONE BLANK _____ ml.

TOTAL PARTICULATE _____ g.
BLANK CORRECTION _____ g.

CORRECTED TOTAL PARTICULATE _____ g.

MOISTURE

IMPINGERS

FINAL VOLUME 416 g.
INITIAL VOLUME 200 g.
NET VOLUME 216 g.

SILICA GEL

FINAL WEIGHT 259.5 g.
INITIAL WEIGHT 250.0 g.
NET WEIGHT 9.5 g.

TOTAL MOISTURE 225.5 g.

SAMPLING DATA

Date: 10-3-78 Plant: Florence, KY Location: EXP. CYC. Stack Test no: 1

MOLECULAR WEIGHT:

COMPONENT	1	2	3	Ave.	Mol. Wt.	Mole Frac.
Carbon Dioxide %	5.5	5.0	5.0	5.2	.44	2.288
Oxygen %	14.5	14.5	14.5	14.5	.32	4.640
Carbon Monoxide %	-	-	-	-	.28	-
Nitrogen %	80.0	80.5	80.5	80.3	.28	22.484

Average Molecular Weight - $M_a = 29.412$ lb.Mol

MOLECULAR WEIGHT OF STACK GASES:

$$M_s = M_a (1 - F_w) + 18 \times F_w$$

$$= 29.412 (1 - 0.20805) + 18 \times 0.20805 = 27.038$$

ANALYTICAL DATA:

A. Weight of the particulate collected

Container	Final Weight - Gms	Tare - Gms.	Weight Gained - Gms.

Total Weight - Grams:

B. Weight of Liquid Water Collected:

Container	Final	Initial	Difference
Impinger no.1	255 ml.	100 ml.	155 ml.
Impinger no.2	157 ml.	100 ml.	57 ml.
Impinger no.3	4 ml.	0 ml.	4 ml.
Silica Gel -	259.5 Gms.	250 Gms.	9.5 Gms.

Assuming density of water = 1 gm/cc, Total Weight: 225.5 Grams.

CALCULATIONS

TEST #1

PLANT: Florence, KY STACK EXP. CYC. stack DATE: 10-3-78

METER: $V_m =$ 40.58 Ft^3 $P_m =$ 29.98 in. Hg $T_m =$ 530 $^{\circ}\text{R}^*$

STACK: $P_b =$ 29.96 in. Hg $P_s =$ 29.96 in. Hg $T_s =$ 600 $^{\circ}\text{R}$

SAMPLE: $\theta =$ 96 Min. $Wt =$ 0.2290 Grams $Vic =$ 225.5 ML.

$M_s =$ 27.038 $A_s =$ 9.62 Ft^2 $A_d =$ 3.342×10^{-4} Ft^2

F_w FRACTIONAL MOISTURE CONTENT OF THE STACK GAS:-

$$= \frac{\frac{Vic}{8164.8} + \frac{0.0458 V_m \times P_m}{T_m}}{\frac{225.5}{8164.8} + \frac{0.0458 \times 40.58 \times 29.98}{530}}$$

where $P_m = P_{bar} + dh/13.6$
 $= 29.98 + \frac{0.284}{13.6}$
 $=$

0.20805 Fractional Moisture Content

V_s AVERAGE STACK GAS VELOCITY:-

$$= 85.48 \times (K \times \sqrt{\Delta P_{ave.}})^{1/2} \times \left(\frac{T_s}{P_s \times M_s} \right)^{1/2}$$

$$= 85.48 \times 0.857 \times 0.49434 \times \left[\frac{600}{29.96 \times 27.038} \right]^{1/2}$$

31.167 AVERAGE VELOCITY FEET/SEC. V

ACFM EXHAUST GAS VOLUME @ STACK CONDITIONS:-

$$= 60 \times V_s \times A_s$$

$$= 60 \times 31.167 \times 9.62$$

17,990 STACK GAS VOLUME CFM AC

PLANT: Florence, KY.

STACK: Expander Cyclone

DATE: 10-3-78

$V_{scfm} \text{ (dry)}$ EXHAUST GAS VOLUME @ STANDARD CONDITIONS (68°F & 29.92" Hg) - DRY:-

$$\begin{aligned} &= \frac{ACFM \times (1 - F_w) \times T_{std} \times P_s}{29.92 \times T_s} \\ &= 17,990 \times (1 - 0.20805) \times \frac{528 \times 29.96}{29.92 \times 600} \\ &= \underline{12.554} \quad \text{SCFM STACK GAS VOLUME - DRY} \end{aligned}$$

V_{m-std} DRY GAS VOLUME SAMPLED @ STANDARD CONDITIONS:-

$$\begin{aligned} &= 0.00006306 \times V_m \times P_m \times T_{std} \\ &= 0.00006306 \times 40.58 \times 29.98 \times 528 \\ &= \underline{40.507} \quad \text{SCF-DRY GAS VOLUME SAMPLED} \end{aligned}$$

C_s GRAIN LOADING - GRAINS PER STANDARD CUBIC FEET DRY:-

$$\begin{aligned} &= \frac{15.4321 \times W_t}{V_{m-std}} \\ &= \frac{15.4321 \times 0.2290}{40.507} \\ &= \underline{0.08724} \quad \text{GRAINS PER STANDARD FT}^3 \text{ DRY -} \end{aligned}$$

E PARTICULATE EMISSION RATE - POUNDS PER HOUR:-

$$\begin{aligned} &= 0.008571 \times C_s \times V_{scfm-dry} \\ &= 0.008571 \times 0.08724 \times 12,554 \\ &= \underline{9.387} \quad \text{lb/hr.} \quad \text{EMISSION RATE - E} \end{aligned}$$

CALCULATIONS

PLANT: Florence, KY

STACK: Expander Cyclone

DATE: 10-3-78

I ISOKINETIC SAMPLING VARIATION:-

$$= \frac{1.667 \times T_s}{\theta \times V_s \times P_s \times A_n} \times \left[(0.00267 \times V_{ic}) + \frac{(V_m \times P_m)}{T_m} \right]$$

$$= \frac{1.667 \times 600}{96 \times 31.167 \times 29.96 \times 3.342 \times 10^{-4}} \times \left[(0.00267 \times 225.5) + \frac{(40.58 \times 29.98)}{530} \right]$$

$$= \underline{96.74} \quad \underline{\text{PERCENT ISOKINETIC VARIATION}}$$

P PROCESS WEIGHT RATE:

10,920

POUNDS PER HOUR

ALLOWABLE

ACTUAL

GRAIN LOADINGS - C_s

EMISSION - Lbs/Hr. - E

12.785

9.387