

AP-42 Section 11.6
Reference 63
Report Sect. 4
Reference 76



LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU ALTERNATE FUELS C.

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

2524 S. Sprigg Street, Cape Girardeau, MO 63701
314 335-8878 FAX: 314 335-1119
P.O. Box 968, Cape Girardeau, MO 63702-0968

April 21, 1993

Mr. Tom Lapp
MRI
401 Harrison Oaks Blvd.
Suite 350
Cary, NC 27513

Dear Mr. Lapp:

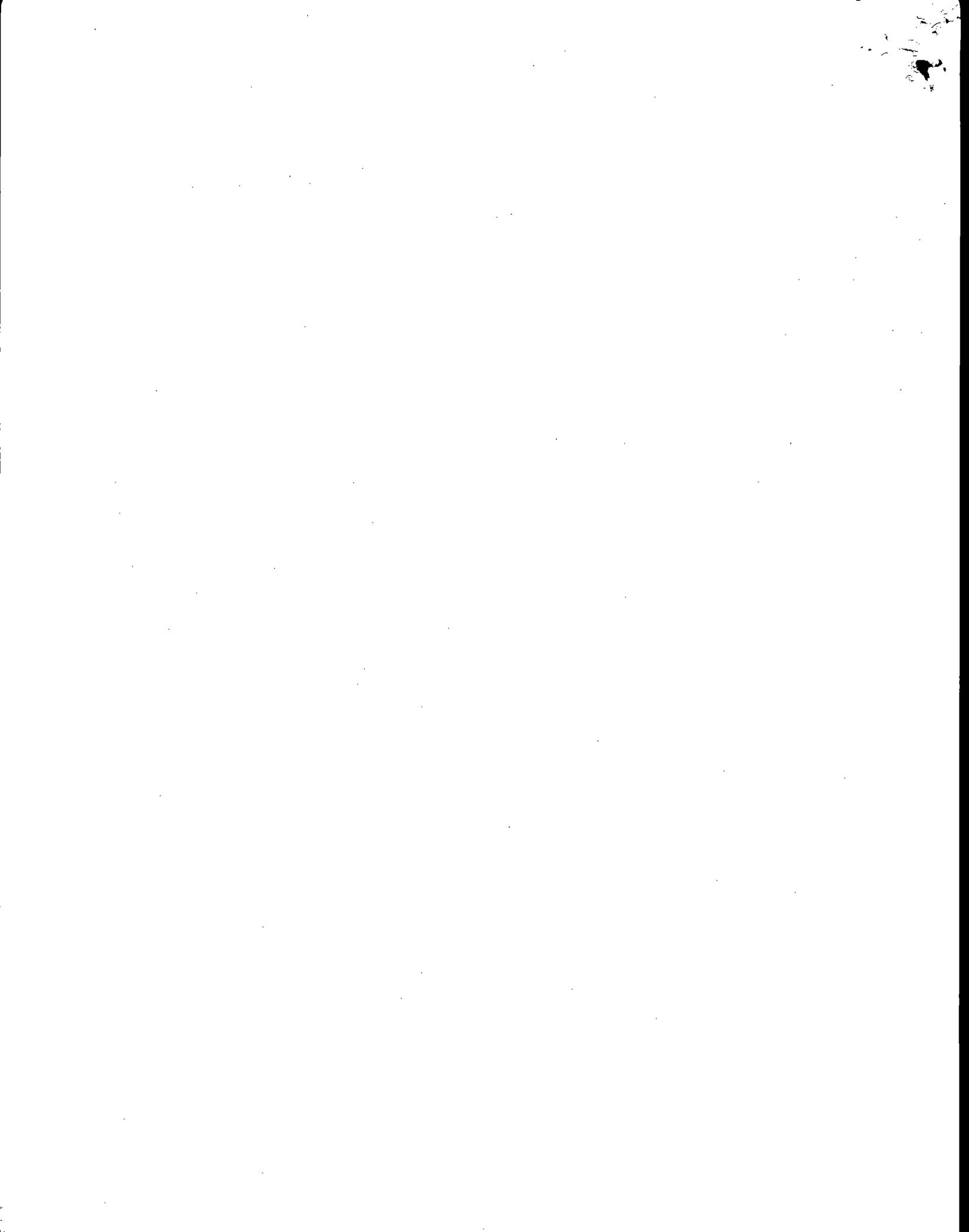
Please find enclosed a copy of the Certification of Compliance testing that Lone Star was required to do under the requirements of the BIF regulations. Prior to this required testing, Lone Star also did background testing to measure certain emissions. Mercury was one of the metals for which testing was conducted. The background testing is identified as "Phase I" throughout this report. This testing was conducted while the kiln was burning conventional fuels. "Phase II" testing was conducted when hazardous waste fuel was being fired in the kiln.

If you need additional information concerning QA/QC procedures, lab analysis, etc., I can supply that information. The entire report is nine volumes in length, and I did not think that you would be interested in the entire report. However, if you need additional data as related to the mercury testing, please let me know.

Sincerely,

Norris Johnson
Facility Manager

cc: Harry Philip



**CERTIFICATION OF COMPLIANCE
STACK EMISSION TEST
PROGRAM AT
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
APRIL & JUNE 1992**

BIF CERTIFICATION OF COMPLIANCE LETTER & FORMS

Revised January 1993

**BIF COC TEST REPORT
& APPENDIX A**

APPENDIX A

- A-1 Particulate/Chlorine/HCl Data Summary/Phase 1
- A-2 Summary of Chloride Mass Balance Data/Phase 1
- A-3 Metals Data Summary/Phase 1
- A-4 Summary of Mass Balance Metals Data/Phase 1
- A-5 VOST Train Worksheet/Phase 1
- A-6 APCC CEM Data Summary/Phase 1
- A-7 Particulate/Chlorine/HCl Data Summary/Phase 2
- A-8 Summary of Chloride Mass Balance Data/Phase 2
- A-9 Metals Data Summary/Phase 2
- A-10 Cr6 Data Summary/Phase 2
- A-11 Mass Balance Metals data/Phase 2
- A-12 VOST Train Worksheet/Phase 2
- A-13 APCC CEM Data Summary/Phase 2

VOLUME 1



LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU ALTERNATE FUELS COMPANY

2524 S. Sprigg Street, Cape Girardeau, MO 63701
314 335-8878 FAX: 314 335-1119
P.O. Box 968, Cape Girardeau, MO 63702-0968

September 24, 1992

Mr. John Smith
U. S. EPA RCRA Branch
726 Minnesota Avenue
Kansas City, KS 66101

RE: EPA I.D. NO. MO 981127319

Dear Mr. Smith,

Please find enclosed the Certificate of Compliance as required for Boilers and Industrial Furnaces burning hazardous waste under the BIF regulations in 40 CFR Part 266. This certification was revised in September and should replace that document date August 17, 1992.

Some revisions to Sections 3.5.2, Phase 2 have been made in order to detail the testing process.

After reviewing analyses of raw mix and waste derived liquid fuel (WDLF) it was ascertained that the digestion method used for sample preparation of these materials was inadequate. Those metals in raw mix and WDLF taken under Tier III guidelines were reanalyzed using the ASTM sample preparation technique, and these analyses for those metals were used in this COC. The QA/QC documentation for the analysis is found in Appendix C, starting with page 1000A.

Also, under this revision, Mercury was considered under Tier IA guidelines, and the appropriate changes to the Precompliance Certification have been made to reflect this change.

Please contact me if further questions or clarification is required.

Sincerely,

Norris Johnson
Facility Manager



LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU ALTERNATE FUELS COMPANY

2524 S. Sprigg Street, Cape Girardeau, MO 63701
314 335-8878 FAX: 314 335-1119
P.O. Box 968, Cape Girardeau, MO 63702-0968

August 17, 1992

Mr. Joe Galbraith
U.S. EPA RCRA Branch
726 Minnesota Avenue
Kansas City, KS 66101

Dear Mr. Galbraith,

Please find enclosed the Certificate of Compliance as required for Boiler and Industrial Furnaces burning hazardous waste under the BIF regulations in 40 CFR part 266.

The document is complete as far as we can ascertain. It should be noted that the CO limit was established after the certification testing upon your verbal approval on August 10, 1992. The CO limit discussion contained herein should be used for the backup for the limitation established for CO.

Much of the laboratory data was very late in arriving. Although, it was checked for accuracy, the shortness of time between receiving all the laboratory data and filing of this document might be a source of error upon closer examination of all the data. If any errors exist we will contact your office immediately.

If you need to communicate with me, I can be reached at address and telephone number listed above.

Sincerely,

Norris Johnson
Facility Manager

cc: Wane Roberts
Jim Burris

COMPLIANCE CERTIFICATION FORM 1 (CC-1)
 GENERAL FACILITY AND TESTING INFORMATION

Initial Certification Revised Certification Recertification

| | |
|---|----------------------------------|
| 1. EPA facility ID Number: | MO 981127319 |
| 2. Facility Name: | LONE STAR ALTERNATE FUELS CO. |
| Contact Person: | NORRIS JOHNSON |
| Telephone Number: | (314) 335-8878 |
| Facility Address: | 2524 SOUTH SPRIGG STREET |
| | CAPE GIRARDEAU, MO 63701 |
| 3. Type of boiler/industrial furnace: | INDUSTRIAL FURNACE (CEMENT KILN) |
| 4. Person responsible for conducting compliance test: (Attach statement of qualifications) | JOHN POWELL |
| Telephone Number: | (203) 871-8557 |
| Company Name: | APCC |
| Address: | 60 INDUSTRIAL PARK ROAD WEST |
| | TOLLAND, CT 06084 |
| 5. Date(s) of compliance test: | JUNE 25-26, 1992 |
| 6. Person responsible for QA/QC: | JOHN SCHNEIDER |
| Title: | SENIOR PROJECT ENGINEER |
| Telephone Number: | (203) 871-8557 |
| Attach a statement certifying that procedures prescribed in QA/QC plan submitted with Compliance Test Notification Form 3 (CTN-3) have been followed, or a description of any changes and an explanation of why changes were necessary. | |

I certify under penalty of law that this information was prepared under my direction or supervision in accordance with a system designed to ensure that qualified personnel properly gathered and evaluated the information and supporting documentation. Copies of all emissions tests, dispersion modeling results, and other information used to determine conformance with the requirements of §266.103(e) are available at the facility, and can be obtained from the facility contact person listed above. Based on my inquiry of the person or persons who manages the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

I also acknowledge that the operating conditions established in this certification pursuant to §266.103(e)(4)(iv) are enforceable limits at which the facility can legally operate during interim status until (1) a revised certification of compliance is submitted or (2) an operating permit is issued.

Signature: Raymond J. Powell Date: 9/28/92

Title: Vice President, Cement Operations

COMPLIANCE CERTIFICATION FORM 2 (CC-2)

DEVIATIONS FROM SUBMITTED NOTIFICATION OF COMPLIANCE TEST

1. Were there any changes in the unit configuration prior to or during testing that would alter any of the information submitted on Form CTN-2 of the unit's Notification of Compliance Test? ___ Yes No

If yes, describe these changes and why they were necessary and attach an amended Form CTN-2 describing the unit as actually tested. (Attach additional sheets if necessary).

2. Were there any changes in the planned test conditions prior to or during testing that alter any of the information submitted on Form CTN-3 of the unit's Notification of Compliance Test? Yes ___ No

If yes, describe these changes and why they were necessary and attach amended Form CTN-3 describing test conditions. (Attach additional sheets if necessary.)

In the initial protocol for testing it was planned to test the kiln while firing 100% hazardous waste fuel and coal, with no tires being used as fuel. However, upon completion of testing using tires, waste fuel, and coal as fuels, it was determined this testing was not needed.

**COMPLIANCE CERTIFICATION FORM 3 (CC-3)
SUMMARY OF COMPLIANCE TEST EMISSIONS**

Complete a separate form for each test condition (if more than 1) under each mode of operation for each unit.

1. Use the same identification codes as on Form CTN-3 for the following:

Unit # 1; Mode (letter) A; Test Condition (1, 2 or N/A)* 1

Brief Description of Mode and Test Condition: Minimum burning zone condition

2. Purpose of Test (e.g., Demonstrate compliance with PM, metals, HCl, and Cl₂ emission limits when firing sludges at maximum feed rate and flue gas flow):

Demonstrates compliance with HCL/CL2, PM and POHC DRE for state while firing hazardous waste feed at maximum rate.

3. Attach a complete copy of QA/QC results for each test.

| 4. Test Results: | Run No. | | | Avg ^b | Allowable Emission Rate ^c | OK ^d |
|-----------------------------------|-----------------------------|---------|---------|------------------|--------------------------------------|-----------------|
| | 1 | 2 | 3 | | | |
| Date (month/day/yr) | 6-25-92 | 6-25-92 | 6-25-92 | | | |
| Time Run Started (hr:min) | 8:30 | 17:45 | 21:45 | | | |
| Total Run Time (mins) | 180 | 180 | 210 | | | |
| Sootblow Time (mins) ^e | | | N/A | | | |
| CO (ppmv @ 7% O ₂) | | | | | | |
| Run Avg | See CO | Limit | | | | |
| Highest 60-min rolling avg | Paper | | | | | |
| HC (ppmv @ 7% O ₂) | | | | | | |
| Run avg | See CO | Limit | | | | |
| Highest 60-min rolling avg | Paper | | | | | |
| PM emissions (gr/dscf) | 0.026 | 0.024 | 0.023 | 0.0243 | 0.032 | |
| HCl emissions (g/hr) | 3577 | 4077 | 6615 | 4756 | 501991.2 | |
| Cl ₂ emissions (g/hr) | 23.4 | 47.1 | 70.1 | 46.9 | 28684.8 | |
| Antimony (g/hr) | Not Measured this condition | | | | | |
| Arsenic (g/hr) | " | " | " | " | " | |
| Barium (g/hr) | " | " | " | " | " | |
| Beryllium (g/hr) | " | " | " | " | " | |
| Cadmium (g/hr) | " | " | " | " | " | |
| Chromium (g/hr) | " | " | " | " | " | |
| Lead (g/hr) | " | " | " | " | " | |
| Mercury (g/hr) | " | " | " | " | " | |
| Silver (g/hr) | " | " | " | " | " | |
| Thallium (g/hr) ^{**} | " | " | " | " | " | |

* If facility conducted tests at only one set of test conditions for the stated mode, enter N/A. If two sets of test conditions were run for the mode, fill out a separate form for each set of test conditions, identifying the test condition (1 or 2) as on Form CTN-3.

^b If soot blowing or other daily activity that increases the PM emission rate was incorporated into the testing, calculate average using equation provided in instructions.

^c Allowable levels are the same as indicated on Form PC-4.

^d Check if each non-sootblowing run and average are less than or equal to allowable.

^e Indicate sootblowing time or time of other activity that was incorporated into the testing.

**COMPLIANCE CERTIFICATION FORM 3 (CC-3)
SUMMARY OF COMPLIANCE TEST EMISSIONS**

Complete a separate form for each test condition (if more than 1) under each mode of operation for each unit.

1. Use the same identification codes as on Form CTN-3 for the following:

Unit # 1; Mode (letter) A; Test Condition (1, 2 or N/A) 2

Brief Description of Mode and Test Condition: Maximum Burning Zone Temperature

2. Purpose of Test (e.g., Demonstrate compliance with PM, metals, HCl, and Cl₂ emission limits when firing sludges at maximum feed rate and flue gas flow):

Comply with metal emissions, maximum APCD temperatures, maximum hazardous waste feed rate, maximum production

3. Attach a complete copy of QA/QC results for each test.

| 4. Test Results: | Run No. | | | Avg ^b | Allowable Emission Rate ^c | OK ^d |
|-----------------------------------|-------------------------|---------|---------|------------------|--------------------------------------|-----------------|
| | 1 | 2 | 3 | | | |
| Date (month/day/yr) | 6-26-92 | 6-26-92 | 6-26-92 | | | |
| Time Run Started (hr:min) | 13:45 | 17:45 | 21:45 | | | |
| Total Run Time (mins) | 180 | 180 | 180 | | | |
| Sootblow Time (mins) ^e | | | N/A | | | |
| CO (ppmv @ 7% O ₂) | | | | | | |
| Run Avg | See CO | limit | | | | |
| Highest 60-min rolling avg | Paper | | | | | |
| HC (ppmv @ 7% O ₂) | | | | | | |
| Run avg | See CO | Limit | | | | |
| Highest 60-min rolling avg | Paper | | | | | |
| PM emissions (gr/dscf) | Not measured condition? | | | | | |
| HCl emissions (g/hr) | " | " | " | " | | |
| Cl ₂ emissions (g/hr) | " | " | " | " | | |
| Antimony (g/hr) | Tier I | | | | 21513.94 | |
| Arsenic (g/hr) | 0.64 | 1.03 | 0.97 | 0.88 | 164.97 | |
| Barium (g/hr) | Tier I | | | | 3585657.4 | |
| Beryllium (g/hr) | 0.02 | 0.02 | 0.07 | 0.037 | 301.20 | |
| Cadmium (g/hr) | 0.82 | 7.19 | 0.02 | 2.68 | 401.59 | |
| Chromium (g/hr) | 5.47 | 0.02 | 0.02 | 1.84 | 71713147.41 | |
| Lead (g/hr) | 6.34 | 5.64 | 12.94 | 8.31 | 6454.18 | |
| Mercury (g/hr) | 18.11 | 16.42 | 58.14 | 30.89 | 21513.94 | |
| Silver (g/hr) | Tier I | | | | 215139.44 | |
| Thallium (g/hr) | Tier I | | | | 35856.57 | |

^a If facility conducted tests at only one set of test conditions for the stated mode, enter N/A. If two sets of test conditions were run for the mode, fill out a separate form for each set of test conditions, identifying the test condition (1 or 2) as on Form CTN-3.

^b If soot blowing or other daily activity that increases the PM emission rate was incorporated into the testing, calculate average using equation provided in instructions.

^c Allowable levels are the same as indicated on Form PC-4.

^d Check if each non-sootblowing run and average are less than or equal to allowable.

^e Indicate sootblowing time or time of other activity that was incorporated into the testing.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 3; Test Date: 6-25-92
2. Run Start Time (hr:min): 8:30; Run End Time (hr:min): 12:30
- If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg ^a |
|---|--------------------------|-------------------------|
| Max. Production Rate (specify units) | 245.4 | 256.2 |
| Max. PM Control Device Inlet Temp. (*F) ^b | Not measured condition 1 | |
| Max. Combustion Chamber Temp. (*F) ^b | " | " |
| APCS Operating Parameters (List applicable parameters, see §266.103(c)(1)(i)-(iii)) | Run Avg | 60-min Avg ^a |
| | Not measured condition 1 | |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|--------------------------|------------|-----------|----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | Nonpump HW | RM | Fuel |
| Mass Feed Rate (g/hr) | 9.28E+06 | 3.90E+05 | 2.13E+08 | 1.08E+07 |
| Thermal Feed Rate (Btu/hr) | 2.3E+08 | 3.06E+06 | 0 | 2.65E+08 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 447,068.2 | 453.6 | 95,754.96 | 11,793.6 |
| Antimony (g/hr) | Not measured condition 1 | | | |
| Arsenic (g/hr) | | | | |
| Barium (g/hr) | | | | |
| Beryllium (g/hr) | | | | |
| Cadmium (g/hr) | | | | |
| Chromium (g/hr) | | | | |
| Lead (g/hr) | | | | |
| Mercury(g/hr) | | | | |
| Silver (g/hr) | | | | |
| Thallium (g/hr) | | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.

^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.

^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.

^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.

^eCopy form and add additional pages if more than four streams were fed during test.

^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4) SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 3; Test Date: 6-25-92
2. Run Start Time (hr:min): 8:30; Run End Time (hr:min): 12:30
If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg. | 60-min Avg. ^a |
|---|--------------|--------------------------|
| Max. Production Rate (specify units) | 245.4 | 256.2 |
| Max. PM Control Device Inlet Temp. (°F) ^b | Not measured | Condition 1 |
| Max. Combustion Chamber Temp. (°F) ^b | - | - |
| | Run Avg. | 60-min Avg. ^a |
| APCS Operating Parameters (List applicable parameters, see §266.103(c)(1)(ix-xiii)) | Not measured | Condition 1 |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|--------------------------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | Tires | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Fuel | | | |
| Mass Feed Rate (g/hr) | 1.36E ⁶ | | | |
| Thermal Feed Rate (Btu/hr) | 4.27E ⁷ | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 1496.88 | | | |
| Antimony (g/hr) | Not measured condition 1 | | | |
| Arsenic (g/hr) | | | | |
| Barium (g/hr) | | | | |
| Beryllium (g/hr) | | | | |
| Cadmium (g/hr) | | | | |
| Chromium (g/hr) | | | | |
| Lead (g/hr) | | | | |
| Mercury (g/hr) - | | | | |
| Silver (g/hr) | | | | |
| Thallium (g/hr) | | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 4; Test Date: 6-25-92
2. Run Start Time (hr:min): 17:45; Run End Time (hr:min): 20:45

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg ^a |
|--|--------------|-------------------------|
| Max. Production Rate (specify units) | 248.1 | 255.92 |
| Max. PM Control Device Inlet Temp. (°F) ^b | NOT measured | condition 1 |
| Max. Combustion Chamber Temp. (°F) ^b | " | " |
| APCS Operating Parameters (List applicable parameters; see §266.103(c)(1)(i-xiii)) | Run Avg | 60-min Avg ^a |
| | Not measured | condition 1 |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|-----------|-----------|-------------|----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | NonpumpHW | R.M. | Fuel |
| Mass Feed Rate (g/hr) | 9.09E+06 | 4.53E+05 | 2.20E+08 | 1.10E+07 |
| Thermal Feed Rate (Btu/hr) | 2.23E+08 | 4.75E+06 | 0 | 2.65E+08 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 422185.48 | 907.2 | 107773.36 | 9843.12 |
| Antimony (g/hr) | Not | measured | condition 1 | |
| Arsenic (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Barium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Beryllium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Cadmium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Chromium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Lead (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Mercury (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Silver (g/hr) | | | | |
| Thallium (g/hr) | | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 4; Test Date: 6-25-92
2. Run Start Time (hr:min): 17:45; Run End Time (hr:min): 20:45

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg. | 60-min Avg. ^a |
|---|--------------|--------------------------|
| Max. Production Rate (specify units) | 248.1 | 255.92 |
| Max. PM Control Device Inlet Temp. (*F) ^b | Not Measured | Condition 1 |
| Max. Combustion Chamber Temp. (*F) ^b | " | " |
| APCS Operating Parameters (List applicable parameters; see §266.103(c)(1)(iv-xiii)) | Run Avg. | 60-min Avg. |
| | Not Measured | Condition 1 |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|--------------------------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | Tires | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Fuel | | | |
| Mass Feed Rate (g/hr) | 1.36E ⁺⁶ | | | |
| Thermal Feed Rate (Btu/hr) | 4.51E ⁺⁷ | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 1360.8 | | | |
| Antimony (g/hr) | Not Measured Condition 1 | | | |
| Arsenic (g/hr) | ↓ | | | |
| Barium (g/hr) | | | | |
| Beryllium (g/hr) | | | | |
| Cadmium (g/hr) | | | | |
| Chromium (g/hr) | | | | |
| Lead (g/hr) | | | | |
| Mercury (g/hr) | | | | |
| Silver (g/hr) | | | | |
| Thallium (g/hr) | | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 5; Test Date: 6-25-92
2. Run Start Time (hr:min): 21:45; Run End Time (hr:min): 1:05

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg. | 60-min Avg. ^a |
|---|--------------|--------------------------|
| Max. Production Rate (specify units) | 247.4 | 255.9 |
| Max. PM Control Device Inlet Temp. (°F) ^b | Not measured | Condition 1 |
| Max. Combustion Chamber Temp. (°F) ^b | " | " |
| APCS Operating Parameters (List applicable parameters; see §266.103(c)(1)(i)-(iii)) | Run Avg. | 60-min Avg. |
| | Not measured | Condition 1 |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|--------------|------------|-------------|----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | Nonpump HW | R.M. | Fuel |
| Mass Feed Rate (g/hr) | 9.11E+06 | 4.12E+05 | 2.19E+08 | 1.06E+07 |
| Thermal Feed Rate (Btu/hr) | 2.41E+08 | 5.84E+05 | 0 | 2.52E+08 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 416813.04 | 997.92 | 111494.88 | 8436.96 |
| Antimony (g/hr) | Not measured | | condition 1 | |
| Arsenic (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Barium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Beryllium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Cadmium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Chromium (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Lead (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Mercury (g/hr) ^g | ↓ | ↓ | ↓ | ↓ |
| Silver (g/hr) | ↓ | ↓ | ↓ | ↓ |
| Thallium (g/hr) | ↓ | ↓ | ↓ | ↓ |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 1;
Run No.: 5; Test Date: 6-25-92
2. Run Start Time (hr:min): 21:45; Run End Time (hr:min): 1:05

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg ^a |
|---|--------------|-------------------------|
| Max. Production Rate (specify units) | 247.4 | 255.9 |
| Max. PM Control Device Inlet Temp. (°F) ^b | Not Measured | Condition 1 |
| Max. Combustion Chamber Temp. (°F) ^b | " | " |
| APCS Operating Parameters (List applicable parameters see §266.103(c)(1)(i-xiii)) | Run Avg | 60-min Avg ^a |
| | Not Measured | Condition 1 |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. ^e | 1 | 2 | 3 | 4 |
|--|--------------------------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | Tires | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Fuel | | | |
| Mass Feed Rate (g/hr) | 1.36E ⁺ 6 | | | |
| Thermal Feed Rate (Btu/hr) | 4.21E ⁺ 7 | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 1905.12 | | | |
| Antimony (g/hr) | Not Measured Condition 1 | | | |
| Arsenic (g/hr) | | | | |
| Barium (g/hr) | | | | |
| Beryllium (g/hr) | | | | |
| Cadmium (g/hr) | | | | |
| Chromium (g/hr) | | | | |
| Lead (g/hr) | | | | |
| Mercury (g/hr) | | | | |
| Silver (g/hr) | | | | |
| Thallium (g/hr) | | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 5 (CC-5)
 SUMMARY OF OPERATING AND FEED RATE LIMITS FOR A SPECIFIC MODE

1. Unit #: 1; Mode: A-1; Run Nos.: 3-5; Test Date: 6-25-92

2. Operating Condition Limits^a

| | | |
|---|---|-----------------------------|
| Max. PM Control Device Inlet Temp. (°F) ^a | * | * Not determined |
| Max. Combustion Chamber Temp. (°F) ^a | * | * Not determined |
| APCS Operating Conditions (list applicable parameters, see § 266.103(c)(1)(ix-xiii)): | | |
| Low pressure drop Main APCD | | -6" WC manufacturers design |
| Low pressure drop Bypass APCD | | -2.95" WC |
| Max. Production Rate (specify units) | | 256 TPH |
| Max. Total HW Feed Rate (g/hr) | | 9328919 |
| Max. Total Pumpable HW Feed Rate (g/hr) ^b | | 9328919 |
| Max. Total Chlorine and Chloride Feed Rate (g/hr) | | 553044.24 |
| Max. Total Ash Feed Rate (g/hr) ^d | | N/A |

3. Maximum Metals Feed Rates

| | Total Feed Streams ^a | Total HW Feed Streams ^b | Total Pumpable HW Feed Streams ^c |
|--------------------|---------------------------------|------------------------------------|---|
| Antimony (g/hr) * | Not determined | this | condition |
| Arsenic (g/hr) * | " | " | " |
| Barium (g/hr) * | " | " | " |
| Beryllium (g/hr) * | " | " | " |
| Cadmium (g/hr) * | " | " | " |
| Chromium (g/hr) * | " | " | " |
| Lead (g/hr) * | " | " | " |
| Mercury (g/hr) * | " | " | " |
| Silver (g/hr) * | " | " | " |
| Thallium (g/hr) * | " | " | " |

4. CO, HC, and PM Limits

| | |
|--|--------------------------------|
| CO (ppmv @ 7% O ₂) ^{f,h} | 1169.7 See CO limit discussion |
| HC (ppmv as propane @ 7% O ₂) ^{e,h} | 20.0 " " " " |
| PM (gr/dscf @ 7% O ₂) ⁱ | 0.032 " " " " |

^a Asterisk any parameter not determined under the primary test conditions.
^b Not applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.
^c If applicable, attach documentation that the increased cancer risk to the MEL from emissions of dioxins and furans is not greater than 1 in 100,000.
^d Not required for cement and light-weight aggregate kilns.
^e Not required for furnaces monitoring metals concentrations in collected PM.
^f If under Tier I, CO limit is 100 ppmv. If under Tier II, limit is the average over all runs of the HHA CO level for each run.
^g If under Tier I, HC limit is not applicable. If under Tier II, limit is 20 ppmv.
^h If a furnace cannot meet the Tier II 20 ppmv HC limit because of organic matter in raw material feedstocks, the interim HC and CO limits are the baseline limits proposed in the Part B permit application or the limits established by the Director as a condition of a time extension for certification of compliance.
ⁱ 0.08 gr/dscf or existing permit, whichever is more stringent.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3.

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 2;
Run No.: 7; Test Date: 6-26-92
2. Run Start Time (hr:min): 13:45; Run End Time (hr:min): 16:45

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg |
|---|--------------|--------------|
| Max. Production Rate (specify units) | 251.1 TPH | 256.2 TPH |
| Max. PM Control Device Inlet Temp. (*F) | 310°F 428°F | 365°F 434°F |
| Max. Combustion Chamber Temp. (*F) | 1669.3 | 1688 |
| APCS Operating Parameters (List applicable parameters, see §266.103(c)(3)(i)-(iii)) | Run Avg | 60-min Avg |
| Pressure Drop Main APCD*/Bypass APCD | 6"wc 3.08"wc | 6"wc 2.96"wc |
| *Manufacturers specifications | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. | 1 | 2 | 3 | 4 |
|--|----------|------------|----------|----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | Nonpump HW | R. M. | Fuel |
| Mass Feed Rate (g/hr) | 9.27E+06 | 1.24E+05 | 2.28E+08 | 1.11E+07 |
| Thermal Feed Rate (Btu/hr) | 2.3E+08 | 1.9E+06 | 0 | 2.74E+08 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 4.21E+08 | 226.8 | 118,343 | 121.57 |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 1854.52 | 1.02 | 173.98 | 60.70 |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 22.25 | 0.02 | 117.73 | 3.68 |
| Cadmium (g/hr) | 2679.75 | 0.16 | 799.32 | 2.63 |
| Chromium (g/hr) | 6500.48 | 25.28 | 4258.48 | 184.49 |
| Lead (g/hr) | 5517.14 | 8.12 | 2024.49 | 70.02 |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.

^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.

^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.

^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.

^eCopy form and add additional pages if more than four streams were fed during test.

^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3:

1. Unit #: 1; Modc: A; Test Condition (1, 2, or N/A): 2
Run No.: 7; Test Date: 6-26-92
2. Run Start Time (hr:min): 13:45; Run End Time (hr:min): 16:45
If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg |
|---|--------------|--------------|
| Max. Production Rate (specify units) | 251.1 TPH | 256.2 TPH |
| Max. PM Control Device Inlet Temp. (*F) | 310°F 428°F | 365°F 434°F |
| Max. Combustion Chamber Temp. (*F) | 1669.4 | 1688 |
| APCS Operating Parameters (list applicable parameters per 261.03(c)(3)(ii)) | Run Avg | 60-min Avg |
| Pressure drop main APCD*/Bypass APCD | 6"wc 3.08"wc | 6"wc 2.96"wc |
| *used manufacturers specifications | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^c

| Stream No. | 1 | 2 | 3 | 4 |
|--|----------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | TIRES | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | FUEL | | | |
| Mass Feed Rate (g/hr) | 1.36E+06 | | | |
| Thermal Feed Rate (Btu/hr) | 4.42E+07 | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 0.00 | | | |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 1.31 | | | |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 0.07 | | | |
| Cadmium (g/hr) | 2.48 | | | |
| Chromium (g/hr) | 6.58 | | | |
| Lead (g/hr) | 14.71 | | | |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.

^bNot applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.

^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.

^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.

^eCopy form and add additional pages if more than four streams were fed during test.

^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3:

1. Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 2;
Run No.: 8; Test Date: 6-26-92
2. Run Start Time (hr:min): 17:45; Run End Time (hr:min): 20:45
If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Ave. | 60-min. Ave. |
|--|--------------|--------------|
| Max. Production Rate (specify units) | 250.7 TPH | 255.6 TPH |
| Max. PM Control Device Inlet Temp. (°F) | 310°F 430°F | 366°F 436°F |
| Max. Combustion Chamber Temp. (°F) | 1677°F | 1699.6°F |
| APCS Operating Parameters (list applicable parameters, see §260.103(c)(1)(viii)) | Run Ave. | 60-min. Ave. |
| P MAIN APCD BYPASS APCD | 6"wc 3.05"wc | 6"wc 2.99"wc |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. | 1 | 2 | 3 | 4 |
|--|------------|------------|------------|-----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | Nonpump HW | R.M. | Fuel |
| Mass Feed Rate (g/hr) | 9.43E+06 | 1.24E+05 | 2.28E+08 | 1.14E+07 |
| Thermal Feed Rate (Btu/hr) | 2.30E+08 | 1.52E+06 | 0 | 2.78E+09 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 365,011.92 | 181.44 | 132,133.60 | 11,285.26 |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 1744.47 | 0.83 | 326.04 | 44.94 |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 22.82 | 0.03 | 138.62 | 6.60 |
| Cadmium (g/hr) | 2860.28 | 0.26 | 362.51 | 1.99 |
| Chromium (g/hr) | 6530.61 | 23.18 | 4651.18 | 178.62 |
| Lead (g/hr) | 6064.61 | 6.77 | 3328.78 | 63.60 |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.

^bNot applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.

^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.

^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in non-hazardous waste feed streams.

^eCopy form and add additional pages if more than four streams were fed during test.

^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3:

- Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 2;
Run No.: 8; Test Date: 6-26-92
- Run Start Time (hr:min): 17:45; Run End Time (hr:min): 20:45
If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Ave | 60-min Ave |
|---|--------------|--------------|
| Max. Production Rate (specify units) | 250.7 TPH | 255.6 TPH |
| Max. PM Control Device Inlet Temp. (°F) | 310°F 430°F | 366°F 436°F |
| Max. Combustion Chamber Temp. (°F) | 1677°F | 1699.6°F |
| APCS Operating Parameters (list applicable parameters): 5256, 103(6), 103(7), 103(8) | | |
| | Run Ave | 60-min Ave |
| P MAIN APCD BYPASS APCD | 6"wc 3.05"wc | 6"wc 2.99"wc |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. | 1 | 2 | 3 | 4 |
|--|----------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | TIRES | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | FUEL | | | |
| Mass Feed Rate (g/hr) | 1.36E+06 | | | |
| Thermal Feed Rate (Btu/hr) | 4.31E+07 | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 2585.52 | | | |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 4.98 | | | |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 0.11 | | | |
| Cadmium (g/hr) | 22.61 | | | |
| Chromium (g/hr) | 77.36 | | | |
| Lead (g/hr) | 42.49 | | | |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.

^bNot applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.

^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.

^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.

^eCopy form and add additional pages if more than four streams were fed during test.

^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4) SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3:

- Unit #: 1; Mode: A; Test Condition (1, 2, or N/A): 2
Run No.: 9; Test Date: 6-26-92
- Run Start Time (hr:min): 21:30; Run End Time (hr:min): 00:30
If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | | 60-min Avg | |
|---|---------|---------|------------|--------|
| Max. Production Rate (specify units) | 251 TPH | | 256 TPH | |
| Max. PM Control Device Inlet Temp. (°F) | 309°F | 433°F | 367°F | 438°F |
| Max. Combustion Chamber Temp. (°F) | 1666.1 | | 1685.8 | |
| APCS Operating Parameters (List applicable parameters, e.g. 525.103 (c) (3) (i) (ii)) | Run Avg | | 60-min Avg | |
| Pressure drop main APCD*/Bypass APCD | 6"wc | 2.97"wc | 6"wc | 2.89wc |
| | | | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:⁴

| Stream No. | 1 | 2 | 3 | 4 |
|--|-----------|------------|-----------|----------|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | WDLF | WDSF | RAW MIX | COAL |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | Pump HW | Nonpump HW | R.M. | Fuel |
| Mass Feed Rate (g/hr) | 9.43E+06 | 1.81E+05 | 2.28E+08 | 1.08E+07 |
| Thermal Feed Rate (Btu/hr) | 2.37E+08 | 2.1E+06 | 0 | 2.66E+08 |
| Ash Feed Rate (g/hr) ^f | N/A | N/A | N/A | N/A |
| Chlorine and Chloride (g/hr) | 477731.52 | 498.96 | 118434.96 | 11,793.6 |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 1584.47 | 2.75 | 171.91 | 34.29 |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 24.43 | 0.05 | 122.21 | 2.73 |
| Cadmium (g/hr) | 2831.25 | 0.45 | 303.24 | 2.60 |
| Chromium (g/hr) | 6380.80 | 50.05 | 3853.18 | 219.31 |
| Lead (g/hr) | 6157.42 | 10.97 | 2621.99 | 42.57 |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

¹Indicate highest or lowest 60-minute rolling average as appropriate.
²Not applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.
³Indicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
⁴Owners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
⁵Copy form and add additional pages if more than four streams were fed during test.
⁶Owners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 4 (CC-4)
SUMMARY OF COMPLIANCE TEST OPERATING CONDITIONS

Complete a separate form for each run of a specified test condition, use same identification codes as on Forms CC-3 and CTN-3:

1. Unit #: 1; Mode: B; Test Condition (1, 2, or N/A): 2
Run No.: 9; Test Date: 6-26-92
2. Run Start Time (hr:min): 21:30; Run End Time (hr:min): 00:30

If there were any interruptions in sampling, discuss cause, duration, and impact on sampling: _____

3. Operating Conditions:

| | Run Avg | 60-min Avg |
|---|--------------|-------------|
| Max. Production Rate (specify units) | 251 TPH | 256 TPH |
| Max. PM Control Device Inlet Temp. (°F) | 309°F 433°F | 337°F 438°F |
| Max. Combustion Chamber Temp. (°F) | 1666.1 | 1685.8 |
| APCS Operating Parameters (List applicable parameters, e.g., 526, 103, (g)(l)(x)(m)): | Run Avg | 60-min Avg |
| Pressure drop main APCD*/Bypass APCD | 6"wc 2.97"wc | 6"wc 2.89wc |
| | | |
| | | |

4. Description of All Fuel, Raw Material, and Waste Feed Streams:^d

| Stream No. | 1 | 2 | 3 | 4 |
|--|----------|---|---|---|
| Stream Type (e.g., coal, shale, sludge, liquid solvents, etc.) | TIRES | | | |
| Category (e.g., Fuel, Raw Material, Pumpable HW, Nonpumpable HW) | FUEL | | | |
| Mass Feed Rate (g/hr) | 1.36E+06 | | | |
| Thermal Feed Rate (Btu/hr) | 4.23E+07 | | | |
| Ash Feed Rate (g/hr) ^f | N/A | | | |
| Chlorine and Chloride (g/hr) | 3,674.16 | | | |
| Antimony (g/hr) | Tier IA | | | |
| Arsenic (g/hr) | 1.46 | | | |
| Barium (g/hr) | Tier IA | | | |
| Beryllium (g/hr) | 0.13 | | | |
| Cadmium (g/hr) | 47.81 | | | |
| Chromium (g/hr) | 135.93 | | | |
| Lead (g/hr) | 35.14 | | | |
| Mercury (g/hr) | Tier IA | | | |
| Silver (g/hr) | Tier IA | | | |
| Thallium (g/hr) | Tier IA | | | |

^aIndicate highest or lowest 60-minute rolling average as appropriate.
^bNot applicable if complying with Tier 1 or adjusted Tier 1 metals feed rate screening limits.
^cIndicate highest 60-minute rolling averages for maximum flue gas flow rate and, if chosen, maximum suspended solids content of scrubber water where applicable. Indicate lowest 60-minute averages for all other APCS parameters.
^dOwners/operators of furnaces monitoring metals concentrations in collected PM are not required to determine metals feed rates in nonhazardous waste feed streams.
^eCopy form and add additional pages if more than four streams were fed during test.
^fOwners/operators of cement and light-weight aggregate kilns are not required to determine ash feed rates of feed streams.

COMPLIANCE CERTIFICATION FORM 5 (CC-5)
 SUMMARY OF OPERATING AND FEED RATE LIMITS FOR A SPECIFIC MODE.

1. Unit #: 1; Mode: A-2; Run Nos.: 7-9; Test Date: 7-26-92
 2. Operating Condition Limits^a

| | |
|---|-------------------------------------|
| Max. PM Control Device Inlet Temp. (°F) ^a | 366°F and 436°F |
| Max. Combustion Chamber Temp. (°F) ^a | 1691°F |
| APCS Operating Conditions (list applicable parameters, see § 266.103(c)(1)(ix-xiii)): | *Not determined this test condition |
| Max. Production Rate (specify units) | 256 TPH |
| Max. Total HW Feed Rate (g/hr) | 9571322.88 |
| Max. Total Pumpable HW Feed Rate (g/hr) ^b | 9571322.88 |
| Max. Total Chlorine and Chloride Feed Rate (g/hr) | Not determined this condition |
| Max. Total Ash Feed Rate (g/hr) ^d | N/A |

3. Maximum Metals Feed Rates

| | Total Feed Streams ^a | Total HW Feed Streams ^b | Total Pumpable HW Feed Streams |
|------------------|---------------------------------|------------------------------------|--------------------------------|
| Antimony (g/hr) | Tier IA | | |
| Arsenic (g/hr) | 2002.63 | 1729.35 | 1727.82 |
| Barium (g/hr) | Tier IA | | |
| Beryllium (g/hr) | 153.93 | 23.20 | 23.17 |
| Cadmium (g/hr) | 3305.81 | 2790.71 | 2717.09 |
| Chromium (g/hr) | 11029.72 | 6503.47 | 5993.49 |
| Lead (g/hr) | 8669.84 | 5921.67 | 5812.01 |
| Mercury (g/hr) | Tier IA | | |
| Silver (g/hr) | Tier IA | | |
| Thallium (g/hr) | Tier IA | | |

4. CO, HC, and PM Limits

| | |
|--|--------------------------------|
| CO (ppmv @ 7% O ₂) ^{c,d} | 1169.7 See CO limit discussion |
| HC (ppmv as propane @ 7% O ₂) ^{e,f,g} | 20.0 See CO limit discussion |
| PM (gr/dscf @ 7% O ₂) ⁱ | 0.032 See CO limit discussion |

^a Asterisk any parameter not determined under the primary test conditions.

^b Not applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.

^c If applicable, attach documentation that the increased cancer risk to the MFL from emissions of dioxins and furans is not greater than 1 in 100,000.

^d Not required for cement and light-weight aggregate kilns.

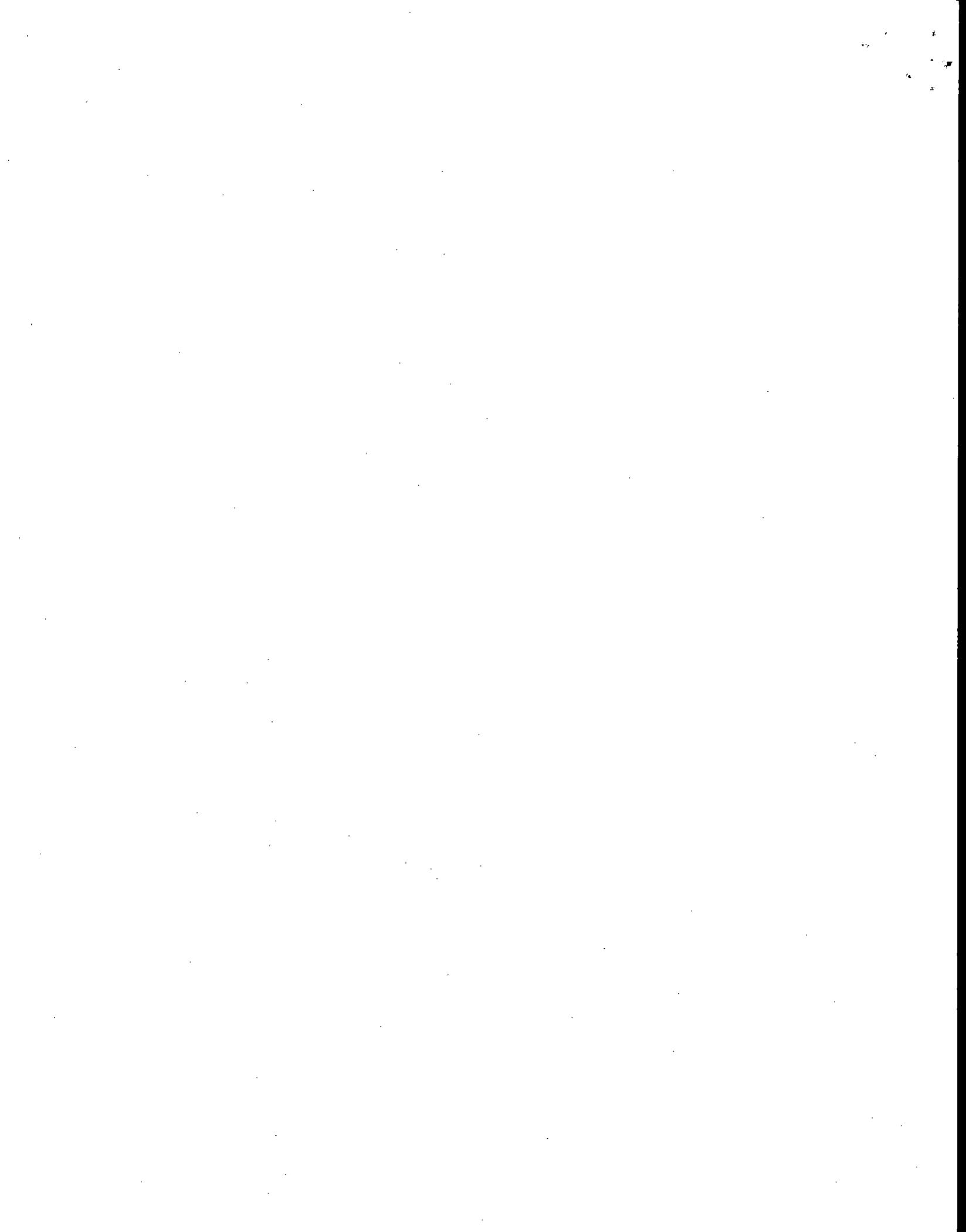
^e Not required for furnaces monitoring metals concentrations in collected PM.

^f If under Tier I, CO limit is 100 ppmv. If under Tier II, limit is the average over all runs of the MHA CO level for each run.

^g If under Tier I, HC limit is not applicable. If under Tier II, limit is 20 ppmv.

^h If a furnace cannot meet the Tier II 20 ppmv HC limit because of organic matter in raw material feedstocks, the interim HC and CO limits are the baseline limits proposed in the Part B permit application or the limits established by the Director as a condition of a time extension for certification of compliance.

ⁱ 0.08 gr/dscf or existing permit, whichever is more stringent.



COMPLIANCE TEST NOTIFICATION FORM 1 (CTN-1)
 GENERAL FACILITY AND PLANNED TESTING INFORMATION

Initial Certification Revised Certification Recertification

| | |
|--|--------------------------------------|
| 1. EPA facility ID Number: | MO 981127319 |
| 2. Facility Name: | LONE STAR ALTERNATE FUELS CO. |
| Contact Person: | NORRIS JOHNSON |
| Telephone Number: | (314) 335-8878 |
| Facility Address: | 2524 South Sprigg Street |
| | Cape Girardeau, Missouri 63701 |
| 3. List all hazardous waste combustors at facility by type (boiler, industrial furnace, incinerator); if more than 3 units, list additional units at bottom of page. | #1: Industrial Furnace (Cement Kiln) |
| | #2: |
| | #3: |
| 4. Person responsible for conducting compliance test: (Attach statement of qualifications) | JOHN POWELL |
| Telephone Number: | (203) 871-8557 |
| Company Name: | APCC |
| Address: | 60 Industrial Park Road West |
| | Tolland, CT 06084 |
| 5. Planned date(s) of compliance test: | June 22-26 |

Signature: Norris Johnson Date: 8-15-92
 Title: Manager Alternate Fuel Co, Lone Star Fuel, Inc

COMPLIANCE TEST NOTIFICATION FORM 2 (CTN-2):

UNIT DESCRIPTION Unit # ____ (see Form CTN-1, Block 3)

Complete a separate form for each unit. Attach additional sheets if necessary.

1. Type and Size of Boiler or Industrial Furnace (e.g., 100 million Btu/hr natural gas-fired boiler with four front-wall burners, 100 ton/hr wet process cement kiln): _____
160 Ton/hr Precalciner Cement Kiln

2. Attach (a) scaled plot plan showing entire facility and location of this unit and (b) schematic drawing showing combustor; fuel, feedstock, and waste feed systems; air pollution control devices; continuous emission monitoring systems; and stack. Drawing should clearly indicate location and design capacities (kg/hr) of all feed systems, and location of all continuously monitored parameter sampling points.

3. Description of air pollution control devices (e.g., 3-field ESP with design PM emissions of 0.03 gr/dscf): Fabric Filter Baghouse with reverse air cleaning

Is APCD Shared with other device(s) or Unique (circle correct answer); if shared, will other device(s) be in use during the test? Yes No

4. List of installed continuous emission monitors:

x Carbon Monoxide; x Oxygen; x Hydrocarbons;

Description of hydrocarbon monitor:

x Heated system; minimum CEM system temperature (°C): 148°C

 Unheated system; minimum CEM system temperature (°C): _____

If not using a heated system, explain why and briefly describe sample gas conditioning system: _____

5. Description of Stack:

Shared with other device(s) or Unique (circle correct answer); if shared, will other device(s) be in use during the test? x Yes No

6. Other information useful to understanding unit design or operation (Note: if it is expected that a conflict between parameters will arise, such that more than one test condition under a given mode is needed in order to determine a parameter, indicate the parameter and the reason for conflict): Kiln APCD is shared with the mill used to grind raw material

COMPLIANCE TEST NOTIFICATION FORM 2 (CTN-2):

UNIT DESCRIPTION Unit # _____ (see Form CTN-1, Block 3)

Complete a separate form for each unit. Attach additional sheets if necessary.

1. Type and Size of Boiler or Industrial Furnace (e.g., 100 million Btu/hr natural gas-fired boiler with four front-wall burners, 100 ton/hr wet process cement kiln): _____

160 Ton/hr Precalciner Cement Kiln

2. Attach (a) scaled plot plan showing entire facility and location of this unit and (b) schematic drawing showing combustor; fuel, feedstock, and waste feed systems; air pollution control devices; continuous emission monitoring systems; and stack.

Drawing should clearly indicate location and design capacities (kg/hr) of all feed systems, and location of all continuously monitored parameter sampling points.

3. Description of air pollution control devices (e.g., 3-field ESP with design PM emissions of 0.03 gr/dscf): Fabric Filter Baghouse with reverse

air cleaning

Is APCD Shared with other device(s) or Unique (circle correct answer); if shared, will other device(s) be in use during the test? Yes No

4. List of installed continuous emission monitors:

X Carbon Monoxide; X Oxygen; X Hydrocarbons;

Description of hydrocarbon monitor:

X Heated system; minimum CEM system temperature (°C): 148°C

 Unheated system; minimum CEM system temperature (°C): _____

If not using a heated system, explain why and briefly describe sample gas conditioning system: _____

5. Description of Stack:

Shared with other device(s) or Unique (circle correct answer); if shared, will other device(s) be in use during the test? X Yes No

6. Other information useful to understanding unit design or operation (Note: if it is expected that a conflict between parameters will arise, such that more than one test condition under a given mode is needed in order to determine a parameter, indicate the parameter and the reason for conflict): Kiln APCD is shared with

the mill used to grind raw material

COMPLIANCE TEST NOTIFICATION FORM 3 (CTN-3)
DESCRIPTION OF PLANNED TESTING

Complete a separate form for each test condition (if more than 1) under each mode of operation for each unit.

1. Unit # 1; Mode (letter) A; Test Condition (1, 2, or N/A)* 1

Brief Description of Mode and Test Condition: Minimum burning zone temperature

2. Purpose of Test (e.g., to demonstrate compliance with PM, metals, HCl, and Cl₂ emission limits when firing sludges at maximum feed rate and flue gas flow):

Carbon dioxide limit, particulate matter, HCl and Cl₂ emission limits

3. Attach a complete copy of QA/QC Plan and test protocol.

4. Planned Operating Conditions:

| | |
|--|---|
| Max. Production Rate (specify units) | 255 TPH |
| Max. PM Control Device Inlet Temp. (°F) ^b | 435°F |
| Max. Combustion Chamber Temp. (°F) | 2800°F |
| APCS Operating Conditions (list applicable parameters, see § 266.103(e)(1)(ix-xiii): | Fiber Filter baghouse with minimum OP-manufactures design |

| 5. Fuel, Raw Material, and Waste Description: | Description of Each Feed Stream ^c | | | |
|--|--|---------------------|------------------------|------------------------|
| | | Liq. Waste | Coal | Tires |
| Type (e.g. liquid sludge, drummed solids, coal, shale) | Raw Mat | Pumpable | Fuel | Fuel |
| Category (e.g. Fuel, Raw Materials, Pumpable HW, Nonpumpable HW) | - | 11,000 | 11,000 | 13,500 |
| Typical Heating Value (Btu/lb) | Airslide | Lanced | Feeder | Gravity |
| How Fed (e.g. atomized, lanced, gravity fed) | N | S | N | N |
| Normal feed material (N) or spike (S) | 2.27 x 10 ⁸ | 9 x 10 ⁶ | 1.09 x 10 ⁷ | 2.18 x 10 ⁶ |
| Total Feed Rate (g/hr) ^d | N/A | N/A | N/A | |
| Ash Feed Rate (g/hr) ^e | 4082.3 | 444566 | 5550.7 | 4298 |
| Chlorine and Chloride (g/hr) | 1360.7 | 8981 | 130.63 | 4.35 |
| Antimony (g/hr) | 340.2 | 1520 | 10.89 | 4.35 |
| Arsenic (g/hr) | 5805.9 | 89811 | 685.83 | 108.9 |
| Barium (g/hr) | 680.4 | 20.94 | 5.99 | 1.74 |
| Beryllium (g/hr) | 3401.9 | 3570 | 87.09 | 13.06 |
| Cadmium (g/hr) | 4735.9 | 9878 | 217.72 | 19.16 |
| Chromium (g/hr) | 2268 | 6286.8 | 195.95 | 141.52 |
| Lead (g/hr) | 11.34 | 13.27 | 0.54 | 1.09 |
| Mercury (g/hr) | 226.8 | 4490.5 | 8.71 | 1.31 |
| Silver (g/hr) | 2268 | 8981.13 | 413.68 | 1.09 |
| Thallium (g/hr) | | | | |

*If facility will conduct tests at only one set of test conditions for the stated mode, enter N/A. If two sets of conditions will be run for the mode, fill out a separate form for each set of test conditions. Identify each test condition as 1 or 2.
^bOwners/operators of dry PM control devices that operate at an inlet temperature between 450°F and 750°F must document that emissions of dioxins and furans will not result in an increased MEI cancer risk of greater than 1 in 100,000.
^cCopy form and add additional pages if firing more than four streams during test.
^dRates must not exceed those certified on Form PC-5.
^eNot applicable for cement kilns and light-weight aggregate kilns.

COMPLIANCE TEST NOTIFICATION FORM 3 (CTN-3)
DESCRIPTION OF PLANNED TESTING

Complete a separate form for each test condition (if more than 1) under each mode of operation for each unit.

1. Unit # 1; Mode (letter) A; Test Condition (1, 2, or N/A)* 2

Brief Description of Mode and Test Condition: Maximum burning zone temperature

2. Purpose of Test (e.g., to demonstrate compliance with PM, metals, HCl, and Cl₂ emission limits when firing sludges at maximum feed rate and flue gas flow):

Metal emissions, Hexavalent chromium

3. Attach a complete copy of QA/QC Plan and test protocol.

4. Planned Operating Conditions:

| | |
|---|---|
| Max. Production Rate (specify units) | 255 TPH |
| Max. PM Control Device Inlet Temp. (°F) ^b | 435°F |
| Max. Combustion Chamber Temp. (°F) | 2800°F |
| APCS Operating Conditions (list applicable parameters, see § 266.103(c)(1)(ix-xii): | Fiber filter baghouse with minimum DP-manufactures design |

| 5. Fuel, Raw Material, and Waste Description: | Description of Each Feed Stream ^c | | | |
|---|--|---------------------|------------------------|------------------------|
| | Kiln Feed | Liq. Waste | Coal | Tires |
| Type (e.g., liquid sludge, drummed solids, coal, shale) | Raw Material | Pumpable HW | Fuel | Fuel |
| Category (e.g., Fuel, Raw Materials, Pumpable HW, Nonpumpable HW) | - | 11,000 | 11,000 | 13,500 |
| Typical Heating Value (Btu/lb) | | | | |
| How Fed (e.g., atomized, lanced, gravity fed) | Airslide | Lanced | Feeder | Gravity |
| Normal feed material (N) or spike (S) | N | S | N | N |
| Total Feed Rate (g/hr) ^d | 2.27 x 10 ⁵ | 9 x 10 ⁶ | 1.09 x 10 ⁷ | 2.18 x 10 ⁶ |
| Ash Feed Rate (g/hr) ^e | N/A | N/A | N/A | |
| Chlorine and Chloride (g/hr) | 4082.3 | 444566 | 5550.7 | 4298 |
| Antimony (g/hr) | 1360.7 | 8981 | 130.63 | 4.35 |
| Arsenic (g/hr) | 340.2 | 1520 | 10.89 | 4.35 |
| Barium (g/hr) | 5805.9 | 89811 | 685.83 | 108.9 |
| Beryllium (g/hr) | 680.4 | 29.94 | 5.99 | 1.74 |
| Cadmium (g/hr) | 3401.9 | 3570 | 87.09 | 13.06 |
| Chromium (g/hr) | 4535.9 | 9878 | 217.72 | 19.16 |
| Lead (g/hr) | 2268 | 6286.8 | 195.95 | 141.52 |
| Mercury (g/hr) | 11.34 | 13.27 | 0.54 | 1.09 |
| Silver (g/hr) | 226.8 | 4490.5 | 8.71 | 1.31 |
| Thallium (g/hr) | 2268 | 8981.13 | 413.68 | 1.09 |

*If facility will conduct tests at only one set of test conditions for the stated mode, enter N/A. If two sets of conditions will be run for the mode, fill out a separate form for each set of test conditions. Identify each test condition as 1 or 2.

^bOwners/operators of dry PM control devices that operate at an inlet temperature between 450°F and 750°F must document that emissions of dioxins and furans will not result in an increased MEI cancer risk of greater than 1 in 100,000.

^cCopy form and add additional pages if firing more than four streams during test.

^dRates must not exceed those certified on Form PC-5.

^eNot applicable for cement kilns and light-weight aggregate kilns.

COMPLIANCE TEST NOTIFICATION FORM 4 (CTN-4)

DOCUMENTATION OF PLANNED VERSUS ALLOWABLE FEED RATE LIMITS

Complete a separate form for each mode of operation for each unit.

| Unit #: 1 | Planned Feed Rate ^a | | | Allowable Feed Rates ^b | | |
|------------------------------|--------------------------------|---|---|-----------------------------------|------------------------------------|---|
| | Total Feed Streams | Total Hazardous Waste Feed Streams ^c | Total Pumpable Hazardous Waste Feed Streams | Total Feed Streams | Total Hazardous Waste Feed Streams | Total Pumpable Hazardous Waste Feed Streams |
| Mode (letter): A | | | | | | |
| Constituent | | | | | | |
| Ash (g/hr) ^d | N/A | | | N/A | | |
| Chlorine and Chloride (g/hr) | 455458.97 | | | 455458.97 | | |
| Antimony (g/hr) | N/A | N/A | N/A | 10472.74 | 8981.13 | 8981.13 |
| Arsenic (g/hr) | 1878 | 1526 | 1526 | 1878.07 | 1526.79 | 1526.79 |
| Barium (g/hr) | N/A | N/A | N/A | 96303.30 | 89811.29 | 89811.29 |
| Beryllium (g/hr) | 713 | 26.9 | 26.9 | 713.32 | 26.94 | 26.94 |
| Cadmium (g/hr) | 7081 | 3592 | 3592 | 7081.68 | 3592.45 | 3592.45 |
| Chromium (g/hr) | 15444 | 9879 | 9879 | 15444.00 | 9879.24 | 9879.24 |
| Lead (g/hr) | 87588 | 6286 | 6286 | 875.88 | 6286.68 | 6286.68 |
| Mercury (g/hr) | 27.3 | 15.2 | 15.2 | 27.35 | 15.27 | 15.27 |
| Silver (g/hr) | N/A | N/A | N/A | 4726.26 | 4490.56 | 4490.56 |
| Thallium (g/hr) | N/A | N/A | N/A | 11662.77 | 8981.13 | 8981.13 |

^a Sum of applicable feed streams from all Form CTN-3's.

^b From Form PC-5.

^c Not applicable if complying with Tier I or adjusted Tier I metals feed rate screening limits.

^d Not applicable for cement kilns and light-weight aggregate kilns.

QUALITY ASSURANCE CERTIFICATION

The attached Certification of Compliance Test Report was prepared in accordance to APCC QA/QC procedures as outlined in Section 6.0 of the attached report. As part of the addendum to this report, section 6.8 was added to include a narrative discussion concerning the QA/QC results and a table indicating where the laboratory QA/QC data can be found in the Appendix. To the best of my knowledge all previously missing data has been received and is complete in this report.

John Schneider
Senior Project Engineer



Quality Assurance Manager

ALTERNATE MEASUREMENT TECHNIQUES
FOR MEASURING HYDROCARBONS
UNDER INTERIM STATUS

Under 266.103 of the BIF regulations, an owner that is required to comply with the hydrocarbon controls may use a conditioned gas monitoring system in conformance with the specifications provided in appendix IX, provided that the certification of compliance is submitted without a time extension.

The HC monitoring device used at Lone Star has needed to be cleaned on a regular basis in order to keep this instrument operational. If these problems persist it may be necessary to correct the present hot probe system to a conditional gas system. Every effort will be made to retain the presently used hot probe unconditioned system, however, we can see potential problems that may make this system inoperable unless a conditioned gas system is utilized.

BURNING ZONE MEASUREMENT

The fourth stage inlet temperature was chosen as the point to measure the burning zone temperature. This point was chosen because it represents the point nearest the burning zone temperature where a continuous measurement can be measured. Conditions at locations closer to the burning zone are too severe to measure temperature on a continuous basis.

The fourth stage temperature does respond to changes in the burning zone. During the compliance testing the burning zone temperature was measured by a hand held optical pyrometer and this measurement was compared to the temperature at the fourth stage. The pyrometer used for this measurement was an old instrument and was not in calibration. The calibration is being accomplished at the present time. However, the trend to note is when the fourth stage temperature is high, the burning zone temperature is elevated, and when the fourth stage temperature is low, the temperature in the burning zone is lower. The results are found in the table below:

BURNING ZONE TEMPERATURES
VS 4TH STAGE TEMPERATURES

| | Minimum Conditions | Maximum Conditions |
|--------------|--------------------|--------------------|
| Fourth Stage | 1629 | 1691 |
| Burning Zone | 1928 | 2068 |

During the minimum conditions, the Burning Zone Temperature (BZT) was measured every five minutes and the fourth stage temperatures were monitored on a rolling hourly average basis. The 1629 represents the average of the maximum rolling averages for each test conducted, while 1928 represents the average of the five minute BZT temperatures. During the maximum conditions BZT temperatures were only measured every 15 minutes. This was done for safety reasons. Since the measurement was taken in an opening very near the kiln by a hand held pyrometer, and since the opening through which the pyrometer read the BZT was continually clogged with dust, temperatures could only be obtained every 15 minutes. However, the trend is still apparent, when the fourth stage temperature is raised, the BZT temperature is higher.

Again, it should be pointed out that BZT temperatures are much higher than indicated by the pyrometer. The dusty conditions of the kiln and the calibration of the pyrometer account for the lower temperatures.

BURNING ZONE TEMPERATURES

DATE: 6/25/92 THURSDAY - MINIMUM 4TH STAGE TEMPERATURE

| TIME | TEMP | TIME | TEMP | TIME | TEMP |
|-----------|---------|-----------|---------|------------|---------|
| ===== | ===== | ===== | ===== | ===== | ===== |
| 8:50 A.M. | | 6:00 P.M. | 2060 | 10:15 P.M. | 2095 |
| 8:55 A.M. | | 6:05 P.M. | 2000 | 10:20 P.M. | 2080 |
| 9:00 A.M. | | 6:10 P.M. | 2025 | 10:25 P.M. | 2090 |
| 9:05 A.M. | | 6:15 P.M. | 2040 | 10:30 P.M. | 2025 |
| 9:10 A.M. | | 6:20 P.M. | 2040 | 10:35 P.M. | 2040 |
| 9:15 A.M. | 1725 | 6:25 P.M. | 2040 | 10:40 P.M. | 1995 |
| 9:20 A.M. | 1750 | 6:30 P.M. | 2035 | 10:45 P.M. | 1990 |
| 9:25 A.M. | 1760 | 6:35 P.M. | 2020 | 10:50 P.M. | 1985 |
| 9:30 A.M. | 1740 | 6:40 P.M. | 2010 | 10:55 P.M. | 2040 |
| 9:35 A.M. | 1740 | 6:45 P.M. | 2020 | 11:00 P.M. | 2040 |
| 9:40 A.M. | 1725 | 6:50 P.M. | 1995 | 11:05 P.M. | 2025 |
| 9:45 A.M. | 1675 | 6:55 P.M. | 1970 | 11:10 P.M. | 2050 |
| 9:50 A.M. | 1725 | 7:00 P.M. | 1950 | 11:15 P.M. | |
| R AVG | 1730.00 | R AVG | 2015.77 | R AVG | 2037.92 |

4TH STAGE TEMP
OF 1622.26

4TH STAGE TEMP
OF 1624.19

4TH STAGE TEMP
OF 1642.15

DATE: 6/26/92 FRIDAY - MAXIMUM 4TH STAGE TEMPERATURE

| TIME | TEMP | TIME | TEMP | TIME | TEMP |
|-----------|---------|-----------|---------|------------|---------|
| ===== | ===== | ===== | ===== | ===== | ===== |
| 1:55 P.M. | | 6:15 P.M. | 2020 | 10:00 P.M. | 2030 |
| 2:00 P.M. | 1990 | 6:20 P.M. | | 10:05 P.M. | |
| 2:05 P.M. | | 6:25 P.M. | | 10:10 P.M. | |
| 2:10 P.M. | | 6:30 P.M. | 2085 | 10:15 P.M. | 2000 |
| 2:15 P.M. | 2000 | 6:35 P.M. | | 10:20 P.M. | |
| 2:20 P.M. | | 6:40 P.M. | | 10:25 P.M. | |
| 2:25 P.M. | | 6:45 P.M. | 2100 | 10:30 P.M. | 2050 |
| 2:30 P.M. | 2020 | 6:50 P.M. | | 10:35 P.M. | |
| 2:35 P.M. | | 6:55 P.M. | | 10:40 P.M. | |
| 2:40 P.M. | | 7:00 P.M. | 2140 | 10:45 P.M. | 2130 |
| 2:45 P.M. | 2050 | 7:05 P.M. | | 10:50 P.M. | |
| 2:50 P.M. | | 7:10 P.M. | | 10:55 P.M. | |
| 2:55 P.M. | | 7:15 P.M. | 2180 | 11:00 P.M. | 2190 |
| 3:00 P.M. | 2030 | 7:20 P.M. | | 11:05 P.M. | |
| R AVG | 2018.00 | R AVG | 2105.00 | R AVG | 2080.00 |

4TH STAGE TEMP
OF 1699.6

4TH STAGE TEMP
OF 1685.84

4TH STAGE TEMP
OF 1688.15

PRODUCTION OF NORMAL PRODUCT

Under BIF guidelines, the BIF unit must produce a product within specification for the product normally produced. The unit at Lone Star Cape Girardeau is a cement kiln and produces clinker as its normal product. During the compliance testing, clinker was produced in the kiln system in an acceptable manner to produce cement, and the total production was used to produce portland and/or masonry cement.

Under normal conditions clinker is considered of quality to produce portland cement if the Free Lime (FL) is less than 1.8% and the C3S content is above 40%. Also, contents of other constituent of the clinker are controlled more broadly as shown below:

| <u>Constituent</u> | <u>Range of Acceptable Values</u> |
|--------------------|-----------------------------------|
| K2O | 0-1.1% |
| SO3 | 0.2-2.7% |
| Silica Ratio (SR) | 2.6-3.4 |
| Al2O3/Fe2O3 | 2.5-1.3 |

Clinker outside any of these criteria may also be used to produce portland cement, but is blended with higher quality clinker.

Clinker used to produce masonry cement is generally the same make up as that used to produce portland cement, except that the free lime content can be higher in that clinker used to produce masonry cement.

The laboratory control sheets for clinker during the stack testing is enclosed. The clinker quality during the compliance testing fell within the guidelines listed above, and all the clinker produced during this time period was used to produce product.

6-25-92

| TIME | FL | AL ₂ O ₃ | Fe ₂ O ₃ | SO ₃ | K ₂ O | C ₃ S | SR | LSF | POSITION | REB. | MG |
|-------|------|--------------------------------|--------------------------------|-----------------|------------------|------------------|------|-------|----------|-------|------|
| 7:00 | .47 | 4.67 | 2.84 | .86 | .54 | 49.14 | 3.02 | 88.25 | 6 | 6 | 4.43 |
| 8:00 | .41 | 4.67 | 2.84 | 1.53 | .90 | 44.52 | 3.01 | 87.36 | 6 | 6 | 4.14 |
| 10:00 | .73 | | | | | | | | 6 | 6 | |
| 12:00 | RAW | | | | | | | | 9 1/2 | 9 1/2 | |
| 12:00 | NOON | | | | | | | | 5 1/2 | 5 1/2 | |
| 14:00 | | | | | | | | | 5 1/2 | 5 1/2 | |
| 15:30 | .45 | 4.59 | 2.91 | .95 | .41 | 54.10 | 2.98 | 90.33 | | | 4.31 |
| 16:00 | .41 | | | | | | | | | | |
| 18:00 | .37 | | | | | | | | | | |
| 20:00 | .30 | 4.38 | 2.67 | 1.05 | .55 | 60.36 | 3.13 | 82.78 | 5 1/2 | 5 1/2 | 3.98 |
| 22:00 | .32 | | | | | | | | 5 1/2 | 5 1/2 | |
| 24:00 | .36 | | | | | | | | 6 1/2 | 6 1/2 | |
| 26:00 | .41 | 4.76 | 2.68 | 1.00 | .50 | 47.15 | 3.03 | 82.62 | | | 3.93 |
| 28:00 | .38 | | | | | | | | 10 | 10 | |
| 30:00 | .34 | | | | | | | | | | |
| 32:00 | .29 | 4.64 | 2.72 | 1.11 | .65 | 53.51 | 3.05 | 89.83 | 6 1/2 | 6 1/2 | 3.89 |
| 34:00 | .36 | | | | | | | | | | |
| 36:00 | .42 | | | | | | | | | | |
| 38:00 | .41 | | | | | | | | | | |

DESTROY: AL₂O₃ 4.3% 1st 2nd 3rd

SO₃ K₂O Coal

SO₂ RSP Coal

326 2.87 3.12

UNIT 6-26-02

DATE 6-26-02

| TIME | FL | Al ₂ O ₃ | Fe ₂ O ₃ | SO ₃ | K ₂ O | CaO | SiO ₂ | ISF | POSITION | REL _H | MG |
|---------|-----|--------------------------------|--------------------------------|-----------------|------------------|-------|------------------|-------|----------|------------------|------|
| 8:00 | .71 | 4.63 | 2.70 | 1.20 | .54 | 56.74 | 3.01 | 91.75 | 6:09 | | 4.05 |
| 10:00 | .65 | | | | | 46.72 | | | 6:09 | | |
| 12:00 | .37 | | | | | 48.91 | 3.03 | 87.94 | 5:10 | | 4.16 |
| 12:00 N | .41 | 4.53 | 3.02 | .96 | .47 | | | | | | |
| 14:00 | .46 | 4.57 | 2.79 | 1.10 | .55 | 54.0 | 3.04 | 90.41 | 5:10 | | 4.08 |
| 16:00 | .45 | 4.64 | 2.76 | 1.19 | .54 | 51.02 | 3.04 | 89.36 | 5:10 | | 4.40 |
| 18:00 | .39 | 4.71 | 2.86 | 1.06 | .48 | 48.43 | 3.00 | 88.17 | 5 | | 4.01 |
| 20:00 | .32 | 4.79 | 2.89 | .81 | .53 | 46.01 | 2.99 | 86.94 | 5:12 | | 4.03 |
| 22:00 | .34 | | | | | | | | 5:12 | | |
| 24:00 | .32 | 4.70 | 2.82 | 1.04 | .53 | 44.44 | 3.08 | 86.50 | 5:12 | | 3.99 |
| 2:00 | .32 | | | | | | | | 5 | | |
| 4:00 | .38 | 4.76 | 3.09 | .62 | .57 | 48.72 | 2.91 | 87.82 | | | 3.96 |
| 6:00 | .58 | | | | | 4.58 | | | | | |

| DESCRIPTION | 1st | 2nd | 3rd |
|--------------------------------|-------|-----|-----|
| Al ₂ O ₃ | 4.32 | | |
| Fe ₂ O ₃ | 3.12 | | |
| SO ₃ | 52.02 | | |
| 503 KILN COAL | 3.58 | | |
| 502 RSP COAL | 3.58 | | |
| TOTAL | 3.60 | | |

TOTAL P. 13

FUGITIVE EMISSIONS SYSTEMS

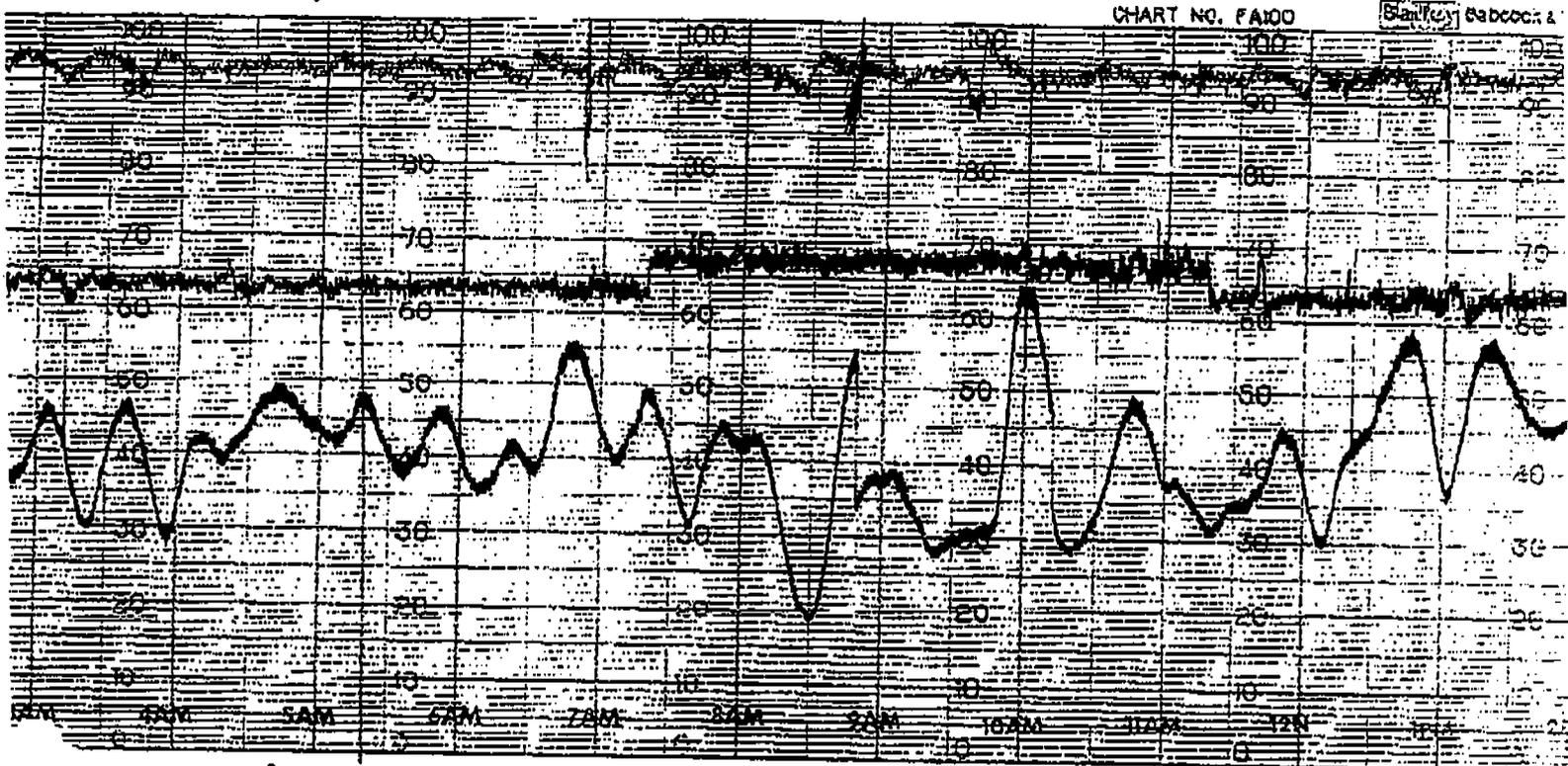
During interim status, BIF's must comply with the requirements in 266.103 (h) to control fugitive emissions from the combustion zone. Measurements are presented below showing that the kiln at the Lone Star Cape Girardeau plant maintains a pressure less than atmospheric when containerized waste are fed into the kiln system.

The kiln at the Lone Star Cape Girardeau plant operates under a negative-pressure. Containerized waste are fed into the front part of the kiln by an air cannon. The containers are injected 50 feet into the burning zone of the kiln. When these wastes are fed into the kiln it has been demonstrated that the system does not generate pressures greater than atmospheric when the containers burst.

The demonstration is based on the pressure at the front of the kiln called the "Hood Pressure". By a system of fans, the pressure at the kiln hood is maintained at a desired set point. The set point chosen to operate the kiln is between -0.10 and -0.20" wc for this particular system. The line near the 60% mark on the enclosed chart paper represents the hood pressure (HP) on a 0-100% scale. The actual range for the HP is -1.0" wc for 0% and 100% represents +.25" wc. The chart indicated that the HP normally is controlled in the 63% range. This would indicate an actual HP of approximately -0.2" wc.

On July 28, 1992, containerized waste was injected into the kiln with an air cannon between the hours of 6:00 a.m. and 10:00 p.m. at a rate of one bucket per minute. Each bucket contained 25 pounds of waste. The chart indicates that the HP remained very near the set point before containerized waste was fed to the kiln and after the waste was fed to the kiln. At no time did the HP approach atmospheric pressure (indicated by 80% on the chart). Containerized waste have no significant effect on the pressure inside the kiln.

If process conditions occur that cause the HP to approach 0"wc (atmospheric) an alarm is activated and the injection of waste is discontinued until the system stabilizes.



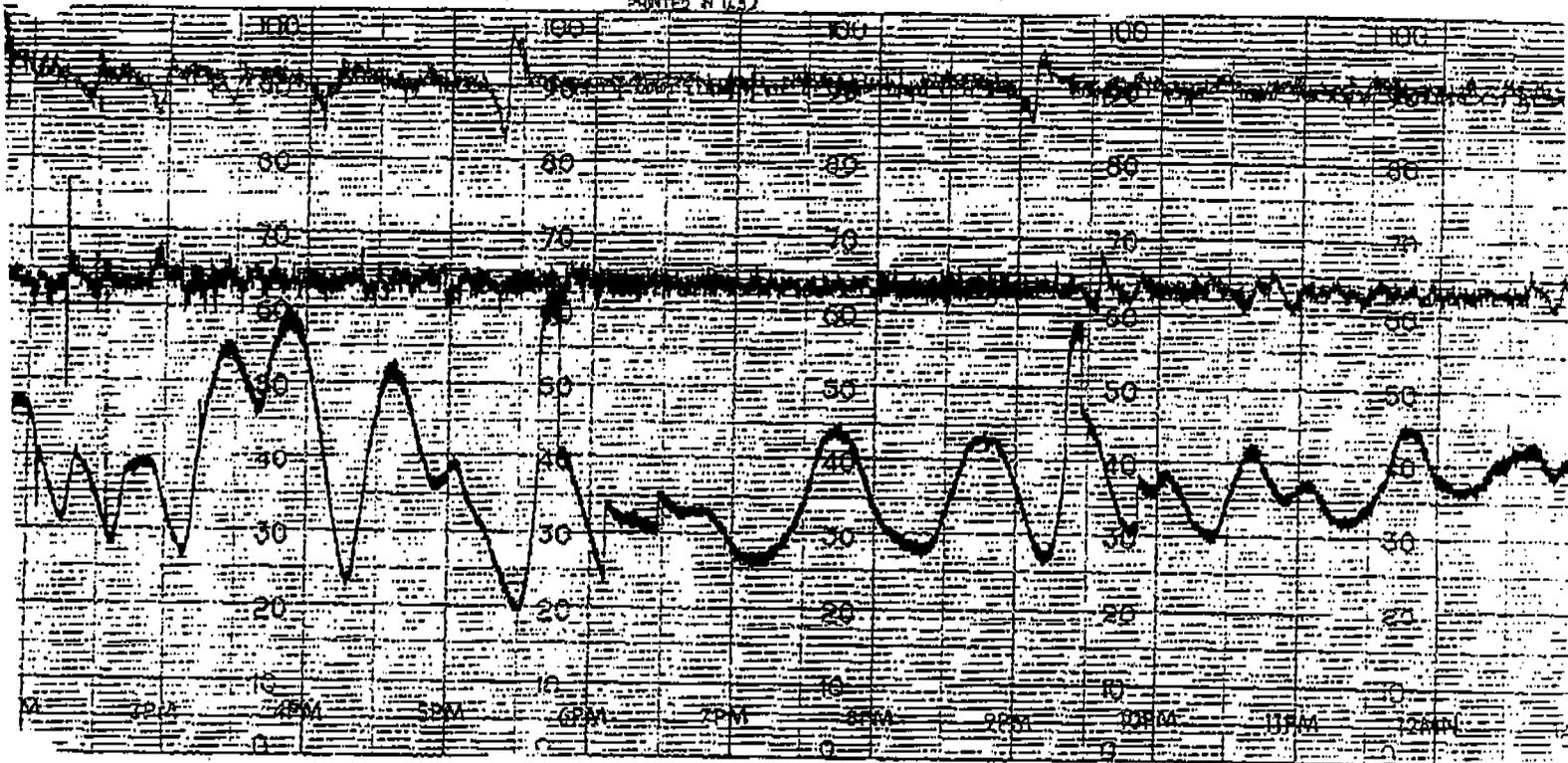
28-92

0% = -1.0 "wc

100% = +0.25 "wc

15A

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7-29-92

3.0 QUALIFICATIONS AND EXPERIENCE

Air Pollution Characterization and Control, Ltd. (APCC) was incorporated in the State of Connecticut in May 1988 to provide specialty professional environmental services to aid industry and government in their quest to keep abreast of regulatory issues, to maintain compliance with government regulations, to assist in industrial process evaluations, to aid in the definition of air pollution problems and establish control strategies for those problems. APCC is expertly qualified to assist its clients in the following areas at extremely cost effective rates:

- AIR TOXICS EVALUATION AND CONTROL
- AIR POLLUTION CONTROL TECHNOLOGY
- CONTINUOUS EMISSION MONITORING
- INDOOR AIR QUALITY EVALUATION
- HAZARDOUS WASTE INCINERATION
- TRIAL BURNS
- PART B PREPARATION
- SARA TITLE III
- SOURCE EMISSION MEASUREMENTS
- FUGITIVE EMISSION EVALUATION
- ENVIRONMENTAL AUDITS
- EMISSION INVENTORIES
- AEROMETRIC MONITORING
- DISPERSION MODELING
- ENVIRONMENTAL PERMITTING
- ODOR ASSESSMENT
- MUNICIPAL WASTE INCINERATION
- RISK ASSESSMENT

3.1 Summary of Capabilities

APCC consists of a team of scientists and engineers, complemented by a network of other consulting engineers and scientists, dedicated to defining and solving environmental problems. Although a relatively new firm, APCC has amassed a significant amount of project experience in the past three years, which is supplemented by over 50 man-years of experience in the field of air pollution measurements and control by the expertly qualified staff. During this period, the staff has established contacts with numerous environmental professionals, including many at the U.S. EPA as well as many state and local regulatory agencies. Principal consultants which are drawn from a network to make up a project team are professional engineers registered in numerous states with over 15 years experience in the field of air pollution. Projects are managed by skilled professionals who give proper attention to planning, technical direction and quality assurance for the project team. These project teams are made complete by a group of field technicians to assist in the performance of field projects on a nationwide basis.

APCC project teams consist of engineers, scientists and technicians, each with a clear area of responsibility and experience working together as an efficient team. These teams are supported by a network of state-of-the-art measurement equipment,

computer facilities and laboratory facilities capable of virtually any chemical analytical technique. In addition, APCC can provide on-site analytical services for many wet chemical as well as gas chromatographic analyses.

Atmospheric contamination from toxic air pollutants is of primary industrial, regulatory and public concern. APCC specializes in providing timely, cost effective air pollution measurement and control technology services followed up by thorough and interpretive reports with high quality, usable results. This valuable strategy for solving air pollution problems begins with basic problem identification with follow through to complete permitting and compliance. A "Whole Process Orientation" towards these problems looks at a specific problem as a function of the whole, thereby allowing objective points of view in the definition and solution of the problem to include the entire process or facility rather than a narrow focus on only an apparent problem. This approach helps to avoid short-sighted "solutions" to problems that could cause further problems in the future or in other segments of the facility or process as well as to provide cost effective, defensible solutions.

Upon the inception of any project, APCC routinely visits the site to perform a plant survey to develop a "hands-on" feel of the situation and to collect the information required to formulate a comprehensive project plan. In the case of a project for compliance determination, this information is used to prepare protocols for submission to regulatory agencies for approval prior to performance. In performing measurements, APCC utilizes EPA, ASTM, ASME, NIOSH and other approved protocols to determine emissions and ambient levels of toxic substances as well as criteria and priority pollutants, including Dioxins and Furans, POHC, VOC, PIC, Heavy Metals, HCl, NO_x, SO₂, CO, TRS and particulate. In the absence of applicable approved methodology, APCC has integrated published sampling and analytical methods and developed new methods to provide clients with accurate and reliable engineering data.

In addition to a full range of air pollution measurement services, APCC can provide expert services to evaluate the degree of air pollution control required to meet emission and ambient air standards for numerous pollutants. Engineers review potentially available control technologies or combinations thereof to afford the required emission reduction. Practical systems are then scrutinized in great detail to determine technical, operational and economic compatibility with the defined problem utilizing BACT, RACT and LAER analyses. Working closely with the client, APCC develops preliminary design specifications, solicits vendor bids, prepares air permit applications, supervises installation and performs performance and compliance emission testing. APCC engineers and scientists will provide expert testimony before state and federal regulatory agencies as well as public hearings in defense of the specified system.

APCC is expertly qualified to design, fabricate, install and calibrate ambient and aerometric monitoring networks to comply with Prevention of Significant Deterioration (PSD) requirements. Upon the installation of a system, APCC provides operational training to clients personnel to ensure ease of operation and maintenance.

Design and installation of permanent Continuous Emission Monitoring Systems is a service provided by APCC. These systems can be designed, specified, installed and made operational, certified, maintained and audited by APCC personnel.

Air permitting services provided by APCC require the resolution of complex state and local regulatory issues, streamlined to meet individual project requirements. APCC will interact with federal, state and local regulatory agencies to determine the applicability of regulations, establish a rapport with agency personnel and negotiate permit conditions.

In conjunction with the aforementioned services, APCC performs emission inventories and environmental audits to cost effectively determine environmental liability. These inventories and audits consist of in-plant surveys to determine the use and fate of toxic and other regulated substances. Mass balances are then performed and calculated emissions compared to regulations to determine possible problem areas. Further study is then performed, including measurements, to determine compliance with federal, state and local regulations.

In addition to a dedicated staff of professionals, APCC is aided by a complete assortment of brand new state-of-the-art equipment to perform engineering measurements. Over the past two years, APCC has invested over \$250,000 in air pollution measurement equipment and computerization to provide our clients with the best data possible upon which to formulate solutions to their problems. The APCC Environmental Monitoring Laboratory (EML), a mobile instrument laboratory housed in a 24 foot climate controlled custom built trailer, is designed to provide a cost effective solution for continuous emission monitoring of CO, NO_x, SO₂, O₂, CO₂ and total hydrocarbons; for on-site on-line gas chromatography (dual column/dual detector) and on-site wet chemical analyses of samples. This unit is ideal for CEMS Relative Accuracy Testing, Reference Method Testing during in-plant CEMS down-time in order to avoid process interruptions, hazardous waste trial burns, performance testing of air pollution control equipment and measurements requiring immediate analyses of samples in order to avoid sample degradation or implement process modifications. An additional advantage allows the performance of emission measurements and sample recovery under almost any weather and plant conditions and in any season.

In summary, APCC is qualified and ready to assist your organization with problems related to air pollution characterization and control. Section 2 of this Statement of Qualifications and Experience relates specific project experience of APCC since its inception as well as experience gained by its principals over the past 10 years. Section 3 presents resumes of key APCC personnel and those of the consulting engineers and scientists available to the project team.

3.2 Case Studies of Experience

Since its inception in May 1988, APCC has performed a number of projects for a diverse group of clientele. Since all work is performed on a strictly confidential basis, actual client names cannot be utilized in a document of this type. Actual references can be provided upon request. The first group of project experience relates to work directly performed by APCC, while the second group past reflects experience of its principals.

3.2.1 APCC EXPERIENCE

WASTE FUEL COMBUSTOR

APCC performed a trial burn program for a client firing hazardous waste fuels in an expanded aggregate kiln under the proposed EPA Industrial Furnace Regulations. The project involved air and hazardous waste permitting, process operational parameter measurements for permit verification, Trial Burn Protocol preparation (requiring over three years of negotiations with the state regulatory agency), preparation of the facility for the trial burn program including trouble shooting and "tune ups" of the air pollution control and continuous emission monitoring systems as well as performance of the actual trial burn including measurements of PCDD/PCDF, POHC, particulate, metals, acid gases and complete continuous emission monitoring. CEMS Performance Specification Testing was also performed. Consultation was provided in the preparation of a health risk assessment related to plant emissions subsequent to the trial burn.

Results of the Trial Burn program indicated acceptable emissions for all measured parameters with the exception of particulate. A BACT analysis was then performed to determine the most practical form of emission control for the source. APCC then assisted the client in soliciting bids, selecting a vendor to install the new air pollution control equipment (a fabric filter followed by a series of wet venturi scrubbers) and reviewing the engineering design of the system. A Supplemental Trial Burn Protocol was then negotiated. Following completion of the new air pollution control system, performance and shakedown testing of the new system was performed followed by the Supplemental Trial Burn. The Trial Burn Report was recently submitted and permit issuance is expected soon.

SECONDARY ALUMINUM ALLOYING

APCC was retained by a Midwest specialty aluminum refiner following the denial by the state EPA of an application to renew a Permit to Operate a melting furnace. A test program previously performed by a local firm had demonstrated noncompliance with state emission limitations for particulate, but the report failed to bring this fact to the owner's attention and was unknowingly submitted to the state EPA as part of the application package. Along with the rejection of the permit application, the state EPA demanded the installation of hard air pollution control technology (estimated cost in excess \$500,000) prior to consideration of further applications. APCC's task at that point was to

**CERTIFICATION OF COMPLIANCE TEST
FOR THE BURNING OF
WASTE DERIVED FUELS
AT
LONE STAR INDUSTRIES, INC
CAPE GIRARDEAU, MISSOURI**

PREPARED FOR
US EPA REGION VII
and
MISSOURI DNR

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August 1992
Revised September 1992

APCC Project 92007

EPA Facility ID No. MOD 981127319

TABLE OF CONTENTS

| Section No. | Title | Page No. |
|-------------|---|----------|
| 1.0 | INTRODUCTION | 1 |
| 1.1 | Technical Approach | 1 |
| 2.0 | RESULTS AND DISCUSSION | 7 |
| 2.1 | Phase 1 | 9 |
| 2.1.1 | Particulate, Chloride and Chlorine Measurements | 9 |
| 2.1.2 | Chloride Mass Balance | 9 |
| 2.1.3 | Heavy Metals Emissions | 9 |
| 2.1.4 | Metals Mass Balance | 13 |
| 2.1.5 | POHC Emissions | 13 |
| 2.1.6 | Continuous Emissions Monitoring of CO, THC and O ₂ | 13 |
| 2.2 | Phase 2 | 18 |
| 2.2.1 | Particulate, Chloride and Chlorine Measurements | 18 |
| 2.2.2 | Chloride Mass Balance | 18 |
| 2.2.3 | Heavy Metals Emissions | 18 |
| 2.2.4 | Metals Mass Balance | 23 |
| 2.2.5 | POHC Emissions | 23 |
| 2.2.6 | Continuous Emissions Monitoring of CO, THC and O ₂ | 27 |
| 3.0 | PROCESS AND OPERATIONS | 30 |
| 3.1 | Portland Cement Process | 30 |
| 3.2 | Fuel Burning | 33 |
| 3.3 | Air Pollution Control System | 37 |
| 3.4 | Kiln Safety Systems | 39 |
| 3.5 | COC Process Operations | 39 |
| 3.5.1 | Phase 1 | 39 |
| 3.5.2 | Phase 2 | 40 |
| 3.6 | Metals Spiking | 51 |
| 3.7 | POHC Spiking | 52 |

TABLE OF CONTENTS

| Section No. | Title | Page No. |
|-------------|---|----------|
| 3.8 | Process Mass Balance Sampling | 53 |
| 4.0 | SAMPLING AND ANALYTICAL METHODS | 54 |
| 4.1 | Stack Emission Measurements | 54 |
| 4.1.1 | Particulate, HCl and Chlorine Emission Measurements | 54 |
| 4.1.2 | O ₂ , CO ₂ and CO Manual Determination | 56 |
| 4.1.3 | Heavy Metals Emission Measurement | 56 |
| 4.1.4 | Volatile POHC / DRE | 59 |
| 4.1.5 | Hexavalent Chromium | 60 |
| 4.1.6 | Continuous Emission Monitoring of CO, THC, O ₂ & CO ₂ | 61 |
| 4.2 | Combustion Efficiency | 63 |
| 4.3 | Raw Material and Product Samples | 64 |
| 5.0 | SCOPE OF THE SAMPLING PROGRAM BY SITE | 66 |
| 5.1 | Stack Emission Samples | 66 |
| 5.1.1 | Particulate, HCl and Chlorine Emission Measurements | 66 |
| 5.1.2 | O ₂ , CO ₂ and CO Integrated Measurements | 66 |
| 5.1.3 | Heavy Metal Emission Measurements | 69 |
| 5.1.4 | Volatile POHC Emission Measurements | 69 |
| 5.1.5 | Hexavalent Chrome Emission Measurements | 69 |
| 5.1.6 | Continuous Emission Monitoring | 69 |
| 5.2 | Raw Material and Product Samples | 69 |
| 5.3 | Test Schedule | 72 |
| 6.0 | QUALITY ASSURANCE PROGRAM | 73 |
| 6.1 | Project Organization and Responsibility | 73 |
| 6.2 | Sampling Quality Assurance | 75 |
| 6.2.1 | EPA & SW Manual Methods | 76 |
| 6.2.2 | CEM System | 76 |
| 6.2.3 | VOST Method | 76 |

TABLE OF CONTENTS

| Section No. | Title | Page No. |
|-------------|------------------------------------|----------|
| 6.3 | Analytical Quality Control | 77 |
| 6.4 | Sample Chain of Custody Procedures | 78 |
| 6.5 | Laboratory QA/QC Procedures | 78 |
| 6.6 | Data Reduction and Reporting | 79 |
| 6.7 | Data Validation | 79 |
| 6.8 | QA/QC Results | 79 |
| 6.8.1 | Phase 1 | 80 |
| 6.8.2 | Phase 2 | 80 |

LIST OF TABLES

| Table No. | Title | Page No. |
|-----------|---|----------|
| 1-1 | Test Sequence | 2 |
| 2-1 | Particulate/Chlorine/HCl Data Summary/Phase 1 | 10 |
| 2-2 | Chloride Mass Balance/Phase 1 | 11 |
| 2-3 | Summary of Metals Emissions/Phase 1 | 12 |
| 2-4 A&B | Mass Balance Metals Data/Phase 1 | 14,15 |
| 2-5 | POHC Emission Summary/Phase 1 | 16 |
| 2-6 | APCC CEM Data Summary/Phase 1 | 17 |
| 2-7 | Particulate/Chlorine/HCl Data Summary/Phase 2 | 19 |
| 2-8 A&B | Chloride Mass Balance/Phase 2 | 20,21 |
| 2-9 | Summary of Metals Emissions/Phase 2 | 22 |
| 2-10 A&B | Mass Balance Metals Data/Phase 2 | 24,25 |
| 2-11 | DRE Summary Data | 26 |
| 2-12 | APCC (Stack) CEM Data Summary/Phase 2 | 28 |
| 2-13 | Lonestar Bypass Duct CEMS Data | 29 |
| 3-1 | Typical Coal Analysis | 34 |
| 3-2 | Typical Organic Substances in WDLF & WDSF | 35 |
| 3-3 | WDLF & WDSF Burn Specifications | 36 |
| 3-4 | Typical Tire Analysis | 37 |
| 3-5 A&B | Monitored Operational Data | 43,44 |
| 4-1 | Mass Balance Methods of Analysis | 65 |
| 5-1 | Sampling Matrix | 67 |

LIST OF TABLES

| Table No. | Title | Page No. |
|-----------|--|----------|
| 6-1 | Chlorine, HCl, and Particulate Q.C. Data | 81 |
| 6-2 | Metals Q.C. Data | 82 |
| 6-3 | Hexavalent Chrome Q.C. Data | 83 |

FIGURES

| Figure No. | Title | Page No. |
|------------|--|----------|
| 3-1 | Process Schematic | 31 |
| 3-2 | Kiln Temperature Profile | 32 |
| 3-3 | Kiln Operation Trends - Test 3 | 45 |
| 3-4 | Kiln Operation Trends - Test 4 | 46 |
| 3-5 | Kiln Operation Trends - Test 5 | 47 |
| 3-6 | Kiln Operation Trends - Test 7 | 48 |
| 3-7 | Kiln Operation Trends - Test 8 | 49 |
| 3-8 | Kiln Operation Trends - Test 9 | 50 |
| 5-1 | Sampling Port and Traverse Point Locations | 68 |
| 5-2 | Mass Balance Sampling Locations | 71 |
| 6-1 | Project Organization Chart | 74 |

APPENDIX LIST

| Appendix No. | Title | Page No. |
|--------------|-------|----------|
|--------------|-------|----------|

Appendix A

| | |
|---|------|
| Particulate/Chlorine/HCl Data Summary/Phase 1 | A-2 |
| Summary of Chloride Mass Balance Data/Phase 1 | A-3 |
| Metals Data Summary/Phase 1 | A-4 |
| Summary of Mass Balance Metals Data/Phase 1 | A-5 |
| VOST Train Worksheet/Phase 1 | A-6 |
| APCC CEM Data Summary/Phase 1 | A-7 |
| Particulate/Chlorine/HCl Data Summary/Phase 2 | A-13 |
| Summary of Chloride Mass Balance Data/Phase 2 | A-14 |
| Metals Data Summary/Phase 2 | A-15 |
| Cr6 Data Summary/Phase 2 | A-16 |
| Mass Balance Metals Data/Phase 2 | A-17 |
| VOST Train Worksheet/Phase 2 | A-18 |
| APCC CEM Data Summary/Phase 2 | A-19 |

Appendix B

| | |
|---|-------|
| Particulate/Chlorine/HCl Emissions | B-1 |
| Mass Balance Sampling | B-7 |
| Metals Emissions | B-48 |
| POHC Emissions | B-57 |
| Continuous Emissions Monitoring/Phase 1 | B-78 |
| Continuous Emissions Monitoring/Phase 2 | B-145 |
| Continuous Emissions Monitoring/Variable Operations | B-341 |

Appendix C

| | |
|---|--------|
| Particulate/Chlorine/HCl Emissions | C-1 |
| Chloride Mass Balance/Fuel Characterization | C-11 |
| Metals Emissions | C-41 |
| Metals Mass Balance | C-786 |
| POHC Emissions/DRE | C-1204 |

APPENDIX LIST

| Appendix No. | Title | Page No. |
|--------------|-------|----------|
|--------------|-------|----------|

Appendix C Addendum

| | |
|-------------------------------|--------|
| Additional Laboratory QC Data | C-1369 |
| Phase 1 VOST Train Data | C-1382 |
| Phase 2 VOST Train Data | C-2159 |
| Phase 2 Volatile Samples | C-2848 |

Appendix D

| | |
|--------------------------|-----|
| Process Operational Data | D-1 |
|--------------------------|-----|

Appendix E

| | |
|-------------------------|-----|
| Sampling Train Diagrams | E-1 |
|-------------------------|-----|

Appendix F

| | |
|------------------|-----|
| Calibration Data | F-1 |
|------------------|-----|

Appendix G

| | |
|------------------|-----|
| Chain of Custody | G-1 |
|------------------|-----|

1.0 INTRODUCTION

Air Pollution Characterization and Control, Ltd. (APCC), of Tolland Connecticut, under contract to the Lone Star Industries, Inc., was contracted to perform a Certification of Compliance (COC) emission measurement program to demonstrate the acceptability of rotary cement kiln incineration of Waste Derived Liquid and Solid Fuels (WDLF/WDSF) for energy recovery purposes at the Lone Star facility in Cape Girardeau, Missouri.

This Certification of Compliance test program was required to be performed by Code of Federal Regulations, Title 40, Part 266 STANDARD FOR THE MANAGEMENT OF SPECIFIC HAZARDOUS WASTE AND SPECIFIC TYPES OF HAZARDOUS WASTE MANAGEMENT FACILITIES (commonly known as Boiler and Industrial Furnace Regulations or 'BIF') and Section 266.103, Interim Status Standards For Burners, promulgated February 21, 1991. In addition, this test program demonstrated the acceptability of the Lone Star kiln to destroy WDLF, WDSF and tires for compliance with Missouri Department of Natural Resources requirements. The State of Missouri also requires an emission test program under 10 CSR 25 of the Missouri Administrative Code. This report intermixes the requirements of both agencies.

John H. Powell, Principal of APCC and program manager, has personally managed hazardous waste trial burn programs at cement / expanded aggregate manufacturing facilities since 1984. Robert J. Zychal, Manager of Engineering for APCC, is the Project Engineer and Field Crew Chief for this project. Edward P. Nowak was responsible for all analytical phases and Yakov Zusmanovich for data reduction. John E. Schneider performed QA/QC review for the project. Other APCC personnel included Don Smith, James Severson, Adam Ploszaj, Peter Day and Earl Most.

Norris Johnson, Manager of Lone Star AAF was responsible for the overall program. Kiln operations were supervised by Harry Phillip of Lone Star. All process input / output sampling for mass balance was performed under the supervision of Steve Sebaugh of Lone Star. Waste fuel feed and spiking was supervised by Paul Knowlson of CP Recycling, the waste fuel supplier.

Lone Star also contracted the Services of Schreiber, Yonley & Grana to provide oversight QA/QC of the program and to ensure adherence to the protocol. Doug Elley of MO DNR was on-site throughout the test program. Wane Roberts, Khalid Aljunadi and Mike Tharpe of DNR were also on-site for portions of the program. No US EPA personnel were on-site during the program.

1.1 TECHNICAL APPROACH

This COC was performed during April and June 1992. The COC program was conducted in two Phases; firing coal only (Phase 1 - April) and firing coal/WDF/tires (Phase 2 - June). Phase II was further divided into two distinct operating conditions as discussed below. Table 1-1 summarizes the testing sequence as presented in this report.

**TABLE 1-1
TEST SEQUENCE
CERTIFICATION OF COMPLIANCE TEST
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
JUNE, 1992**

PHASE 1

| TEST NO. | DATE | DESCRIPTION |
|----------|---------|--|
| 1 | 4/12/92 | Trip & Field Blanks for VOST and Blank Train for PM/HCI/CI |
| 2 | 4/13/92 | PM/HCI/CI, VOST, CEM |
| 3 | 4/13/92 | PM/HCI/CI, VOST, CEM |
| 4 | 4/13/92 | PM/HCI/CI, VOST, CEM |
| 5 | 4/13/92 | Blank Train for Metals |
| 6 | 4/14/92 | Metals, CEM |
| 7 | 4/14/92 | Metals, CEM |
| 8 | 4/14/92 | Metals, CEM |

PHASE 2

| TEST NO. | DATE | DESCRIPTION |
|----------|---------|--|
| 1 | 6/22/92 | Trip & Field Blanks for VOST and Blank Train for PM/HCI/CI |
| 2 | 6/25/92 | Discarded Test Run |
| 3 | 6/25/92 | PM/HCI/CI, VOST, CEM |
| 4 | 6/25/92 | PM/HCI/CI, VOST, CEM |
| 5 | 6/25/92 | PM/HCI/CI, VOST, CEM |
| 6 | 6/24/92 | Train Blanks for Cr+6 and Metals |
| 7 | 6/26/92 | Cr+6, Metals and CEM |
| 8 | 6/26/92 | Cr+6, Metals and CEM |
| 9 | 6/26/92 | Cr+6, Metals and CEM |

Phase 1

Phase 1 was the background determination of kiln emissions while firing coal only. This Phase was performed concurrent with a Tire Trial Burn during April, 1992. Items tested for in triplicate were:

- POHC
- Heavy Metals Emissions (As, Be, Cd, Cr, Ag, Ba, Hg, Pb, Sb, Tl & Zn)
- CEM @ Exhaust Stack
 - Carbon Monoxide Emissions (CO)
 - Total Hydrocarbon (THC) Emissions
 - Stack Gas Oxygen (O₂)
- Particulate Matter (PM)
- Chloride (HCl), Chlorine (Cl₂)

Testing also included mass balance determinations for metals and chlorides. Hexavalent chrome emissions were not monitored during this period.

Phase 2

Phase 2 was performed while the kiln was firing a combination of WDF and tires for 100% kiln fuel replacement. Coal was fired in the pre-calciner only.

This Phase was divided into two operating conditions. The first condition determined the destruction and removal efficiency (DRE) of the kiln for surrogate POHCs while operating under the **MINIMUM PRACTICAL TEMPERATURE CONDITIONS**. During this period triplicate measurements of the following parameters were performed.

- POHC / DRE
- CEM @ Exhaust Stack
 - Carbon Monoxide Emissions (CO)
 - Total Hydrocarbon (THC) Emissions
 - Stack Gas Oxygen (O₂)
- CEM @ Bypass Duct
 - Carbon Monoxide Emissions (CO)
 - Total Hydrocarbon (THC) Emissions
 - Bypass Oxygen (O₂)
- Particulate Matter (PM)
- Chloride (HCl), Chlorine (Cl₂)

The following operating parameters were either minimized or maximized (as appropriate) for the required 1-hour rolling average by the plant operators for determination of operational limits as follows:

- Minimum combustion chamber temperature
- Maximum pumpable waste derived fuel feed rate
- Maximum total waste derived fuel feed rate

- Maximum chlorine feed
- Maximum production rate
- Maximum ID fan amps

The DRE of the POHCs and the maximum CO and THC in the exhaust gases were measured and reported as part of this COC.

The second operating condition of this Phase was to determine the emissions of the following parameters and System Removal Efficiencies (SRE) for metals while the kiln is at **MAXIMUM PRACTICAL TEMPERATURE**. During this phase triplicate measurements of the following parameters were performed:

- Metals Emissions & SRE (Pb, As, Cr, Be, Cd, Hg and Zn)
- Hexavalent Chromium Emissions (Cr⁺⁶)
- Total Hydrocarbon (THC) emissions
- Carbon Monoxide Emissions
- Oxygen Emissions

The following operating parameters were either minimized or maximized (as appropriate) for the required 1-hour rolling average by the plant operators for this portion of the COC:

- Maximum combustion chamber temperature
- Maximum APCD temperatures (both main and bypass)
- Maximum pumpable waste derived fuel feed rate
- Maximum total waste derived fuel feed ratio
- Maximum metals feed rate (Pb, As, Cr, Be, Cd and Hg)
- Maximum total chlorine feed rate
- Maximum ID fan amps

Phase 3

Phase 3 was planned to be a repeat of Phase II while firing 100% WDF in the kiln (no tires) and coal in the precalciner only. The same sampling and operational conditions of Phase II were planned for this test. Upon completion of Phase 2, which was considered a worse case than Phase 3, however, it was determined by Lone Star that there was no need for Phase 3, as all required data was obtained during Phase 2.

It should be noted that a Tier 2 CO emission limitation in the bypass duct was not demonstrated during either Phase 1 or Phase 2. The bypass CEMS was not yet installed during Phase 1 to observe CO emissions under 100% coal fire. During Phase 2 (@ 100% WDF w/ tires in the back end) CO emissions were within the Tier 1 range (i.e. <100 ppm @ 7% O₂). Subsequent to Phase 2 testing, however, significant concentrations of CO have been observed when firing **less waste fuel** and a greater amount of coal. Measured emissions concentrations of THC are always insignificant (< 1 ppm actual) under all operating conditions.

Due to this situation, Lone Star, with the approval of Joe Galbraith of EPA Region VII, conducted a number of additional different tests under varying operating

conditions during the months of July and August to establish a Tier 2 CO emission limitation. These conditions were each approximately 6 hours each in duration and were as follows:

- 100% coal in kiln / coal in precalciner
- 100% coal in kiln / tires at back end & coal in precalciner
- 50% WDF & 50% coal in kiln / coal in precalciner
- 50% WDF & 50% coal in kiln / tires at back end & coal in precalciner
- 100% WDF in kiln / coal in precalciner
- 100% WDF in kiln / tires at back end & coal in precalciner

The results of this testing are presented under separate cover and were used to determine a CO Limitation for WDF cutoff.

A material mass balance on the kiln was performed during both Phases for chlorides as per Part 266.103 (c) (1) Limits on operating conditions. In addition, a metals mass balance was performed during each phase to determine maximum metals input and validate PCC Engineering Judgements. Listed below are the material input and output sample locations.

INPUTS

- Coal feed belts (2)
- Water for the Conditioning Tower
- Raw material feed to kiln
- Tire feed
- WDLF feed
- WDSF feed
- Metals Spike
- Spent kiln brick (planned for, not available during COC)

OUTPUTS

- Clinker cooler conveyer
- Kiln / Preheater dust
- Bypass baghouse hopper
- Stack/Kiln outlet (Emissions)

Sampling was not performed for dioxins and furans (PCDD/PCDF). The BIF regulation exempts facilities from the requirements for PCDD/PCDF testing if the following regulations are met: 266.104, Standards to Control Organic Emissions and 266.112, Regulation of Residues. CO concentrations at the bypass did not exceed 100 ppm corrected to 7 % oxygen during the actual test program. Although CO did exceed 100 ppm under subsequent operational conditions (firing **less WDF** and more coal, the concentration of total hydrocarbons was always less than 20 ppm (as propane) corrected to 7% O₂. With the inlet to the air pollution control system maintained below 450°F, no PCDD/PCDF testing was required for the COC.

Section 2 of this report presents all test results and a discussion thereof. Section 3 presents a summary of the portland cement process, the air pollution control system, the kiln safety systems and COC process operations. A full description of all sampling and analytical methods employed is presented in Section 4. Section 5 describes the Scope of the Sampling Program on a Site Specific Basis and specifies the test schedule. Section 6 of this plan presents the APCC Quality Assurance Plan for this program. Data summaries, raw field and laboratory data, process operational data, sampling train figures and calibrations are presented in the Appendix of this Report. See Table of Contents for exact document locations.

2.0 RESULTS AND DISCUSSION

The Certification of Compliance test program was performed over 2 distinct one-week periods. Phase 1 testing was performed while the kiln fired only coal in April 1992. Phase 2 was performed while the kiln was firing 100% WDF, with tires in the back end and coal in the precalciner in June 1992.

During Phase 1, the kiln was operated under normal steady state operating conditions. During Phase 2, two distinct abnormal operating conditions were run in an attempt to set minimum and maximum kiln operating limits. This typically meant running the kiln under near upset conditions while still producing saleable product. In an attempt to set minimum and maximum hourly rolling averages for operational parameters as required by BIF, it should be noted that it was necessary to manipulate the kiln to the edge of upset and/or shut-down conditions. Operation was then held at this point as long as possible to set the limitation by establishing a 1-hour rolling average, as required by Section 5.3.1 of "Technical Implementation Document for EPA's Boiler and Industrial Furnace Regulations" (EPA-530-R-92-011, March 1992).

The first condition determined the destruction and removal efficiency (DRE) of the kiln for surrogate POHCs while operating under the **MINIMUM PRACTICAL TEMPERATURE CONDITIONS**. During this period triplicate measurements were performed of the following parameters:

- POHC / DRE
- CEM @ Exhaust Stack
 - Carbon Monoxide Emissions (CO)
 - Total Hydrocarbon (THC) Emissions
 - Stack Gas Oxygen (O₂)
- CEM @ Bypass Duct
 - Carbon Monoxide Emissions (CO)
 - Total Hydrocarbon (THC) Emissions
 - Bypass Oxygen (O₂)
- Particulate Matter (PM)
- Chloride (HCl) and Chlorine (Cl₂) Emissions

The following operating parameters were either minimized or maximized (as appropriate) for the required 1-hour rolling average by the plant operators for determination of operational limits as follows:

- Maximum CO concentration
- Minimum combustion chamber temperature
- Maximum pumpable waste derived fuel feed rate
- Maximum total waste derived fuel feed rate
- Maximum chlorine feed
- Maximum production rate
- Maximum ID fan amps

The second operating condition of this Phase was to determine the emissions of the following parameters and System Removal Efficiencies (SRE) for metals while the kiln is at **MAXIMUM PRACTICAL TEMPERATURE**. During this phase triplicate measurements of the following parameters were performed:

- Metals Emissions & SRE (Pb, As, Cr, Be, Cd, Hg and Zn)
- Hexavalent Chromium Emissions & SRE (Cr+6)
- Total Hydrocarbon (THC) emissions
- Carbon Monoxide Emissions
- Oxygen Emissions

The following operating parameters were either minimized or maximized (as appropriate) for the required 1-hour rolling average by the plant operators for this portion of the COC:

- Maximum combustion chamber temperature
- Maximum APCD temperatures (both main and bypass)
- Maximum pumpable waste derived fuel feed rate
- Maximum total waste derived fuel feed ratio
- Maximum metals feed rate (Pb; As, Cr, Be, Cd and Hg)
- Maximum total chlorine feed rate
- Maximum ID fan amps

A material mass balance of the kiln was performed during both Phases for chloride and chlorine in accordance with Part 266.103 (c) (1) Limits on operating conditions. In addition, a metals mass balance was performed during each phase to determine maximum metals input and validate PCC Engineering Judgements. Listed below are the material input and output sample locations.

INPUTS

- Coal feed pipes (2)
- Water for the Conditioning Tower
- Raw material feed to kiln
- Tire feed
- WDLF feed
- WDSF feed
- Metals Spike
- Spent kiln brick (planned for, not available during COC)

OUTPUTS

- Clinker cooler conveyer
- Kiln / Preheater dust
- Bypass baghouse hopper
- Stack/Kiln outlet

2.1 Phase 1

Phase 1 testing was performed on 13 and 14 April 1992 during steady state coal fired kiln operation. Three tests were performed for POHC, particulate and HCl/Cl₂ on 13 April (Tests 2, 3 & 4), and heavy metals on 14 April (Tests 6, 7 & 8). Test #1 was a "Blank Train" performed for QA/QC purposes, as was Test #5. Blank train data are presented in Section 6 of this report. The kiln was operated under normal conditions for these tests, as presented in Section 3.

2.1.1 Particulate, Chloride and Chlorine Emission Measurements

A summary of particulate, chloride (HCl) and chlorine emission measurements from 13 April is presented in Table 2-1. Data presented include: test times, process conditions, stack conditions, sample conditions and measured emissions.

Particulate emissions as measured were less than 0.03 gr/dscf @ 7% O₂ and within limitations set by US EPA (NSPS) and MO DNR, which are stricter than the 0.08 gr/dscf @ 7% O₂ set by the BIF regulation. Opacity, as determined by EPA Method 9 was less than 10% throughout the tests.

Chloride emissions as HCl averaged 406 g/hr, less than 0.1% of the limitation set by the Lone Star Precompliance Certification (PCC) of 502,000 g/hr. Chlorine emissions averaged 157 g/hr, less than 0.5% of the PCC limitation of 28,700 g/hr.

Data summaries including all calculation inputs and outputs are presented in Appendix A, field data in B-1 and laboratory data in C-1. All tests were acceptable with leak rates less than 0.02 cfm and isokinesis at 100% ± 10%.

2.1.2 Chloride Mass Balance

A summary of the chloride mass balance performed during Phase 1 is presented in Table 2-2. Data summaries are presented in Appendix A, field data in B-2 and laboratory data in C-2.

Closure of the balance on a mass input / output basis was good at 100±5%. Total measured chloride input to the system was consistent, averaging approximately 220 lbs/hr for the tests performed in Phase 1. Most Cl⁻ input is attributable to the raw feed.

2.1.3 Heavy Metals Emissions

A summary of heavy metals emissions (Tests 6, 7 & 8; 5 was blank train) is presented in Table 2-3. Please note that no metals spiking was performed during Phase 1. Emissions of heavy metals were well within the limitations set by the PCC. All metals emissions were less than 10% of the PCC limitations, with most measured emissions below 1% of the allowable. No hexavalent chromium testing was performed during Phase 1. Data summaries are presented in Appendix A, field data in B-3 and laboratory data in C-3.

TABLE 2-1
PARTICULATE/ CHLORINE/ HCl DATA SUMMARY
BIF COC TEST PROGRAM - PHASE 1
LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST NO. | 2 CL | 3 CL | 4 CL |
|--|--------------|---------------|---------------|
| DATE: | 4/13/92 | 4/13/92 | 4/13/92 |
| TIME : | 9:24 - 11:31 | 13:08 - 15:13 | 16:55 - 19:00 |
| PROCESS CONDITIONS | | | |
| Raw Feedrate (lbs/hr) | 507400 | 505000 | 507400 |
| Kiln Coal Feedrate (lbs/hr) | 16800 | 16800 | 16800 |
| Pre-Cal Coal Feedrate (lbs/hr) | 24200 | 23800 | 23600 |
| SAMPLE CONDITIONS | | | |
| Volume at STD Conditions (dscf) | 67.2 | 65.0 | 65.1 |
| Particulate Catch (mg) | 74.2 | 81.5 | 64.6 |
| Chlorine Catch (mg) | 0.7 | 0.4 | 0.9 |
| HCl Catch (mg) | 6.1 | 3.6 | 1.5 |
| Isokinesis (%) | 102.6 | 99.2 | 100.6 |
| STACK CONDITIONS | | | |
| Stack Temperature (°F) | 240 | 238 | 239 |
| Moisture (%) | 12.7 | 14.8 | 13.9 |
| Actual Gas Flowrate (acfm) | 397564 | 406747 | 399357 |
| Corrected Gas Flowrate (dscfm) | 260724 | 261101 | 257569 |
| EMISSIONS | | | |
| Particulate Concentration (gr/dscf) | 0.017 | 0.019 | 0.015 |
| Particulate Concentration (gr/dscf @ 7% O ₂) | 0.022 | 0.025 | 0.021 |
| Particulate Emission Rate (lbs/hr) | 38.06 | 43.26 | 33.80 |
| Chlorine Emission Rate (g/hr) | 163 | 95 | 213 |
| Chlorine Emission Rate (g/sec) | 0.045 | 0.026 | 0.059 |
| HCL Emission Rate (g/hr) | 1416 | 863 | 354 |
| HCL Emission Rate (g/sec) | 0.393 | 0.240 | 0.098 |

**TABLE 2-2
CHLORIDE MASS BALANCE
BIF COC TEST PROGRAM/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST #2 | MASS FLOW | % Chloride | Chloride Flow |
|------------------|------------------|-------------------|----------------------|
| FEEDS: | lbs/hr | | lbs/hr |
| Raw Feed | 507400 | 0.035 | 177.6 |
| Raw Feed (H2O) | 14000 | | |
| Coal-Kiln | 16800 | 0.11 | 18.5 |
| Coal-Precalciner | 24200 | 0.09 | 21.8 |
| Quench Water | 63959 | 0.0056 | 3.6 |
| TOTAL: | 626359 | | 221.4 |
| OUTPUTS: | | | |
| Clinker | 324000 | 0.0063 | 20.4 |
| Kiln Dust | 50800 | 0.47 | 238.8 |
| Bypass Dust | 1960 | 0.99 | 19.4 |
| Calcination CO2 | 177590 | | |
| Stack Gas (H2O) | 108752 | | 3.0 |
| TOTAL: | 663102 | | 281.6 |
| % CLOSURE | 105.87 | | 127.17 |
| TEST #3 | MASS FLOW | % Chloride | Chloride Flow |
| FEEDS: | lbs/hr | | lbs/hr |
| Raw Feed | 505000 | 0.035 | 176.8 |
| Raw Feed (H2O) | 14000 | | |
| Coal-Kiln | 16800 | 0.11 | 18.5 |
| Coal-Precalciner | 23800 | 0.09 | 21.4 |
| Quench Water | 65458 | 0.0058 | 3.8 |
| TOTAL: | 625058 | | 220.4 |
| OUTPUTS: | | | |
| Clinker | 322000 | 0.005 | 15.1 |
| Kiln Dust | 50600 | 0.27 | 136.6 |
| Bypass Dust | 1960 | 3.00 | 58.8 |
| Calcination CO2 | 176750 | | |
| Stack Gas (H2O) | 108752 | | 1.8 |
| TOTAL: | 660062 | | 212.4 |
| % CLOSURE | 105.60 | | 96.35 |
| TEST #4 | MASS FLOW | % Chloride | Chloride Flow |
| FEEDS: | lbs/hr | | lbs/hr |
| Raw Feed | 507400 | 0.034 | 172.5 |
| Raw Feed (H2O) | 14000 | | |
| Coal-Kiln | 16800 | 0.11 | 18.5 |
| Coal-Precalciner | 23600 | 0.09 | 21.2 |
| Quench Water | 66957 | 0.0054 | 3.6 |
| TOTAL: | 628757 | | 215.9 |
| OUTPUTS: | | | |
| Clinker | 324000 | 0.0063 | 20.4 |
| Kiln Dust | 50800 | 0.26 | 132.1 |
| Bypass Dust | 1960 | 1.6 | 31.4 |
| Calcination CO2 | 177590 | | |
| Stack Gas (H2O) | 108752 | | 0.8 |
| TOTAL: | 663102 | | 184.6 |
| % CLOSURE | 105.46 | | 85.54 |

**TABLE 2-3
SUMMARY OF METALS EMISSIONS
BIF COC TEST PROGRAM - PHASE 1
LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST NO. | 6 ME | 7 ME | 8 ME | |
|---------------------------------|---------------|---------------|---------------|---------|
| DATE: | 4/14/92 | 4/14/92 | 4/14/92 | |
| TIME : | 11:28 - 14:10 | 16:10 - 18:35 | 20:30 - 22:44 | |
| PROCESS CONDITIONS | | | | |
| Raw Feedrate (lbs/hr) | 517200 | 514800 | 514800 | |
| Kiln Coal Feedrate (lbs/hr) | 17000 | 16600 | 16200 | |
| Pre-Cal Coal Feedrate (lbs/hr) | 24000 | 23800 | 24400 | |
| SAMPLE CONDITIONS | | | | |
| Volume at STD Conditions (dscf) | 67.17 | 68.08 | 67.90 | |
| Isokinesis (%) | 102.87 | 102.31 | 101.44 | |
| STACK CONDITIONS | | | | |
| Stack Temperature (°F) | 238 | 237 | 235 | |
| Moisture (%) | 14.09 | 13.92 | 13.13 | |
| Actual Gas Flowrate (acfm) | 403942 | 411704 | 410029 | |
| Corrected Gas Flowrate (dscfm) | 260019 | 265017 | 266550 | |
| METALS EMISSIONS | | | | |
| Antimony | (ug/Nm3) | 0.273 | 0.467 | 0.343 |
| | (g/hr) | 0.121 | 0.210 | 0.155 |
| Arsenic | (ug/Nm3) | 1.740 | 2.339 | 1.997 |
| | (g/hr) | 0.769 | 1.053 | 0.905 |
| Barium | (ug/Nm3) | 30.912 | 34.437 | 159.661 |
| | (g/hr) | 13.658 | 15.508 | 72.314 |
| Beryllium | (ug/Nm3) | 0.168 | 0.062 | 0.099 |
| | (g/hr) | 0.074 | 0.028 | 0.045 |
| Cadmium | (ug/Nm3) | 0.357 | 0.410 | 0.307 |
| | (g/hr) | 0.158 | 0.185 | 0.139 |
| Chromium | (ug/Nm3) | 16.245 | 15.818 | 36.613 |
| | (g/hr) | 7.177 | 7.123 | 16.583 |
| Lead | (ug/Nm3) | 12.880 | 13.277 | 11.337 |
| | (g/hr) | 5.691 | 5.979 | 5.135 |
| Silver | (ug/Nm3) | 0.100 | 0.104 | 0.120 |
| | (g/hr) | 0.044 | 0.047 | 0.054 |
| Thallium | (ug/Nm3) | 1.178 | 0.773 | 0.754 |
| | (g/hr) | 0.520 | 0.348 | 0.342 |
| Zinc | (ug/Nm3) | 43.424 | 32.362 | 95.173 |
| | (g/hr) | 19.186 | 14.573 | 43.106 |
| Mercury | (ug/Nm3) | 4.274 | 2.899 | 2.897 |
| | (g/hr) | 1.888 | 1.306 | 1.312 |

2.1.4 Metals Mass Balance

A summary of the metals mass balance and System Removal Efficiencies (SRE) is presented in Table 2-4. Please note that no metals spiking was performed. As can be seen, the majority of metals input results from the raw feed material, which can vary greatly. Closure of the mass portion (actual product) of the balance was good at $100\pm 5\%$, but closure of the metals balance was erratic, at best.

Metals analyses were performed on what were ultimately very small samples of massive process streams. Although grab samples were drawn at 15 minute intervals and composited over an entire test period, questionable results still occurred. An analytical variance of 1 ppm when multiplied by a massive flow rate (raw feed) of 500,000 lbs/hr, can result in a mass rate difference of 227 g/hr, which can be a significant factor in a mass balance such as this.

System Removal Efficiencies (SRE) were determined using the total metal input and the stack gas exhaust rate for each metal species. Although no metals spiking was performed during this phase, SRE were typically greater than 99% for all metals except mercury, which was determined at 97%. Data summaries are presented in Appendix A, field data in B-2 and laboratory data in C-4.

2.1.5 POHC Emissions

No POHC spiking was performed during this phase of the test program, as no WDF was fired. Emissions of the surrogate POHC used in Phase 2 were, however, monitored for comparison with emissions while firing spiked waste fuels. Measured emissions of these compounds were in the same range as the emissions measured while firing spiked WDF, which were all measured at or near the lower detection of the sampling and analytical method. Emissions of all POHC were less than 0.6 g/hr.

A summary of measured POHC emissions is presented in Table 2-5. Emissions of surrogate POHC were below analytical detection limits as well as insignificant. Other organic emissions included typical products of incomplete combustion. Data summaries are presented in Appendix A, field data in B-4 and laboratory data in C-5.

2.1.6 Continuous Emission Monitoring of CO, THC and O₂

A summary of CEM data for CO, THC and O₂ is presented in Table 2-6. CEM was performed at the exhaust stack only (not in bypass duct) during Phase 1. CO emissions concentrations, corrected to 7% O₂, ranged from approximately 1000 to 1500 ppm for the 6 tests performed, while THC emissions concentrations ranged from 75 to 125 ppm (dry) corrected to 7% O₂, as propane. No THC data was recorded during Tests 3, 4 and 5 due to instrument problems.

These data are not totally representative of combustion conditions in the kiln, but primarily represent conditions in the pre-calciner, where coal is fired at oxygen conditions and incomplete calcination takes place. Data summaries are presented in Appendix A and field data in B-5.

TABLE 2-4A
MASS BALANCE METALS DATA
BIF COC TEST PROGRAM-PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST #6 | MASS FLOW | Antimony (Sb) | Flow | Arsenic (As) | Flow | Radium (Ra) | Flow | Barium (Ba) | Flow | Strontium (Sr) | Flow | Cadmium (Cd) | Flow |
|-----------------|-----------|---------------|---------|--------------|---------|-------------|----------|-------------|--------|----------------|---------|--------------|------|
| FEEDS | lbs/hr | MG/KG | g/hr | MG/KG | g/hr | MG/KG | g/hr | MG/KG | g/hr | MG/KG | g/hr | MG/KG | g/hr |
| RAW FEED | 517200 | 0.458 | 107.542 | 1.220 | 288.467 | 18.400 | 4555.291 | 0.080 | 18.785 | 0.606 | 142.294 | | |
| RAW FEED (H2O) | 14000 | | | | | | | | | | | | |
| COAL KILN | 17000 | <0.277 | 2.138 | 2.070 | 15.978 | 23.300 | 179.829 | 0.803 | 4.654 | 1.930 | 14.898 | | |
| COAL PRECAL | 24000 | <0.353 | 3.848 | 3.450 | 37.591 | 46.700 | 506.843 | 0.508 | 5.535 | 2.790 | 30.400 | | |
| QUENCH H2O | 86958 | <0.005 | 0.150 | < 0.002 | 0.060 | 0.090 | 2.895 | < 0.0005 | 0.015 | < 0.001 | 0.030 | | |
| TOTAL: | 638158 | 113.88 | 113.88 | | 340.09 | | 5246.66 | | 28.99 | | 187.82 | | |
| CLINGER | 330000 | <0.442 | 68.220 | 1.950 | 292.149 | 51.300 | 7685.766 | 0.468 | 70.116 | 1.400 | 208.748 | | |
| KILN DUST | 61800 | <0.381 | 8.490 | 2.190 | 51.503 | 23.300 | 547.951 | 0.159 | 3.730 | 0.658 | 15.474 | | |
| BYPASS DUST | 1960 | <0.388 | 0.345 | 1.600 | 1.424 | 40.300 | 35.881 | 0.388 | 0.345 | 2.120 | 1.888 | | |
| CALCINATION CO2 | 181020 | | | | | | | | | | | | |
| STACK GAS (H2O) | 102746 | 0.121 | 0.121 | | 0.769 | | 13.658 | | 0.743 | | 0.158 | | |
| TOTAL: | 667528 | 75.18 | 75.18 | | 345.84 | | 8283.24 | | 74.94 | | 227.27 | | |
| % CLOSURE | 104.80 | | 88.13 | | 101.69 | | 157.88 | | 258.53 | | 121.13 | | |
| SRE % | | | 99.894 | | 99.774 | | 99.740 | | 97.436 | | 98.916 | | |
| TEST #7 | | | | | | | | | | | | | |
| FEEDS | | | | | | | | | | | | | |
| RAW FEED (H2O) | 514800 | 0.410 | 95.925 | 1.340 | 313.184 | 19.500 | 4557.524 | 0.104 | 24.307 | 0.832 | 147.711 | | |
| COAL KILN | 18600 | < 0.327 | 2.464 | 1.020 | 7.687 | 15.300 | 115.307 | 0.321 | 2.419 | 1.620 | 12.209 | | |
| COAL PRECAL | 23800 | < 0.398 | 4.279 | 4.290 | 48.354 | 46.200 | 499.200 | 0.460 | 4.970 | 2.610 | 28.202 | | |
| QUENCH H2O | 60457 | < 0.005 | 0.151 | 0.003 | 0.091 | 0.087 | 2.825 | < 0.0005 | 0.015 | < 0.001 | 0.030 | | |
| TOTAL: | 635657 | 102.72 | 102.72 | | 367.32 | | 5174.86 | | 31.71 | | 188.15 | | |
| CLINGER | 328000 | < 0.275 | 40.951 | 2.580 | 384.193 | 49.400 | 7356.253 | 0.467 | 69.542 | 1.350 | 201.031 | | |
| KILN DUST | 51400 | < 0.335 | 7.817 | 1.690 | 39.437 | 23.400 | 546.053 | 0.168 | 3.920 | 0.619 | 14.445 | | |
| BYPASS DUST | 1960 | < 0.305 | 0.271 | 1.790 | 1.593 | 40.400 | 35.950 | 0.396 | 0.352 | 2.810 | 2.500 | | |
| CALCINATION CO2 | 180180 | | | | | | | | | | | | |
| STACK GAS (H2O) | 103458 | 0.210 | 0.210 | | 1.053 | | 15.508 | | 0.028 | | 0.185 | | |
| TOTAL: | 684998 | 49.25 | 49.25 | | 426.28 | | 7953.76 | | 73.84 | | 218.16 | | |
| % CLOSURE | 104.82 | | 47.95 | | 118.05 | | 153.71 | | 232.86 | | 115.95 | | |
| SRE % | | | 99.795 | | 99.713 | | 99.700 | | 99.912 | | 99.902 | | |
| TEST #8 | | | | | | | | | | | | | |
| FEEDS | | | | | | | | | | | | | |
| RAW FEED (H2O) | 514800 | < 0.371 | 86.710 | 1.210 | 282.900 | 18.400 | 4300.433 | 0.128 | 29.449 | 0.476 | 111.250 | | |
| COAL KILN | 14000 | | | | | | | | | | | | |
| COAL PRECAL | 16200 | < 0.335 | 2.464 | 2.740 | 20.152 | 22.900 | 186.425 | 0.817 | 6.009 | 1.870 | 13.753 | | |
| QUENCH H2O | 24000 | < 0.398 | 4.387 | 3.620 | 42.318 | 48.100 | 532.833 | 0.738 | 8.153 | 2.660 | 29.486 | | |
| TOTAL: | 86457 | < 0.005 | 0.151 | 0.004 | 0.121 | 0.094 | 2.836 | < 0.0005 | 0.015 | < 0.001 | 0.030 | | |
| TOTAL: | 635957 | 93.71 | 93.71 | | 345.39 | | 5004.53 | | 43.83 | | 154.50 | | |
| CLINGER | 326000 | < 0.288 | 44.378 | 1.730 | 257.618 | 48.800 | 7288.906 | 0.524 | 78.030 | 1.400 | 208.477 | | |
| KILN DUST | 51400 | < 0.454 | 10.594 | 1.310 | 30.570 | 21.200 | 494.715 | 0.245 | 5.717 | 0.516 | 12.041 | | |
| BYPASS DUST | 1960 | < 0.364 | 0.324 | 1.860 | 1.655 | 37.700 | 33.547 | 0.480 | 0.427 | 2.720 | 2.420 | | |
| CALCINATION CO2 | 180100 | | | | | | | | | | | | |
| STACK GAS (H2O) | 98151 | 0.155 | 0.155 | | 0.905 | | 72.314 | | 0.045 | | 0.139 | | |
| TOTAL: | 859601 | 55.45 | 55.45 | | 290.75 | | 7867.48 | | 84.22 | | 223.08 | | |
| % CLOSURE | 103.75 | | 59.17 | | 84.18 | | 157.21 | | 193.05 | | 144.39 | | |
| SRE % | | | 99.834 | | 99.738 | | 99.555 | | 99.897 | | 99.910 | | |

RESULTS REPORTED IN MGAL

TABLE 2-4B
 MASS BALANCE METALS DATA
 BIF COC TEST PROGRAM-PHASE 1
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

| TEST # | MASS FLOW lb/hr | Chromium (Cr) MO/KG | FLOW g/hr | Lead (Pb) MO/KG | FLOW g/hr | SILVER (Ag) MO/KG | FLOW g/hr | Thallium (Tl) MO/KG | FLOW g/hr | Zinc (Zn) MO/KG | FLOW g/hr | MERCURY (Hg) MO/KG | FLOW g/hr |
|-----------------|--------------------|------------------------|--------------|--------------------|--------------|----------------------|--------------|------------------------|--------------|--------------------|--------------|-----------------------|--------------|
| FEEDS | | | | | | | | | | | | | |
| RAWFEED | 517200 | 5.540 | 1300.841 | 10.500 | 2465.492 | < 0.066 | 15.497 | 0.756 | 177.515 | 12.600 | 2958.591 | 0.260 | 61.050 |
| RAWFEED (H2O) | 14000 | | 74.479 | 9.030 | 69.694 | 0.105 | 0.810 | < 0.111 | 0.957 | 37.800 | 291.740 | 0.167 | 1.289 |
| COAL KLN | 17000 | 9.650 | 90.873 | 11.200 | 122.035 | < 0.071 | 0.774 | < 0.141 | 1.538 | 51.200 | 557.875 | 0.230 | 2.506 |
| COAL PRECAL | 24000 | 8.340 | 91.390 | 0.049 | 1.467 | < 0.001 | 0.030 | < 0.002 | 0.060 | < 0.001 | 0.030 | < 0.001 | 0.030 |
| QUENCH H2O | 65958 | < 0.005 | 1466.34 | | 2656.69 | | 17.11 | | 179.37 | | 3808.24 | | 64.88 |
| TOTAL: | 638158 | | | | | | | | | | | | |
| CLINKER | 330000 | 45.700 | 6846.774 | 12.300 | 1842.786 | < 0.088 | 13.184 | 0.177 | 28.518 | 23.700 | 3550.734 | < 0.090 | 13.484 |
| KLN DUST | 51800 | 7.010 | 164.856 | 21.300 | 500.918 | 0.116 | 2.728 | 45.400 | 1087.681 | 12.300 | 289.262 | 0.415 | 9.760 |
| BYPASS DUST | 1960 | 19.400 | 17.263 | 67.900 | 60.420 | 0.465 | 0.414 | 0.372 | 0.331 | 21.200 | 18.865 | 0.100 | 0.089 |
| CALCINATION CO. | 181020 | | 7.177 | | 5.691 | | 0.044 | | 0.520 | | 19.188 | | 1.888 |
| STACK GAS (H2O) | 102746 | | 7038.07 | | 2409.81 | | 16.37 | | 1085.05 | | 3678.05 | | 25.22 |
| TOTAL: | 687526 | | | | | | | | | | | | |
| %CLOSURE | 104.80 | | 479.84 | | 90.64 | | 95.67 | | 608.47 | | 101.83 | | 36.88 |
| SRE % | | | 99.511 | | 99.786 | | 99.742 | | 99.711 | | 99.496 | | 97.080 |
| TEST #7 | | | | | | | | | | | | | |
| FEEDS | | | | | | | | | | | | | |
| RAWFEED | 514800 | 5.900 | 1378.943 | 30.300 | 7081.692 | < 0.075 | 17.529 | 1.200 | 280.463 | 13.100 | 3081.722 | 0.228 | 53.288 |
| RAWFEED (H2O) | 14000 | | 73.028 | 4.540 | 34.215 | 0.131 | 0.987 | < 0.131 | 0.987 | 43.800 | 330.094 | 0.127 | 0.957 |
| COAL KLN | 16600 | 9.800 | 81.255 | 13.700 | 148.031 | < 0.079 | 0.854 | < 0.158 | 1.707 | 51.300 | 556.488 | 0.121 | 1.307 |
| COAL PRECAL | 23800 | 7.520 | 91.255 | 0.022 | 0.864 | < 0.001 | 0.030 | < 0.002 | 0.060 | 0.001 | 0.030 | 0.005 | 0.151 |
| QUENCH H2O | 68457 | < 0.005 | 1533.38 | | 7264.60 | | 19.40 | | 283.22 | | 3948.31 | | 55.70 |
| TOTAL: | 635657 | | | | | | | | | | | | |
| CLINKER | 328000 | 50.300 | 7490.274 | 14.000 | 2084.768 | < 0.055 | 8.190 | < 0.110 | 16.380 | 18.700 | 2764.654 | < 0.088 | 12.806 |
| KLN DUST | 51400 | 7.760 | 181.084 | 24.300 | 567.055 | 0.107 | 2.497 | 46.500 | 1085.105 | 18.800 | 496.709 | 0.335 | 7.817 |
| BYPASS DUST | 1980 | 18.100 | 16.106 | 109.000 | 96.993 | 0.648 | 0.575 | 0.457 | 0.407 | 24.700 | 21.979 | < 0.078 | 0.089 |
| CALCINATION CO. | 180180 | | 7.123 | | 5.979 | | 0.047 | | 0.348 | | 14.573 | | 1.308 |
| STACK GAS (H2O) | 103456 | | 7694.59 | | 2754.79 | | 11.31 | | 1102.24 | | 3259.92 | | 22.00 |
| TOTAL: | 664998 | | | | | | | | | | | | |
| %CLOSURE | 104.62 | | 501.81 | | 37.92 | | 58.29 | | 389.18 | | 82.56 | | 39.49 |
| SRE % | | | 99.535 | | 99.918 | | 99.759 | | 99.877 | | 99.631 | | 97.656 |
| TEST #8 | | | | | | | | | | | | | |
| FEEDS | | | | | | | | | | | | | |
| RAWFEED | 514800 | 5.870 | 1371.932 | 14.700 | 3435.672 | 40.100 | 9372.140 | 2.210 | 516.519 | 9.200 | 2150.217 | 0.473 | 110.549 |
| RAWFEED (H2O) | 14000 | | 67.591 | 8.250 | 60.677 | 0.080 | 0.688 | < 0.134 | 0.988 | 52.900 | 389.069 | 0.119 | 0.875 |
| COAL KLN | 16200 | 9.190 | 91.390 | 1.240 | 13.738 | < 0.079 | 0.875 | < 0.158 | 1.750 | 55.002 | 609.268 | 0.136 | 1.507 |
| COAL PRECAL | 24400 | 8.290 | 91.390 | < 0.004 | 0.121 | < 0.001 | 0.030 | < 0.002 | 0.060 | 0.002 | 0.060 | 0.0004 | 0.012 |
| QUENCH H2O | 68457 | < 0.005 | 1531.06 | | 3510.21 | | 9973.63 | | 519.32 | | 3148.61 | | 112.94 |
| TOTAL: | 635657 | | | | | | | | | | | | |
| CLINKER | 328000 | 48.100 | 7162.667 | 15.700 | 2337.918 | 0.077 | 11.466 | < 0.119 | 17.721 | 23.600 | 3514.323 | < 0.083 | 12.360 |
| KLN DUST | 51400 | 6.960 | 162.416 | 21.500 | 501.715 | 0.118 | 2.754 | 58.900 | 1374.467 | 23.500 | 595.056 | 0.275 | 6.417 |
| BYPASS DUST | 1980 | 16.200 | 16.195 | 105.000 | 93.433 | 0.837 | 0.745 | 0.582 | 0.518 | 28.400 | 25.271 | < 0.079 | 0.070 |
| CALCINATION CO. | 180180 | | 16.583 | | 5.135 | | 0.054 | | 0.342 | | 43.106 | | 1.312 |
| STACK GAS (H2O) | 859691 | | 7357.66 | | 2938.20 | | 15.02 | | 1393.05 | | 4177.78 | | 20.16 |
| TOTAL: | 659691 | | | | | | | | | | | | |
| %CLOSURE | 103.75 | | 400.57 | | 63.70 | | 0.16 | | 268.25 | | 192.60 | | 17.85 |
| SRE % | | | 98.917 | | 99.854 | | 99.999 | | 99.934 | | 98.631 | | 99.638 |

* RESULTS REPORTED IN MO/KG

TABLE 2-5
POHC EMISSION SUMMARY
BIF COC TEST PROGRAM - PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
13-Apr-92

| | Perchloroethylene | Trichlorotrifluoromethane | 1,1,2 Trichloroethane | 1,1,1 Trichloroethane |
|--------------------------|-------------------|---------------------------|-----------------------|-----------------------|
| TEST #2 9:25 - 12:48 | <0.571 | <0.571 | <0.571 | <0.571 |
| TEST #3 13:08 - 16:20 | <0.596 | <0.596 | <0.596 | <0.596 |
| TEST #4 16:55 - 20:06 | <0.583 | <0.583 | <0.583 | <0.583 |

TABLE 2-6
APCC CEM DATA SUMMARY
BACKGROUND TEST/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Apr-92

| TEST NO. DATE | TIME | | CO (ppm) | THC (ppm) | OXYGEN (%) | CO2 (%) | CO @ 7% O2 (ppm) | THC @ 7% O2 (ppm) |
|--------------------|-------|-------|-------------|--------------|---------------|------------|---------------------|----------------------|
| | From | To | | | | | | |
| Test #2 4/13/92 | 9:25 | 12:48 | 849 | - | 10.3 | 17.7 | 1113 | - |
| Test #3 4/13/92 | 13:08 | 16:20 | 759 | - | 10.2 | 17.5 | 986 | - |
| Test #4 4/13/92 | 16:55 | 20:06 | 746 | - | 10.5 | 17.7 | 997 | - |
| Test #6 4/14/92 | 11:28 | 14:05 | 1182 | 76.1 | 10.2 | 17.8 | 1535 | 99 |
| Test #7 4/14/92 | 16:11 | 18:35 | 1016 | 56.2 | 10.6 | 17.5 | 1371 | 76 |
| Test #8 4/14/92 | 20:33 | 22:48 | 1038 | 64.1 | 10.6 | 17.2 | 1401 | 87 |

2.2 Phase 2

Phase 2 testing was performed on 25 and 26 June 1992. Three tests were performed for POHC, particulate and HCl/Cl₂ (Tests 3, 4 & 5) on 25 June, and heavy metals (Tests 7, 8 & 9) on 26 June. The blank trains for this series of tests were Tests 1 & 6. Test 2 was voided due to a thunder storm which forced personnel from the stack. The kiln was operated under near upset conditions while still producing saleable product as discussed above in order to set operational limitations.

2.2.1 Particulate, Chloride and Chlorine Emission Measurements

A summary of particulate, chloride (HCl) and chlorine emission measurements from 25 June is presented in Table 2-7. Data presented include: test times, process conditions, stack conditions, sample conditions and measured emissions.

Particulate emissions as measured were less than 0.03 gr/dscf @ 7% O₂ and within limitations set by US EPA (NSPS) and MO DNR, which are stricter than the 0.08 gr/dscf @ 7% O₂ set by the BIF regulation. Emissions were almost identical to those measured during the background test in Phase 1. This result was expected, as the majority of particulate emissions result from the raw mill and preheater tower, and not the kiln.

Chloride emissions as HCl averaged 4760 g/hr, higher than the background test but still less than 1% of the limitation set by the Lone Star Precompliance Certification of 502,000 g/hr. Chlorine emissions averaged 47 g/hr, less than 0.1% of the PCC limitation of 28,700 g/hr.

Data summaries including all calculation inputs and outputs are presented in Appendix A, field data in B-1 and laboratory data in C-1. All tests were acceptable with leak rates less than 0.02 cfm and isokinesis at 100% ± 10%.

2.2.2 Chloride Mass Balance

A summary of the chloride mass balance performed during Phase 2 is presented in Table 2-8A and 2-8B. Data summaries are presented in Appendix A, field data in B-2 and laboratory data in C-2.

Closure of the balance on a mass input / output basis was good at 100±5%. Total chloride into the system was consistent, ranging from 1200 to 1350 lbs/hr for the 6 tests performed in Phase 2.

2.2.3 Heavy Metals Emissions

A summary of heavy metals emissions and System Removal Efficiencies (SRE) is presented in Table 2-9. Emissions of heavy metals were all within the limitations set by the PCC. Data summaries are presented in Appendix A, field data in B-3 and laboratory data in C-3.

**TABLE 2-7
PARTICULATE/CHLORINE/HCl DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST NO. | 3-CL | 4-CL | 5-CL |
|----------|------------|-------------|-------------|
| DATE: | 6/25/92 | 6/25/92 | 6/25/92 |
| TIME : | 8:38-10:46 | 17:50-19:56 | 22:02-00:10 |

PROCESS CONDITIONS

| | | | |
|------------------------|--------|--------|--------|
| Raw Feedrate (lbs/hr) | 469200 | 484800 | 482000 |
| Coal Feedrate (lbs/hr) | 23680 | 24160 | 23280 |
| WDLF Feedrate (lbs/hr) | 20448 | 20016 | 20064 |
| WDSF Feedrate (lbs/hr) | 859 | 998 | 907 |
| Tires (lbs/hr) | 3000 | 3000 | 3000 |

SAMPLE CONDITIONS

| | | | |
|---------------------------------|-------|-------|-------|
| Volume at STD Conditions (dscf) | 67.3 | 68.6 | 68.7 |
| Particulate Catch (mg) | 82.5 | 77.3 | 74.1 |
| Chlorine Catch (mg) | 0.1 | 0.2 | 0.3 |
| HCl Catch (mg) | 15.3 | 17.3 | 28.3 |
| Isokinesis (%) | 103.3 | 104.6 | 105.5 |

STACK CONDITIONS

| | | | |
|--------------------------------|--------|--------|--------|
| Stack Temperature (°F) | 246 | 246 | 242 |
| Moisture (%) | 14.8 | 14.6 | 14.6 |
| Actual Gas Flowrate (acfm) | 422041 | 433547 | 427157 |
| Corrected Gas Flowrate (dscfm) | 262015 | 269655 | 267690 |

EMISSIONS

| | | | |
|--|-------|-------|-------|
| Particulate Concentration (gr/dscf) | 0.02 | 0.02 | 0.02 |
| Particulate Concentration (gr/dscf @ 7% O ₂) | 0.026 | 0.024 | 0.023 |
| Particulate Emission Rate (lbs/hr) | 42.48 | 40.13 | 38.15 |
| Chlorine Emission Rate (g/hr) | 23.38 | 47.14 | 70.12 |
| Chlorine Emission Rate (g/sec) | 0.006 | 0.013 | 0.019 |
| HCL Emission Rate (g/hr) | 3577 | 4077 | 6615 |
| HCL Emission Rate (g/sec) | 0.994 | 1.133 | 1.837 |

**TABLE 2-8A
CHLORIDE MASS BALANCE
BIF COC TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES INC.
CAPE GIRARDEAU, MISSOURI
Jun-92**

| TEST #3 | MASS FLOW | % Chloride | Chloride Flow |
|------------------|---------------|------------|---------------|
| FEEDS: | lbs/hr | | lbs/hr |
| Raw Feed | 469200 | 0.045 | 211.1 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 23680 | 0.11 | 26.0 |
| Quench Water | 67460 | 0.0031 | 2.1 |
| Tires | 3000 | 0.11 | 3.3 |
| WDSF | 859 | 0.12 | 1.0 |
| WDLF | 20448 | 4.82 | 985.6 |
| Spike Material | | | |
| TOTAL: | 598647 | | 1229.2 |
| OUTPUTS: | | | |
| Clinker | 298854 | 0.200 | 597.7 |
| Kiln Dust | 46920 | 0.31 | 145.5 |
| Bypass Dust | 6000 | 7.4 | 444.0 |
| Calcination CO2 | 164220 | | |
| Stack Gas (H2O) | 108752 | | 7.7 |
| TOTAL: | 624746 | | 1194.8 |
| % CLOSURE | 104.36 | | 97.20 |
| TEST #4 | | | |
| FEEDS: | | | |
| Raw Feed | 484800 | 0.049 | 237.6 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 24160 | 0.09 | 21.7 |
| Quench Water | 67460 | 0.0033 | 2.2 |
| Tires | 3000 | 0.10 | 3.0 |
| WDSF | 998 | 0.20 | 2.0 |
| WDLF | 20016 | 4.65 | 930.7 |
| Spike Material | | | |
| TOTAL: | 614434 | | 1197.3 |
| OUTPUTS: | | | |
| Clinker | 308790 | 0.093 | 287.2 |
| Kiln Dust | 48480 | 0.29 | 140.6 |
| Bypass Dust | 6000 | 10.0 | 600.0 |
| Calcination CO2 | 169680 | | |
| Stack Gas (H2O) | 110411 | | 8.8 |
| TOTAL: | 643361 | | 1036.5 |
| % CLOSURE | 104.71 | | 86.57 |
| TEST #5 | | | |
| FEEDS: | | | |
| Raw Feed | 482000 | 0.051 | 245.8 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 23280 | 0.08 | 18.6 |
| Quench Water | 67460 | 0.0035 | 2.4 |
| Tires | 3000 | 0.14 | 4.2 |
| WDSF | 907 | 0.24 | 2.2 |
| WDLF | 20064 | 4.58 | 918.0 |
| Spike Material | | | |
| TOTAL: | 610711 | | 1192.1 |
| OUTPUTS: | | | |
| Clinker | 307006 | 0.140 | 429.8 |
| Kiln Dust | 48200 | 0.30 | 144.6 |
| Bypass Dust | 6000 | 9.3 | 558.0 |
| Calcination CO2 | 168700 | | |
| Stack Gas (H2O) | 109606 | | 14.2 |
| TOTAL: | 639512 | | 1146.6 |
| % CLOSURE | 104.72 | | 96.18 |

TABLE 2-3B
CHLORIDE MASS BALANCE
BIF COC TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST #7 | MASS FLOW | % Chloride | Chloride Flow |
|------------------|---------------|------------|---------------|
| FEEDS: | lbs/hr | | lbs/hr |
| Raw Feed | 501600 | 0.052 | 260.8 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 24480 | 0.11 | 26.9 |
| Quench Water | 67460 | 0.0032 | 2.2 |
| Tires | 3000 | 0.12 | 3.6 |
| WDSF | 273 | 0.17 | 0.5 |
| WDLF | 20424 | 4.55 | 929.3 |
| Spike Material | 21 | | |
| TOTAL: | 631258 | | 1223.3 |
| OUTPUTS: | | | |
| Clinker | 319490 | 0.110 | 351.4 |
| Kiln Dust | 50160 | 0.33 | 165.5 |
| Bypass Dust | 6000 | 14.0 | 840.0 |
| Calcination CO2 | 175560 | | |
| Stack Gas (H2O) | 106567 | | |
| TOTAL: | 657777 | | 1357.0 |
| % CLOSURE | 104.20 | | 110.93 |
| TEST #8 | | | |
| FEEDS: | | | |
| Raw Feed | 502200 | 0.058 | 291.3 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 25060 | 0.10 | 25.1 |
| Quench Water | 67460 | 0.0039 | 2.6 |
| Tires | 3000 | 0.19 | 5.7 |
| WDSF | 273 | 0.14 | 0.4 |
| WDLF | 20770 | 4.50 | 934.7 |
| Spike Material | 22 | | |
| TOTAL: | 632785 | | 1259.7 |
| OUTPUTS: | | | |
| Clinker | 319873 | 0.047 | 150.3 |
| Kiln Dust | 50220 | 0.29 | 145.6 |
| Bypass Dust | 6000 | 18.0 | 1080.0 |
| Calcination CO2 | 175770 | | |
| Stack Gas (H2O) | 106002 | | 9.0 |
| TOTAL: | 657865 | | 1385.0 |
| % CLOSURE | 103.96 | | 109.95 |
| TEST #9 | | | |
| FEEDS: | | | |
| Raw Feed | 502200 | 0.052 | 261.1 |
| Raw Feed (H2O) | 14000 | | |
| Coal | 23680 | 0.11 | 26.0 |
| Quench Water | 67460 | 0.0036 | 2.4 |
| Tires | 3000 | 0.27 | 8.1 |
| WDSF | 398 | 0.28 | 1.1 |
| WDLF | 20774 | 5.07 | 1053.2 |
| Spike Material | 22 | | |
| TOTAL: | 631534 | | 1352.1 |
| OUTPUTS: | | | |
| Clinker | 319873 | 0.050 | 159.9 |
| Kiln Dust | 50220 | 0.27 | 136.6 |
| Bypass Dust | 6000 | 17.0 | 1020.0 |
| Calcination CO2 | 175770 | | |
| Stack Gas (H2O) | 103374 | | |
| TOTAL: | 655237 | | 1315.5 |
| % CLOSURE | 103.75 | | 97.30 |

TABLE 2-9
SUMMARY OF METALS EMISSIONS
CERTIFICATION OF COMPLIANCE TEST/PHASE2
LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

Mechanical
in Case

| TEST NO. | 7-ME | 8-ME | 9-ME |
|---------------------------------|-------------|-------------|-------------|
| DATE: | 6/26/92 | 6/26/92 | 6/26/92 |
| TIME: | 13:51-16:01 | 18:08-20:20 | 21:54-00:03 |
| PROCESS CONDITIONS | | | |
| Raw Feedrate (lbs/hr) | 501600 | 502200 | 502200 |
| Raw Feedrate (lbs/hr) | 24480 | 25060 | 23680 |
| WDLF Feedrate (lbs/hr) | 20424 | 20770 | 20774 |
| WDSF Feedrate (lbs/hr) | 273 | 273 | 398 |
| Tires (lbs/hr) | 3000 | 3000 | 3000 |
| SAMPLE CONDITIONS | | | |
| Volume at STD Conditions (dscf) | 58.39 | 61.04 | 61.06 |
| Isokinesis (%) | 102.32 | 103.55 | 106.22 |
| STACK CONDITIONS | | | |
| Stack Temperature (F) | 310 | 310 | 310 |
| Moisture (%) | 16.21 | 15.62 | 15.61 |
| Actual Gas Flowrate (acfm) | 417,600 | 428,400 | 417,700 |
| Corrected Gas Flowrate (dscfm) | 234,600 | 242,300 | 236,300 |
| METALS EMISSIONS | | | |
| Arsenic (ug/Nm3) | 1.597 | 2.493 | 2.417 |
| (g/hr) | 0.640 | 1.030 | 0.970 |
| SRE (%) | 99.97 | 99.97 | 99.96 |
| Beryllium (ug/Nm3) | 0.060 | 0.058 | 0.168 |
| (g/hr) | 0.020 | 0.020 | 0.070 |
| SRE (%) | 99.57 | 99.63 | 99.58 |
| Cadmium (ug/Nm3) | 2.068 | 17.477 | 0.057 |
| (g/hr) | 0.820 | 7.200 | 0.020 |
| SRE (%) | 99.98 | 99.97 | 99.97 |
| Chromium (ug/Nm3) | 13.722 | 0.058 | 0.058 |
| (g/hr) | 5.470 | 0.020 | 0.020 |
| SRE (%) | 99.95 | 99.95 | 99.94 |
| Lead (ug/Nm3) | 15.917 | 13.705 | 32.223 |
| (g/hr) | 6.340 | 5.640 | 12.940 |
| SRE (%) | 99.92 | 99.93 | 99.93 |
| Zinc (ug/Nm3) | 32.426 | 0.058 | 22.334 |
| (g/hr) | 12.920 | 0.020 | 8.970 |
| SRE (%) | 99.94 | 99.96 | 99.94 |
| Mercury (ug/Nm3) | 45.441 | 39.877 | 144.799 |
| (g/hr) | 18.110 | 16.420 | 58.140 |
| SRE (%) | 84.26 | 86.28 | 86.50 |
| Chrome 6+ (ug/Nm3) | 0.409 | 0.408 | 0.405 |
| (g/hr) | 0.160 | 0.170 | 0.160 |

Although metals inputs to the system were significantly greater in Phase 2, emissions were typically in the same order of magnitude as in Phase 1. Please note that metals spiking was performed during these tests in order to maximize metals input. Emissions of heavy metals were well within the limitations set by the PCC. All metals emissions were less than 10% of the PCC limitations, with most measured emissions below 1% of the allowable. Hexavalent chromium testing was performed during Phase 2.

2.2.4 Metals Mass Balance

A summary of the metals mass balance performed and System Removal Efficiencies (SRE) is presented in Table 2-10A&B. Please note that metals spiking was performed, and as can be seen, the majority of metals input now results from the WDF. Closure of the mass portion (actual product) of the balance was good at 100%±5%, but closure of the metals balance was erratic, at best.

Changes in input mass rates of metals require the kiln system to reach equilibrium before those changes are accurately reflected in the output. This is most likely reason for lack of closure in the metals portion of the mass balance equation.

System Removal Efficiencies (SRE) were determined using the total metal input and the stack gas exhaust rate for each metal species. SRE were typically greater than 99% for all metals except mercury, which was determined at 84% to 86%. Data summaries are presented in Appendix A, field data in B-2 and laboratory data in C-4.

2.2.5 POHC Emissions

POHC spiking was performed during this phase of the test program in the WDLF fired. Surrogate POHC were perchloroethylene, trichlorofluoromethane, 1,2 trichloroethane and 1,1,1 trichloroethane. A summary of DRE measurements is presented in Table 2-11. DRE was greater than 99.99% for all four surrogates used.

Laboratory detection of POHC was acceptable for all tests with the exception of Test 4 for perchloroethylene, where none was detected in the spiked fuel sample. As all other surrogates were present, it is hypothesized that a laboratory interference or error is responsible for this anomaly. Subsequent analysis of the split sample retained on site resulted in the low, but measureable level presented.

The determination of acceptable DRE for the four compounds indicates the acceptability of the Lone Star kiln to fire any and all compounds permitted with DRE at least 99.99%.

Emissions of surrogate POHC were similar to those measured during Phase 1 (at lower detection limits of the method) and were insignificant. Other organic emissions included typical products of incomplete combustion. Data summaries are presented in Appendix A-11, field data in B-4 and laboratory data in C-5.

TABLE 2-10A
 MASS BALANCE METALS DATA
 CERTIFICATION OF COMPLIANCE TEST/PHASE 2
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

| TEST #7 | MASS FLOW lbs/hr | Silver (Ag) mg/kg | Flow g/hr | Arsenic (As) mg/kg | Flow g/hr | Barium (Ba) mg/kg | Flow g/hr | Beryllium (Be) mg/kg | Flow g/hr | Cadmium (Cd) mg/kg | Flow g/hr |
|----------------|---------------------|----------------------|--------------|-----------------------|--------------|----------------------|--------------|-------------------------|--------------|-----------------------|--------------|
| FEEDS | 501600 | 0.665 | 151.44 | 0.754 | 173.98 | 14.100 | 3210.94 | 0.517 | 117.73 | 3.510 | 799.32 |
| RAW FEED (H2O) | 14000 | 0.489 | 5.43 | 5.460 | 60.68 | 60.700 | 674.61 | 0.331 | 3.68 | 0.237 | 2.60 |
| COAL PRECAL | 24480 | 0.007 | 0.21 | 0.005 | 0.15 | 0.104 | 3.19 | 0.004 | 0.12 | 0.001 | 0.03 |
| CUENCHH2O | 67480 | 0.460 | 0.63 | 0.959 | 1.31 | 13.200 | 17.98 | 0.053 | 0.07 | 1.820 | 2.48 |
| TRES | 3000 | 6.190 | 0.77 | 8.260 | 1.02 | 309.000 | 36.30 | 0.196 | 0.02 | 1.280 | 0.16 |
| WDSF | 20424 | 3.670 | 34.03 | 200.000 | 1854.52 | 912.000 | 8458.52 | 2.400 | 22.25 | 289.000 | 2879.75 |
| WOLF | 21 | | | | | | | | | | |
| SPIKE | 21 | | | | | | | | | | |
| TOTAL | 631278 | | 192.51 | 2091.65 | 12401.54 | | | 143.89 | | | 3484.37 |
| CLINKER | 319490 | 0.540 | 78.33 | 15.500 | 2248.25 | 56.400 | 8180.73 | 0.830 | 120.39 | 3.270 | 474.31 |
| FLY DUST | 50160 | 0.364 | 8.29 | 2.220 | 50.56 | 14.700 | 334.76 | 0.210 | 4.78 | 3.640 | 82.89 |
| BYPASS DUST | 6000 | 2.520 | 6.86 | 18.100 | 49.30 | 55.300 | 150.64 | 0.528 | 1.44 | 346.000 | 942.50 |
| CALCINE CO2 | 175580 | | 0.00 | 0.64 | 0.64 | | 0.00 | 0.02 | 0.02 | | 0.82 |
| STACK GAS H2O | 106567 | | 93.48 | 2346.75 | 8665.13 | | | 126.83 | | | 1500.52 |
| TOTAL | 657777 | | 48.56 | 112.29 | 69.88 | | | 88.01 | | | 43.05 |
| % CLOSURE | 104.20 | | | | | | | 99.57 | | | 99.96 |
| SEE % | | | | | | | | | | | |
| TEST #8 | MASS FLOW lbs/hr | Silver (Ag) mg/kg | Flow g/hr | Arsenic (As) mg/kg | Flow g/hr | Barium (Ba) mg/kg | Flow g/hr | Beryllium (Be) mg/kg | Flow g/hr | Cadmium (Cd) mg/kg | Flow g/hr |
| FEEDS | 502200 | 0.411 | 93.73 | 1.430 | 328.04 | 12.400 | 2827.19 | 0.608 | 138.62 | 1.590 | 362.52 |
| RAW FEED (H2O) | 14000 | 0.546 | 6.21 | 3.950 | 44.94 | 51.500 | 585.93 | 0.580 | 6.80 | 0.175 | 1.99 |
| COAL PRECAL | 25060 | 0.007 | 0.21 | 0.001 | 0.02 | 0.100 | 3.06 | 0.004 | 0.12 | 0.001 | 0.03 |
| CUENCHH2O | 67480 | 0.685 | 0.99 | 3.660 | 4.98 | 20.200 | 27.51 | 0.081 | 0.11 | 16.800 | 22.61 |
| TRES | 3000 | 0.503 | 0.06 | 6.660 | 0.83 | 388.000 | 45.61 | 0.237 | 0.03 | 2.060 | 0.26 |
| WDSF | 273 | 3.940 | 37.15 | 185.000 | 1744.47 | 826.000 | 7786.83 | 2.420 | 22.82 | 280.000 | 2640.28 |
| WOLF | 20770 | | | | | | | | | | 220.00 |
| SPIKE | 22 | | | | | | | | | | 3247.69 |
| TOTAL | 632785 | | 198.30 | 2121.28 | 11278.13 | | | 168.30 | | | 650.60 |
| CLINKER | 319873 | 0.444 | 64.40 | 16.500 | 2396.17 | 60.200 | 8742.38 | 0.771 | 111.97 | 4.480 | 650.60 |
| FLY DUST | 50220 | 0.475 | 10.83 | 2.480 | 56.54 | 15.300 | 348.84 | 0.219 | 4.98 | 5.030 | 114.68 |
| BYPASS DUST | 6000 | 4.270 | 11.83 | 16.800 | 45.76 | 60.800 | 220.10 | 0.449 | 1.22 | 501.000 | 1364.72 |
| CALCINE CO2 | 175770 | | 0.00 | 1.03 | 1.03 | | 0.00 | 0.02 | 0.02 | | 7.20 |
| STACK GAS H2O | 103374 | | 86.94 | 2499.51 | 9311.32 | | | 118.20 | | | 2137.20 |
| TOTAL | 659237 | | 62.66 | 117.83 | 82.56 | | | 70.23 | | | 65.81 |
| % CLOSURE | 103.55 | | | | | | | 99.63 | | | 99.97 |
| SEE % | | | | | | | | | | | |
| TEST #9 | MASS FLOW lbs/hr | Silver (Ag) mg/kg | Flow g/hr | Arsenic (As) mg/kg | Flow g/hr | Barium (Ba) mg/kg | Flow g/hr | Beryllium (Be) mg/kg | Flow g/hr | Cadmium (Cd) mg/kg | Flow g/hr |
| FEEDS | 502200 | 0.408 | 93.02 | 0.754 | 171.91 | 11.400 | 2589.19 | 0.536 | 122.21 | 1.330 | 303.24 |
| RAW FEED (H2O) | 14000 | 0.535 | 5.75 | 3.190 | 34.29 | 70.800 | 761.15 | 0.254 | 2.73 | 0.242 | 2.60 |
| COAL PRECAL | 23680 | 0.007 | 0.21 | 0.002 | 0.06 | 0.109 | 3.34 | 0.002 | 0.06 | 0.001 | 0.03 |
| CUENCHH2O | 67480 | 0.664 | 0.93 | 1.070 | 1.46 | 6.430 | 8.76 | 0.099 | 0.13 | 35.100 | 47.81 |
| TRES | 3000 | 0.495 | 0.09 | 15.200 | 2.75 | 356.000 | 64.33 | 0.269 | 0.05 | 2.470 | 0.45 |
| WDSF | 398 | 3.130 | 29.52 | 168.000 | 1584.47 | 490.210 | 4826.36 | 2.590 | 24.43 | 277.000 | 2612.50 |
| WOLF | 20774 | | | | | | | | | | 218.75 |
| SPIKE | 22 | | | | | | | | | | 3185.37 |
| TOTAL | 631534 | | 129.53 | 1794.95 | 8060.12 | | | 149.61 | | | 593.96 |
| CLINKER | 319073 | 0.440 | 63.90 | 17.900 | 2599.48 | 63.900 | 9279.71 | 0.894 | 129.83 | 4.050 | 593.96 |
| FLY DUST | 50220 | 0.559 | 12.75 | 3.120 | 71.14 | 16.700 | 380.70 | 0.296 | 6.75 | 4.320 | 90.50 |
| BYPASS DUST | 6000 | 4.230 | 11.52 | 17.800 | 48.49 | 62.200 | 223.91 | 0.551 | 1.50 | 457.000 | 1272.11 |
| CALCINE CO2 | 175770 | | 0.00 | 0.97 | 0.97 | | 0.00 | 0.07 | 0.07 | | 1964.58 |
| STACK GAS H2O | 103374 | | 88.17 | 2720.07 | 9084.38 | | | 138.15 | | | 61.68 |
| TOTAL | 655237 | | 60.07 | 151.54 | 122.63 | | | 92.34 | | | 69.90 |
| % CLOSURE | 103.75 | | | | | | | 99.90 | | | 99.97 |
| SEE % | | | | | | | | | | | |

TABLE 2-108
MASS BALANCE METALS DATA
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST #7 | MASS FLOW lbs/hr | Chromium (Cr) mg/kg | Flow g/hr | Mercury (Hg) mg/kg | Flow g/hr | Lead (Pb) mg/kg | Flow g/hr | Antimony (Sb) mg/kg | Flow g/hr | Thallium (Tl) mg/kg | Flow g/hr | Zinc (Zn) mg/kg | Flow g/hr |
|----------------|---------------------|------------------------|--------------|-----------------------|--------------|--------------------|--------------|------------------------|--------------|------------------------|--------------|--------------------|--------------|
| FEEDS | 501600 | 16.700 | 4258.46 | 0.414 | 94.28 | 6.890 | 2024.49 | 0.295 | 87.18 | 4.760 | 1063.98 | 20.300 | 4622.85 |
| RAW FEED | 14000 | 16.600 | 184.49 | 0.205 | 2.28 | 6.300 | 70.02 | 0.383 | 4.26 | 0.727 | 8.08 | 53.400 | 593.48 |
| RAW FEED (H2O) | 24480 | 0.150 | 4.60 | 0.004 | 0.12 | 0.008 | 0.25 | 0.005 | 0.15 | 0.002 | 0.06 | 0.066 | 2.02 |
| COAL PRECAL | 67400 | 4.830 | 6.58 | 0.094 | 10.800 | 14.71 | 7.900 | 10.76 | 0.14 | 0.105 | 0.14 | 5594.000 | 7005.41 |
| QUENCHH2O | 3000 | 204.000 | 25.28 | 9.710 | 1.20 | 85.500 | 2.430 | 2.430 | 0.30 | 6.270 | 0.03 | 837.000 | 78.95 |
| TIRES | 273 | 612.000 | 5674.77 | 1.840 | 17.06 | 595.000 | 5517.14 | 19.050 | 176.64 | 0.109 | 1.01 | 951.000 | 8818.14 |
| WDSF | 20424 | | 825.71 | | | | | | | | | | |
| WOLF | 21 | | | | | | | | | | | | |
| SPIKE | 631278 | | 10979.91 | | 115.07 | | 7634.71 | | 259.29 | | 1090.31 | | 21720.85 |
| TOTAL | | | | | | | | | | | | | |
| CLINKER | 319490 | 39.700 | 5758.42 | 0.088 | 12.76 | 23.800 | 3452.15 | 0.389 | 58.42 | 0.179 | 25.96 | 92.800 | 13460.50 |
| KILN DUST | 50180 | 6.550 | 194.71 | 0.524 | 14.21 | 19.400 | 441.79 | 0.274 | 6.24 | 49.200 | 1120.41 | 26.300 | 598.92 |
| BYPASS DUST | 6000 | 32.200 | 87.71 | 0.093 | 0.25 | 685.000 | 1865.94 | 0.767 | 2.09 | 1.850 | 4.60 | 113.000 | 307.81 |
| CALCINE CO2 | 175580 | | 5.47 | | 18.11 | | 6.34 | | 0.00 | | 0.00 | | 12.92 |
| STACK GAS H2O | 106587 | | 6046.31 | | 45.34 | | 5766.22 | | 64.75 | | 1150.98 | | 14380.15 |
| TOTAL | 65777 | | | | | | | | | | | | |
| % CLOSURE | 104.20 | | 55.07 | | 39.40 | | 75.53 | | 24.97 | | 105.28 | | 86.20 |
| SRE % | | | 99.95 | | 84.28 | | 99.92 | | | | | | 99.94 |
| TEST #8 | MASS FLOW lbs/hr | Chromium (Cr) mg/kg | Flow g/hr | Mercury (Hg) mg/kg | Flow g/hr | Lead (Pb) mg/kg | Flow g/hr | Antimony (Sb) mg/kg | Flow g/hr | Thallium (Tl) mg/kg | Flow g/hr | Zinc (Zn) mg/kg | Flow g/hr |
| FEEDS | 502200 | 20.400 | 4851.16 | 0.510 | 116.28 | 14.800 | 3328.78 | 0.281 | 64.07 | 3.940 | 896.32 | 20.900 | 4785.17 |
| RAW FEED | 14000 | 15.700 | 178.62 | 0.076 | 0.89 | 5.500 | 63.40 | 0.302 | 3.44 | 0.671 | 7.63 | 46.100 | 524.49 |
| RAW FEED (H2O) | 25080 | 0.283 | 8.87 | 0.004 | 0.12 | 0.009 | 0.28 | 0.005 | 0.15 | 0.002 | 0.06 | 0.062 | 1.90 |
| COAL PRECAL | 67400 | 56.800 | 77.38 | 0.098 | 31.200 | 42.49 | 6.530 | 6.530 | 8.89 | 0.162 | 0.22 | 16200.000 | 22004.40 |
| QUENCHH2O | 3000 | 187.000 | 23.18 | 9.840 | 1.22 | 54.600 | 6.77 | 1.750 | 0.22 | 0.525 | 0.07 | 658.000 | 81.55 |
| TIRES | 273 | 605.000 | 5704.90 | 1.420 | 13.39 | 611.000 | 5761.47 | 11.650 | 109.85 | 0.123 | 1.16 | 441.000 | 4158.44 |
| WDSF | 20770 | | 825.71 | | | | 303.14 | | 907.46 | | | | 31595.96 |
| WOLF | 22 | | 11489.61 | | 132.03 | | 9506.53 | | 186.62 | | | | 12314.85 |
| SPIKE | 632785 | | | | | | | | | | | | |
| TOTAL | | | | | | | | | | | | | |
| CLINKER | 319873 | 33.000 | 4792.34 | 0.083 | 12.05 | 14.900 | 2163.81 | 0.368 | 53.44 | 0.147 | 21.35 | 84.800 | 12314.85 |
| KILN DUST | 50220 | 10.400 | 237.12 | 0.798 | 18.19 | 20.700 | 471.96 | 0.294 | 6.70 | 56.500 | 1288.19 | 29.900 | 681.72 |
| BYPASS DUST | 8000 | 38.500 | 104.87 | 0.094 | 0.26 | 1080.000 | 2887.44 | 0.588 | 1.60 | 2.260 | 6.16 | 128.000 | 348.67 |
| CALCINE CO2 | 175770 | | 0.02 | | 16.42 | | 5.64 | | 0.00 | | 0.00 | | 0.02 |
| STACK GAS H2O | 103374 | | 5134.35 | | 46.92 | | 5528.85 | | 61.75 | | 1315.70 | | 13345.26 |
| TOTAL | 655237 | | | | | | | | | | | | |
| % CLOSURE | 103.55 | | 44.76 | | 35.54 | | 59.16 | | 33.09 | | 144.99 | | 42.24 |
| SRE % | | | 99.95 | | 86.28 | | 99.93 | | | | | | 99.96 |
| TEST #9 | MASS FLOW lbs/hr | Chromium (Cr) mg/kg | Flow g/hr | Mercury (Hg) mg/kg | Flow g/hr | Lead (Pb) mg/kg | Flow g/hr | Antimony (Sb) mg/kg | Flow g/hr | Thallium (Tl) mg/kg | Flow g/hr | Zinc (Zn) mg/kg | Flow g/hr |
| FEEDS | 502200 | 18.900 | 3853.18 | 0.495 | 112.66 | 11.500 | 2621.99 | 0.350 | 79.80 | 4.440 | 1012.31 | 20.700 | 4719.58 |
| RAW FEED | 14000 | 20.400 | 219.31 | 0.135 | 1.45 | 3.960 | 42.57 | 0.303 | 3.26 | 0.418 | 4.49 | 65.200 | 703.05 |
| RAW FEED (H2O) | 23680 | 0.012 | 0.37 | 0.004 | 0.12 | 0.006 | 0.18 | 0.005 | 0.15 | 0.002 | 0.06 | 0.080 | 2.45 |
| COAL PRECAL | 67400 | 99.800 | 135.93 | 0.085 | 35.14 | 25.600 | 35.14 | 1.240 | 1.69 | 0.179 | 0.24 | 8650.000 | 11781.30 |
| QUENCHH2O | 3000 | 277.000 | 50.95 | 11.500 | 2.08 | 60.700 | 10.97 | 3.410 | 0.62 | 0.774 | 0.14 | 806.000 | 145.64 |
| TIRES | 273 | 589.000 | 5555.09 | 1.880 | 17.54 | 621.000 | 5858.90 | 10.810 | 101.95 | 0.155 | 1.46 | 297.000 | 2801.12 |
| WDSF | 20774 | | 825.71 | | | | 300.52 | | 187.47 | | | | 20151.03 |
| WOLF | 22 | | 10080.64 | | 134.17 | | 9089.27 | | | | | | |
| SPIKE | 631534 | | | | | | | | | | | | |
| TOTAL | | | | | | | | | | | | | |
| CLINKER | 319873 | 32.200 | 4676.16 | 0.078 | 11.33 | 30.200 | 4385.71 | 0.754 | 109.50 | 0.149 | 21.84 | 86.400 | 12547.21 |
| KILN DUST | 50220 | 6.190 | 141.13 | 0.825 | 18.81 | 33.400 | 761.52 | 0.309 | 9.10 | 60.800 | 2024.63 | 29.300 | 688.04 |
| BYPASS DUST | 6000 | 32.900 | 89.62 | 0.154 | 0.42 | 1000.000 | 2724.00 | 2.550 | 6.95 | 5.230 | 14.25 | 126.000 | 343.22 |
| CALCINE CO2 | 175770 | | 0.02 | | 58.14 | | 12.94 | | 0.00 | | 0.00 | | 8.97 |
| STACK GAS H2O | 103374 | | 4906.93 | | 80.70 | | 7804.17 | | 125.54 | | 2060.51 | | 13567.44 |
| TOTAL | 655237 | | | | | | | | | | | | |
| % CLOSURE | 103.75 | | 46.12 | | 66.11 | | 80.90 | | 202.27 | | 202.27 | | 67.33 |
| SRE % | | | 99.95 | | 86.50 | | 99.93 | | | | | | 99.94 |

TABLE 2-11
DRE SUMMARY DATA
BIF COC TEST PROGRAM PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST #3 | MASS FLOW | Perchloroethylene | Flow | Trichlorotrifluoromethane | Flow | 1,1,2 Trichloroethane | Flow | 1,1,1 Trichloroethane | Flow |
|-------------|-----------|-------------------|---------|---------------------------|--------|-----------------------|--------|-----------------------|---------|
| g/hr | ug/g | g/hr | ug/g | g/hr | ug/g | g/hr | ug/g | g/hr | ug/g |
| 6/25/92 | 9275213 | 28833 | 267432 | 1350 | 12526 | 4232 | 39252 | 15294 | 141855 |
| WDLF | 389733 | 5.881 | 2 | 0.125 | 0 | 1.987 | 1 | 4.545 | 2 |
| WDSF | 1362000 | | | | | | | | |
| Tires | 10750720 | | | | | | | | |
| Coal | 21777666 | | | | | | | | |
| TOTAL INPUT | 49373408 | 28839 | 267435 | 1351 | 12526 | 4232 | 39253 | 15299 | 141857 |
| STACK GAS | | | 0.591 | | 0.591 | | 0.591 | | 0.591 |
| % DRE | | | 100.000 | | 99.995 | | 99.998 | | 100.000 |
| TEST #4 | | | | | | | | | |
| 6/25/92 | 9079258 | 7190 | 65280 | 1403.368 | 12742 | 5489 | 49836 | 13406 | 121713 |
| WDLF | 452874 | 0.125 | 0 | 0.125 | 0 | 0.125 | 0 | 7.462 | 3 |
| WDSF | 1362000 | | | | | | | | |
| Tires | 10968640 | | | | | | | | |
| Coal | 21862772 | 7190 | 65280 | 1403 | 12742 | 5489 | 49836 | 13413 | 121717 |
| TOTAL INPUT | 50126594 | | 0.626 | | 0.626 | | 0.626 | | 0.626 |
| STACK GAS | | | 99.999 | | 99.995 | | 99.999 | | 99.999 |
| % DRE | | | 100.000 | | 99.996 | | 99.999 | | 99.999 |
| TEST #5 | | | | | | | | | |
| 6/25/92 | 9101030 | 15570 | 141706 | 1597 | 14539 | 4722 | 42979 | 9029 | 82169 |
| WDLF | 411508 | 0.125 | 0 | 20.574 | 8 | 0.125 | 0 | 143.449 | 59 |
| WDSF | 1362000 | | | | | | | | |
| Tires | 10569120 | | | | | | | | |
| Coal | 21443856 | 15570 | 141706 | 1618 | 14547 | 4722 | 42979 | 9172 | 82228 |
| TOTAL INPUT | 49761124 | | 0.602 | | 0.602 | | 0.602 | | 0.602 |
| STACK GAS | | | 100.000 | | 99.996 | | 99.999 | | 99.999 |
| % DRE | | | 100.000 | | 99.996 | | 99.999 | | 99.999 |

2.2.6 Continuous Emission Monitoring of CO, THC and O₂

During Phase 2, CEM data was collected by APCC from the exhaust stack (as in Phase 1), and also by the Lonestar CEMS installed in the bypass duct. A summary of APCCs CEM data for CO, THC and O₂ is presented in Table 2-12. Emissions of CO from the main exhaust stack were significantly higher than in Phase 1 while THC emissions were approximately 50% lower. This combination of data could indicate different calcination conditions in the precalciner. These data are not representative of combustion conditions in the kiln, but primarily represent conditions in the pre-calciner, where coal is fired at low oxygen conditions and incomplete calcination takes place. Data summaries are presented in Appendix A, with field data in B-5.

A summary of Lone Star's CEM for CO, THC and O₂ is presented in Table 2-13. CO emission concentrations were typically less than 100 ppm, with the exception of Test 3 which was 113 ppm (corrected to 7% O₂). THC concentrations were less than 0.3 ppm (corrected to 7% O₂) throughout all tests. Data summaries are presented in Appendix A, field data in B-6.

It should be noted that, although attempted, a Tier 2 CO emission limitation in the bypass duct was not demonstrated during Phase 1 or Phase 2. The bypass CEMS was not yet installed during Phase 1 to observe CO emissions under 100% coal fire. During Phase 2 (@ 100% WDF w/ tires in the back end) CO emissions were typically within the Tier 1 range (i.e. <100 ppm @ 7% O₂). Subsequent to Phase 2 testing, however, significant concentrations of CO have been observed when firing **less waste fuel** and a greater amount of coal. Measured emissions concentrations of THC are always insignificant (< 1 ppm actual) under all operating conditions.

Due to this situation, Lone Star, with the approval of Joe Galbraith of EPA Region VII, ran under a number of different operating conditions during the months of July and August to establish a Tier 2 CO emission limitation. Field data for these tests are presented in Appendix B-7.

TABLE 2-12
APCC (STACK) CEM DATA SUMMARY
BIF COC TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# DATE | TIME | | CO (ppm) | CO2 (%) | O2 (%) | NOx (ppm) | SO2 (ppm) | THC (ppm) | CO Corr. (ppm) | THC Corr. (ppm dry) | CO Corr. Rolling Avg | THC Corr. Rolling Avg |
|--------------------------------|-------|-------|-------------|------------|-----------|--------------|--------------|--------------|-------------------|------------------------|-------------------------|--------------------------|
| | From | To | | | | | | | | | | |
| Test #3 6/25/92 | 8:33 | 12:03 | 2223 | 16.8 | 10.7 | 110 | 67 | 24 | 2947 | 38 | 3147 | 38 |
| Test #4 6/25/92 | 17:48 | 20:48 | 1156.8 | 16.9 | 11.1 | 216 | 99 | 22 | 1611 | 36 | 1783 | 35 |
| Test #5 6/25/92- 6/26/92 | 21:48 | 1:03 | 1144.7 | 16.9 | 10.8 | 221 | 91 | 20 | 1559 | 33 | 1599 | 33 |
| Test #7 6/26/92 | 13:49 | 16:49 | 2242 | 18.7 | 9.7 | 208 | 152 | 40 | 2704 | 57 | 2983 | 60 |
| Test #8 6/26/92 | 17:49 | 20:49 | 1917 | 19.1 | 9.4 | 274 | 190 | 39 | 2258 | 55 | 2329 | 56 |
| Test #9 6/26/92- 6/27/92 | 21:34 | 0:34 | 2196 | 18.9 | 10.1 | 259 | 187 | 38 | 3136 | 67 | 3075 | 66 |

TABLE 2-13
LONESTAR BYPASS DUCT CEMS DATA
BIF COC TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST# DATE | TIME From | TIME To | O2 (%) | CO (ppm) | CO Corr. (ppm) | THC (ppm) | THC Corr. (ppm) | CO Corr. Rolling Avg | THC Corr. Rolling Avg |
|---------------|--------------|------------|-----------|-------------|-------------------|--------------|--------------------|-------------------------|--------------------------|
| 6/25/02 | | | | | | | | | |
| TEST 3 | 08:33 | 11:33 | 18.6 | 20 | 113 | 0 | 0 | 99 | 0 |
| TEST 4 | 17:40 | 20:48 | 17.2 | 19 | 73 | 0 | 0 | 62 | 0 |
| TEST 5 | 21:48 | 00:48 | 17.3 | 23 | 89 | 0 | 0 | 91 | 0 |
| 6/28/02 | | | | | | | | | |
| TEST 7 | 13:49 | 16:49 | 17.3 | 4 | 16 | 0 | 0 | 23 | 0 |
| TEST 8 | 18:04 | 20:34 | 16.8 | 3 | 4 | 0 | 0 | 12 | 0 |
| TEST 9 | 21:49 | 00:19 | 17.7 | 7 | 32 | 0 | 0 | 34 | 0 |

3.0 PROCESS AND OPERATIONS

Lone Star Industries produces portland cement with a dry preheater, precalciner kiln process. The kiln system was designed by Allis-Chalmers. The kiln is 14'6" diameter and 235' long as shown in Figure 3-1. The kiln is designed for 9" thick refractory throughout and is mounted on a slope for precalcined raw material to enter the top and be conveyed towards the burners at the front end. Energy is provided at three locations in the kiln process; kiln front end, material shelf and precalciner.

The precalciner provides 45% of the total system energy, the tires at the material shelf 15%, and the front end of the kiln 40%. At the front end, pulverized coal is injected to provide heat to transform the raw material to clinker at a temperature of 3500° F (2700° F material temp.). Clinker production is on average 3500-3800 tons/day. Feed rate of raw material mix on an hourly basis varies from 225 to 270 tph, averaging about 250 tph. The kiln rotates 3.5 RPM maximum, and with normal production the kiln turns at 2.7 RPM. Draft air is drawn through the kiln and the preheater tower by a 4000 horsepower I.D. preheater fan. An additional 4000 horsepower I.D. fan located after the raw mill draws hot exhaust gases through the mill to dry raw material. A separate ID fan draws off approximately 10% to 30% of the kiln exhaust gas through the bypass baghouse. This stack discharges into the main stack. Particulate matter is removed from the raw mill exhaust stream by a fabric filter dust collector (main baghouse) before venting to the atmosphere.

3.1 PORTLAND CEMENT PROCESS

Raw materials (limestone, silica, alumina, iron oxide and flyash) are mined, crushed, stockpiled and reclaimed to mill feed bins for storage. The raw materials are conveyed to a roller mill for size reduction and drying. The roller mill is used to grind the product to a 72% passing 200 mesh size (74 microns). The material is dried by hot gases drawn from the kiln and the preheater system through the roller mill by the I.D fan. All ground raw material as well as kiln exhaust emissions are conveyed by air to a glass bag dust collector preceded by multiple cyclones to remove particulate from the gas stream while simultaneously collecting raw material for blending. The conditioned raw material is discharged from the dust collector and cyclones into blending silos to be conveyed by a 292 foot elevator to the first stage of the 4 stage preheater / precalciner as needed. Exhaust gases from the main baghouse are vented to the atmosphere 210 feet above grade.

The preheater uses the kiln and precalciner exhaust gases to heat the raw material to 1500°F before entering the precalciner. Pulverized coal is fired in the precalciner to heat the material to 1750-1900°F. Where the material enters the kiln, the gas temperatures exceed 2100°F and product temperature averages 1600°F. Approximately 85% of the raw feed is calcined before it enters the kiln. The precalciner is fired with a maximum of 14 tph of coal. The heated raw material is then conveyed to one final cyclone for separation from the process gas before entering the rotary kiln. The rotary kiln heats the raw material to incipient melting where the portland cement products are formed near a temperature of 2700 °F (material). A typical temperature profile of the kiln is presented in Figure 3-2.

FIGURE 3 - 1
 PROCESS SCHEMATIC
 LONE STAR CEMENT PLANT
 CAPE GIRARDEAU, MISSOURI

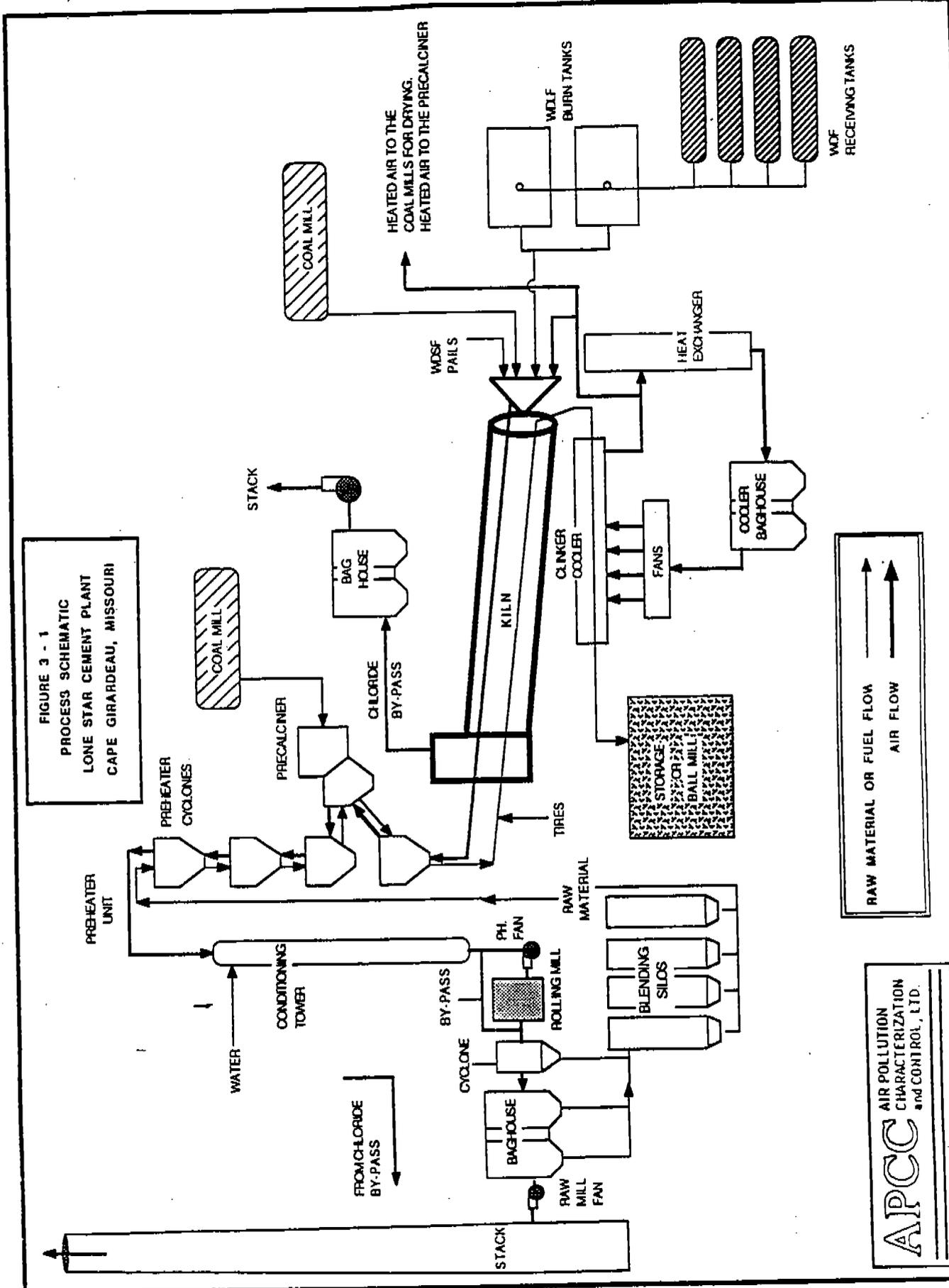
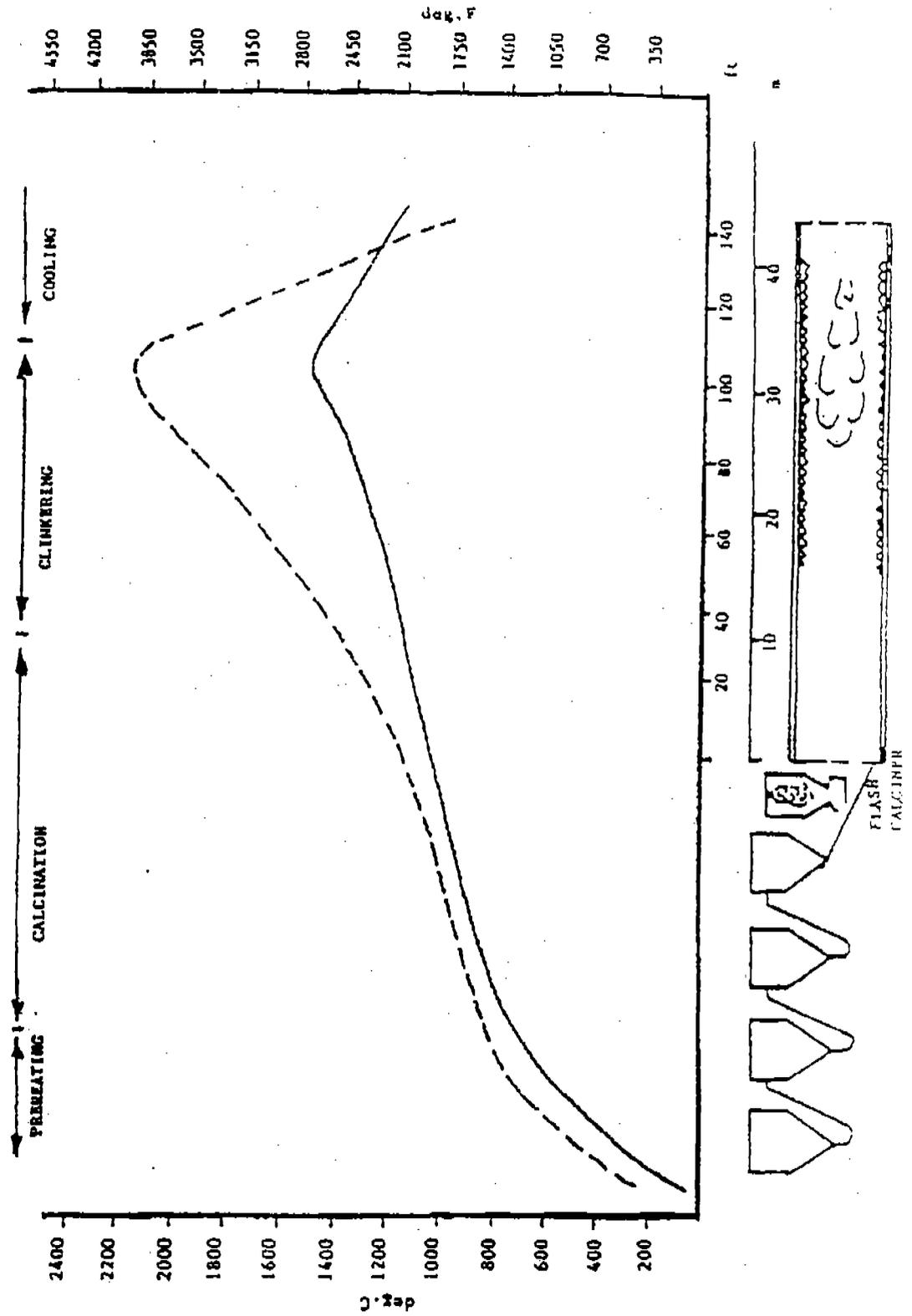


FIGURE 3-2
 PRECALCINER KILN
 MATERIAL & GAS TEMPERATURE PROFILE



Only tires and pulverized coal are used to provide heat to the preheater system. Heat to the kiln is supplied by firing pulverized coal, and/or a combination of WDLF & WDSF. Coal is injected counter current to the product flow through burners at the front (product discharge) end of the kiln. Coal is gravimetrically fed to a coal mill where it is pulverized and fired through a single gun burner system. A second burner for firing WDLF is installed concentric to the coal burner. This burner uses high pressure air atomization to inject WDLF directly into the flame. The burner is rated at 44 gallons per minute. WDSF, contained in 3.5 gallon pails, is fired into the kiln by means of an air cannon mounted on the kiln hood. Tires are introduced to the back end of the kiln at the material shelf, as described in Section 3.2.

While the bulk of kiln gaseous emissions exit the kiln through the precalciner and 4-stage preheater, the majority of the chloride emissions exit the kiln bypass through a bypass duct at the back of the kiln. The chloride bypass (typically 10% to 30% of the total gas flow) kiln exhaust is cooled to approximately 400°F with ambient air and water injection for sensible cooling. The dust is collected by a baghouse described in Section 3.3. The exhaust gases are then vented to the main exhaust stack.

The portland cement product (clinker) is discharged from the front (hot) end of the kiln to the clinker cooler for cooling (to approximately 175 °F). Ambient air is drawn into the clinker cooler at a rate of 247,000 scfm. The heated air is drawn to the kiln for combustion air and for drying coal in the coal mills and raw material in the roller mill. Clinker is conveyed either to storage silos or to the finish mill feed bins. All exhaust from the kiln, precalciner, preheater, and roller mill are vented to atmosphere through the main baghouse and a single stack 210 feet above grade. Bypass exhaust also connects to the same stack.

3.2 FUEL BURNING

No. 2 fuel oil is used to preheat the kiln during start-up. The maximum coal firing rate to the kiln is 10 tph and 14 tph for precalciner. Shredded tires are fired at the material shelf of the 4-stage preheater at the entrance to the kiln. The rated production capacity of the kiln is approximately 3500 to 3800 tons per day.

Heat is supplied to the rotary kiln by firing pulverized coal, tires, WDLF and WDSF. Coal and WDLF are injected counter current to the product flow through burners at the front (product discharge) end of the kiln. WDSF is injected into the burn zone at the front end of the kiln via an air cannon. Coal is feed to a coal mill where it is dried, pulverized and stored in bins. The coal is gravimetrically drawn from the bin and fired through a single gun burner system rated at approximately 10 tph. The coal mill is rated at 15 tph. The fan which draws drying air through the mill is rated at 22,000 acfm at 600°F and -4 in.w.c. The clinkering zone extends into the kiln approximately 1/3 the length of the kiln. A typical coal analysis is presented in Table 3-1.

Heat to the precalciner is provided by firing pulverized coal supplied by a second coal mill. This coal mill is rated at 20 tph and the fan is rated at 36,000 acfm at

600°F and -4 in.w.c. No WDLF or WDSF is fired in the precalciner. Tires fired at the material shelf also supply heat to the precalciner.

WDLF and WDSF consist of organic substances and mixtures immediately useful as fuel, or which are blended into a useful fuel. Typical generic types of organic substances which may be present at some level are shown in Table 3-2. The Table 3-2 list is descriptive and not considered limiting. The substances contained in WDLF and WDSF are typically those used each day in industry, commerce and around the home. They are found in products such as paints, varnishes, lacquers, thinners, cleaners, detergent formulations, spot removers, nail polish remover, lighter fluid and gasoline.

TABLE 3-1
TYPICAL COAL ANALYSIS

| | | |
|------------|--------------|-------------|
| HHV | 11000 Btu/lb | Dry basis |
| Sulfur | 2-3% | Dry basis |
| Ash | 18-24% | As received |
| % Chloride | 565 ppm | As received |
| Antimony | 0.20 ppm | As received |
| Arsenic | 6.0 ppm | As received |
| Barium | 0.37 ppm | As received |
| Cadmium | 5.0 ppm | As received |
| Chromium | 1.40 ppm | As received |
| Lead | 20.0 ppm | As received |
| Mercury | 0.05 ppm | As received |
| Silver | 5.00 ppm | As received |
| Thallium | 0.50 ppm | As received |

TABLE 3-2
TYPICAL ORGANIC SUBSTANCES
PRESENT IN WDLF & WDSF

| | |
|---------------|-------------------------------|
| Alcohols | Degreasers |
| Glycols | Chlorinated Organic Liquids |
| Polyols | Polymers, Copolymers, |
| Glycol Ethers | Oligomers and Resin Fragments |
| Ketones | Esters |
| Aldehydes | Vegetable Oils & Derivatives |
| Aldehydes | Oxides & Epoxides |
| Acrylics | Ethers |
| Hydrocarbons | Petroleum Oils & Derivatives |

Approximately 900, 3.5 gallon plastic pails filled with solid waste filter material, sludges and non-pumpable/unsuspended waste (WDSF) can be fired in the kiln on a daily basis. The pails are injected approximately 60 feet into the front of the kiln by air cannon which is set at 40 to 70 psi., depending upon the container weight which can vary between 20-35 lbs. Along with the firing of WDLF, these pails are fired into the burn zone at an approximate rate of one every 90 seconds. Pails are not fired daily, but only as supply becomes available at the facility.

A second burner for firing WDLF is installed within the coal burner pipe. This burner uses high pressure air atomization to inject WDLF directly into the kiln. The burner is rated at 44 gallons per minute, which is the anticipated burn rate for 100% replacement of coal.

Lone Star does not use as WDLF or WDSF any substances or mixtures subject to Federal PCB regulations pursuant to 40 CFR Part 761. The contents of WDLF streams vary greatly on a daily basis. Burn specification analyses for WDLF and WDSF streams are shown in Table 3-3. No. 2 fuel oil is used to preheat the kiln during start-up. The maximum coal firing rate to the kiln is 10 tph and 14 tph for precalciner. When firing WDLF at 44 gpm, no coal is fired in the kiln. The rated production capacity of the kiln is approximately 3500 to 3800 tons per day.

Shredded tires are supplied to the feed end of the kiln at the material shelf as a supplement to coal firing in the preheater. The tires are delivered to the kiln via a bucket elevator and belt conveyor. The shredded tires are conveyed directly into a chute equipped with two hydraulically controlled gates. The action of the feed gates determines the feed rate into the kiln. The maximum burn rate (approximate) for tires is 2.0 tph. A typical tire analysis is presented in Table 3-4.

TABLE 3-3
WDLF & WDSF
ANNUAL AVERAGE PCC
BURN SPECIFICATIONS
LONE STAR INDUSTRIES
CAPE GIRARDEAU, MISSOURI

| COMPOUND | Maximum Limit | COC Specifications | BIF Tier Control |
|----------------------|---------------|--------------------|------------------|
| Total Chlorides | 5.0 % | 5.0% | |
| Antimony | 50 ppm | NA | I |
| Arsenic | 175 ppm | 175 ppm | III |
| Beryllium | 3 ppm | 3 ppm | III |
| Cadmium | 400 ppm | 400 ppm | III |
| Chromium III | 900 ppm | 900 ppm | III |
| Chromium VI | 100 ppm | 100 ppm | III |
| Total Chromium | 1000 ppm | 1000 ppm | III |
| Barium | 10,000 ppm | NA | I |
| Lead | 700 ppm | 700 ppm | III |
| Mercury | 1.7 ppm | 1.7 ppm | II |
| Silver | 50 ppm | NA | I |
| Thallium | 50 ppm | NA | I |
| Sulfur (yearly avg.) | 2.7 % | | |
| Heating Value | > 5000 Btu/lb | NA | II |

**TABLE 3-4
TYPICAL TIRE ANALYSIS**

| | |
|------------|---------------|
| HHV | 13,000 Btu/lb |
| Carbon | 75.81 % |
| Nitrogen | 7.67 % |
| Hydrogen | 6.95 % |
| Sulfur | 1.47 % |
| Oxygen | 1.05 % |
| Moisture | 0.00 % |
| Arsenic | < 2 ppm |
| Cadmium | 6 ppm |
| Calcium | 0.379 % |
| Chlorine | 0.191 % |
| Chromium | 0.0087 % |
| Fluorine | 10 ppm |
| Iron | 2.90 % |
| Lead | 65 ppm |
| Mercury | <0.5 ppm |
| Phosphorus | 0.02 % |
| Zinc | 1.59 % |

3.3 AIR POLLUTION CONTROL SYSTEM

Kiln emissions are collected with a modified Buell Model 56-RM-12 fabric filter main baghouse designed to collect raw material from the roller mill and dust generated from the kiln / preheater system. Immediately before the baghouse are four cyclones which remove most of the large particles (raw material). The baghouse is a 32 module reverse air cleaning device. This emission control system normally cleans 325,000 acfm of gases at an inlet temperature that is controlled to not exceed 350°F (roller mill by-pass condition). Under normal conditions (roller mill on-line) the inlet

temperature is approximately 250° F. Kiln emissions dust is mixed in with the raw material from the rolling mill and stored in the storage silos.

The reverse air cleaning system utilizes a programmable controller unit (scheduled time periods) to control cleaning duration and sequence. Also, during cleaning cycles, acoustic horns are utilized to assist in cleaning. The reverse air fan is designed to run continuously; compartments are isolated via inlet dampers, and reverse air valves are opened to clean modules. Two modules at a time are isolated and cleaned simultaneously.

There are 56 fabric bags per module for a total of 1792 bags. The total area of cloth is 173,632 ft² with an air to cloth ratio of 2.01:1. The normal differential pressure drop across the baghouse is 10 in. w.c. The minimum pressure drop recommended by the manufacturer 7 in. w.c. Typically one section of the baghouse is isolated for bag replacement, an on-going process of plant maintenance.

Baghouse collection efficiency is estimated to be 99.9%. The basis for the estimation is as follows: According to stack testing done by Lone Star as well as other contractors, a typical particulate emission is 34 pounds per hour, with the MO DNR Permit Limit of 63 lbs/hr. The normal feed rate to the baghouse is 260 tph. If the cyclones immediately before the baghouse are 85% efficient, the baghouse would therefore receive 39 tph of material. The efficiency would therefore be:

$$\text{Efficiency} = \frac{[(39 \times 2000) - 34]}{(39 \times 2000)} \times 100 = 99.9\%$$

Currently the only time any dust in the system is wasted (i.e. not recycled) is when the chloride bypass system is operating. This system is designed to draw off a maximum of 30% of the kiln exit gases to prevent chloride salt accumulation in the preheater section. The maximum volume drawn off is approximately 8,000 scfm. The rate of the bypass is dependent on the amount of chloride and alkali in the system. The system is designed on the theory that all chloride salts are gaseous at kiln temperatures and therefore rise to the top of the kiln. A slipstream, therefore, drawn off the top of the kiln will remove most of the undesirable salts present. A minimum of 10% of the kiln exhaust gas is bypassed during the firing of WDF.

The kiln exit temperature of the gases is above 2000° F. This dust and chloride salt laden air stream is cooled with induced ambient air and water to approximately 400°F and passed through a fabric filter baghouse to control dust in the air stream. The bypass baghouse contains 6 modules with 120 bags per module and is cleaned by reverse air. The dust collected in this baghouse is wasted (i.e. not used as product). Under normal conditions, approximately 1-3 tph of dust is collected by the baghouse. Exhaust gases from the baghouse are vented to the main kiln stack.

Draft is provided by an induced draft preheater fan rated at 430,000 acfm, while secondary combustion air is supplied by eight forced draft clinker cooler fans rated at a

total of 368,000 acfm. The secondary combustion air is preheated by the clinker cooler at the front of the kiln.

3.4 KILN SAFETY SYSTEM

A Foxboro doppler flow meter is installed to control, continuously monitor, and record the WDLF firing rate. In addition, a computer is installed and programmed to energize interlocks to automatically stop the flow of WDLF to the burner if one of the following parameters are exceeded:

- Limits on CO
- THC >20 ppm corrected hourly rolling average
- Total feed rate of WDF and WDLF
- Kiln rotation
- Maximum production rate
- Maximum or minimum combustion zone temperature (as indicated by 4th stage preheater thermocouple)
- Maximum flue gas temperature entering the main baghouse
- Main baghouse minimum ΔP

In addition, an alarm and light signals the WDSF operator to cease manually injecting pails when limits are approached.

Kiln operators, along with the kiln microprocessor based control system programmed to initiate operator alarms, are continually monitoring and logging key operating parameters and are conscious of changing readings or unusual conditions which can be indications of potential problems. The control system warns of problems before they become critical, to allow time for corrective action. Copies of the log sheets are presented in the Appendix of this report.

3.5 COC PROCESS OPERATIONS

The COC was performed in two phases; coal only and coal/WDF/tires. Phase 1 was performed in April 1992, while Phase 2 was performed in June.

3.5.1 Phase 1

Phase 1 was performed in conjunction with a Tire Trial Burn Program in April, and serves as background comparison when the only fuel to the kiln was coal. The kiln was operated under normal conditions during this period. A summary of average kiln conditions is presented in Table 3-5A.

Kiln feed averaged between 252 and 257 tph for the 6 tests performed during Phase 1. 8.1 to 8.5 tph coal was fired in the kiln with an additional 11.9 to 12.1 in the preheater (RSP). Combustion zone temperatures as indicated by the fourth stage of the preheater (as a surrogate, as there is no practical way to monitor actual combustion zone temperatures on a continuous basis) ranged from 1678°F to 1695°F.

3.5.2 Phase 2

During Phase 2, two distinct abnormal operating conditions were run in an attempt to set minimum and maximum kiln operating limits. This typically meant running the kiln under near upset conditions while still producing saleable product. In an attempt to set minimum and maximum hourly rolling averages for operational parameters as required by BIF, it should be noted that it was necessary to manipulate the kiln to the edge of upset and/or shut-down conditions. Operation was then held at this point as long as possible to set the limitation by establishing a 1-hour rolling average, as required by Section 5.3.1 of "Technical Implementation Document for EPA's Boiler and Industrial Furnace Regulations" (EPA-530-R-92-011, March 1992).

Phase 2 was performed in June 1992 under two distinct kiln operating conditions of maximum and minimum combustion chamber temperatures as discussed in Section 1.1, (1) minimum burning zone temperature conditions and (2) maximum burning zone temperature conditions. Three tests were performed for particulate, POHC, HCl, Cl₂, THC, and CO while the kiln was firing approximately 44 gpm (352 lbs/min) of combined WDLF and WDSF in the front end of the kiln as an energy replacement for kiln coal, and approximately 1.5 tph of shredded tires at the material shelf at the back end of the kiln as supplemental heat to the precalciner.

These tests were performed at minimum combustion chamber conditions, as represented by the temperature of the fourth stage of the preheater, representing 100% energy replacement of the kiln coal. The WDSF was preweighed in 3.5 gallon plastic pails and "shot" into the burning zone of the kiln with an air cannon. Each bucket contained API separator sludge and weighed 25 pounds. An effort was made to procure and blend a waste fuel simulating as closely as possible worst case conditions for chlorides and Btu content. This WDF contained a minimum of 5000 Btu/pound and a maximum of 5% chloride. The rate of firing of the two waste derived fuels was set to maximize the **total hazardous fuel feed stream**, as required by the BIF regulation, at approximately 44 gal/min. This limit is based on a MO DNR limitation of 20,000,000 gal/year. WDLF was injected by a lance placed in the coal burner pipe, while WDSF was placed in 3.5 gallon buckets preweighed at 25 pounds each and fired into the burning zone of the kiln via an air cannon.

Pails were not continually fired during the entire period of each test. When the shooting of pails was ceased in order to maintain kiln operations, the WDLF rate was adjusted to increase the **total hazardous fuel feed stream** to 44 gal/min. In a similar manner, when pails were injected, the WDLF feedrate was decreased to bring the **total hazardous fuel feed stream** to 44 gal/min. The minimum burning zone conditions were maintained as was practicable to set the minimum 60-minute rolling average temperature limit as indicated by the temperature of the fourth stage of the

preheater. WDLF was spiked with surrogate POHC to demonstrate destruction under minimum combustion chamber temperatures. No spiking of WDSF in pails was performed.

A summary of Phase 2 / Minimum Combustion Temperature kiln operations is presented in Table 3-5B. Tests 3, 4 and 5 represent this condition. In addition, the following represent the **total hazardous fuel feed stream (THFFS)** to the kiln on 25 June:

| <u>Test#</u> | <u>WDLF (gpm)</u> | <u>WDSF (gpm)</u> | <u>THFFS (gpm)</u> |
|--------------|-------------------|-------------------|--------------------|
| 3 | 42.6 | 1.8 | 44.4 |
| 4 | 41.7 | 2.1 | 43.8 |
| 5 | 41.8 | 1.9 | 43.7 |

As can be determined, the sum of these two rates is approximately 44 gal/min. The average of these numbers was used to determine the total hazardous feed rate to the kiln. However, the maximum pumpable feed rate was determined by the highest hourly rolling average of liquid fuel when buckets were not utilized as fuel.

Kiln feed averaged 241 tph for the three tests performed under this operating condition, with an average fourth stage preheater temperature of 1652°F. Specific trends for these operations can be seen in Figures 3-3, 3-4 and 3-5. These figures represent operations during attempts to establish minimum and maximum kiln operating limits. This typically meant running the kiln under near upset conditions while still producing saleable product. In an attempt to maintain minimum operating temperatures during each test run, it was necessary to decrease kiln feed following the establishment of the 60-minute rolling average maximum to prevent total upset conditions. Due to these requirements, it was impossible to maintain "steady state" operations throughout each test period, as would be done for a normal (non-BIF) test program).

For Phase 2 maximum burning zone temperature conditions, triplicate tests for metals, Cr⁺⁶, THC, and CO were performed. To condition the kiln system, maximum metals were spiked for a period of twelve hours before the start of the first test to ensure that the kiln system approached equilibrium with regards to metals before testing. In addition, analyses of kiln inputs and outputs were performed hourly to determine equilibrium for each metal. A graphic presentation of equilibrium (not to be confused with "steady state", where equilibrium is defined as "the condition where a change in inputs causes an equivalent change in outputs") demonstrations for each metal is presented in Appendix D.

In addition, Region VII BIF coordinator, Joe Galbraith, met with Lone Star and APCC in December 1991 following review of the COC Test Protocol and at that time required twelve hours of preconditioning at maximum metals feedrates prior to metals testing. The same fuels that were utilized under minimum combustion conditions were also used under this condition. WDLF and WDSF fuels rates were adjusted in the same manner as described above. Maximum combustion chamber temperatures were achieved by increasing the coal fired to the kiln precalciner. Under this condition

the feed enters the kiln in a more prepared state and the temperature in the burning zone of the kiln increases. This is because the actual clinkering inside the kiln is somewhat exothermic, while calcination is an endothermic process.

A summary of Phase 2 / Maximum Combustion Temperature kiln operations is presented in Table 3-5B. Tests 6, 7 and 8 represent this condition. In addition, the following represent the **total hazardous fuel feed stream (THFFS)** to the kiln on 26 June:

| Test# | WDLF (gpm) | WDSF (gpm) | THFFS (gpm) |
|-------|------------|------------|-------------|
| 7 | 42.6 | 0.6 | 43.1 |
| 8 | 43.3 | 0.6 | 43.8 |
| 9 | 43.3 | 0.8 | 44.1 |

As can be determined, the sum of these two rates is approximately 44 gal/min. The average of these numbers was used to determine the total hazardous feed rate to the kiln. However, the maximum pumpable feed rate was determined by the highest hourly rolling average of liquid fuel when buckets were not utilized as fuel.

These tests were performed at maximum combustion chamber temperature, as represented by the temperature of the fourth stage of the preheater; representing 100% energy replacement of the kiln coal. The WDSF was preweighed in 3.5 gallon plastic pails and "shot" into the burning zone of the kiln with an air cannon. Each bucket contained API separator sludge and weighed 25 pounds. An effort was made to procure and blend a waste fuel simulating as closely as possible worst case conditions for chlorides and Btu content. This WDF contained a minimum of 5000 Btu/pound and a maximum of 5% chloride. The rate of firing of the two waste derived fuels was set to maximize the **total hazardous fuel feed stream**, as required by the BIF regulation, at approximately 44 gal/min.

As in the minimum temperature scenario, pails were not continually fired during the entire period of each test. When the shooting of pails was ceased in order to maintain kiln operations, the WDLF rate was adjusted to increase the **total hazardous fuel feed stream** to 44 gal/min. In a similar manner, when pails were injected, the WDLF feedrate was decreased to bring the **total hazardous fuel feed stream** to 44 gal/min. WDLF was spiked with metals and additional metals fed in solid form through the coal pipe to demonstrate SRE under maximum combustion chamber temperatures. No spiking of WDSF in pails was performed.

Kiln feed averaged 251 tph for the three tests performed under this maximum temperature operating condition, with an average fourth stage preheater temperature of 1669°F. Specific trends for these operations can be seen in Figures 3-6, 3-7 and 3-8. Also included in these figures is the WDLF feedrate in gph. These figures represent operations during attempts to establish maximum kiln operating limits for metals feedrates, kiln feed and combustion zone temperature. This typically meant running the kiln under near upset conditions while still producing saleable product. As can be seen, from an operational point of view, it is easier to maintain maximum operating

TABLE 3-5A
PROCESS DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Apr-92

| TEST # TIME | UNITS | Main Baghouse | | FEED END O2 % | 4TH STAGE TEMP °F | KILN FEED TPH | STACK OPACITY % | Kiln I.D. Fan | | KILN COAL TPH | RSP COAL TPH |
|----------------|-------|---------------|--------|---------------------|-------------------------|---------------------|-----------------------|---------------|--------|---------------------|--------------------|
| | | Δ PRESS | IN. WC | | | | | TEMP °F | IN. WC | | |
| 4/13/92 | | | | | | | | | | | |
| TEST 2 | | 12.2 | 204 | 4.3 | 1678 | 253.7 | 12.4 | 37.5 | 822.3 | 8.4 | 12.1 |
| 9:25-12:48 | | | | | | | | | | | |
| TEST 3 | | 12.1 | 210 | 4.2 | 1683 | 252.5 | 14.4 | 37.5 | 823.3 | 8.4 | 11.9 |
| 13:08-16:20 | | | | | | | | | | | |
| TEST 4 | | 11.6 | 208 | 4.4 | 1693 | 253.7 | 12.7 | 37.6 | 824.0 | 8.4 | 11.8 |
| 16:55-20:06 | | | | | | | | | | | |
| 4/14/92 | | | | | | | | | | | |
| TEST 6 | | 11.5 | 200 | 4.1 | 1695 | 258.6 | 12.1 | 38.3 | 826.0 | 8.5 | 12.0 |
| 11:28-14:05 | | | | | | | | | | | |
| TEST 7 | | 11.8 | 200 | 3.6 | 1684 | 257.4 | 12.3 | 38.1 | 823.0 | 8.3 | 11.9 |
| 16:11-18:35 | | | | | | | | | | | |
| TEST 8 | | 11.4 | 198 | 3.3 | 1694 | 257.4 | 11.8 | 38.4 | 829.5 | 8.1 | 12.2 |
| 20:33-22:48 | | | | | | | | | | | |

TABLE 3-5B
PROCESS DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST # TIME | UNITS | Main Baghouse | | Bypass Baghouse | | FEED END O2 % | 4TH STAGE TEMP °F | KILN FEED TPH | STACK OPACITY % | TEMP °F | Kiln I.D. Fan | | WDLF FLOW GPM | WDSF FLOW TPH | TIRES FEED TPH |
|----------------|-------|-------------------|------------|-------------------|------------|---------------------|-------------------------|---------------------|-----------------------|------------|-----------------|--------------|---------------------|---------------------|----------------------|
| | | Δ PRESS IN. WC | TEMP °F | Δ PRESS IN. WC | TEMP °F | | | | | | PRESS IN. WC | SPEED RPM | | | |
| 6/25/92 | | | | | | | | | | | | | | | |
| TEST 3 | | 11.6 | 224.8 | 3.5 | 417 | 3.1 | 1644 | 240 | 8.8 | 367 | 38.9 | 862 | 42.6 | 1.79 | 1.5 |
| 8:33-11:33 | | | | | | | | | | | | | | | |
| TEST 4 | | 11.4 | 223.7 | 3.4 | 411 | 3.8 | 1651 | 242 | 8.6 | 367 | 37.9 | 866 | 41.7 | 2.08 | 1.5 |
| 17:48-20:48 | | | | | | | | | | | | | | | |
| TEST 5 | | 11.5 | 220.3 | 3.3 | 410 | 3.6 | 1662 | 241 | 8.2 | 356 | 38.2 | 866 | 41.8 | 1.89 | 1.5 |
| 21:48-00:48 | | | | | | | | | | | | | | | |
| 6/26/92 | | | | | | | | | | | | | | | |
| TEST 7 | | 10.5 | 292.0 | 3.0 | 431 | 4.5 | 1673 | 251 | 9.8 | 386 | 38.6 | 873 | 42.6 | 0.57 | 1.5 |
| 13:49-16:49 | | | | | | | | | | | | | | | |
| TEST 8 | | 10.3 | 305.9 | 3.0 | 433 | 6.9 | 1665 | 251 | 9.0 | 388 | 37.6 | 867 | 43.3 | 0.57 | 1.5 |
| 18:04-20:34 | | | | | | | | | | | | | | | |
| TEST 9 | | 10.3 | 308.5 | 3.0 | 428 | 6.4 | 1669 | 251 | 9.0 | 389 | 38.4 | 869 | 43.3 | 0.83 | 1.5 |
| 21:49-00:19 | | | | | | | | | | | | | | | |

FIGURE 3-3 KILN OPERATION TRENDS - 6/25/92 TEST 3 - (8:33 - 11:33)

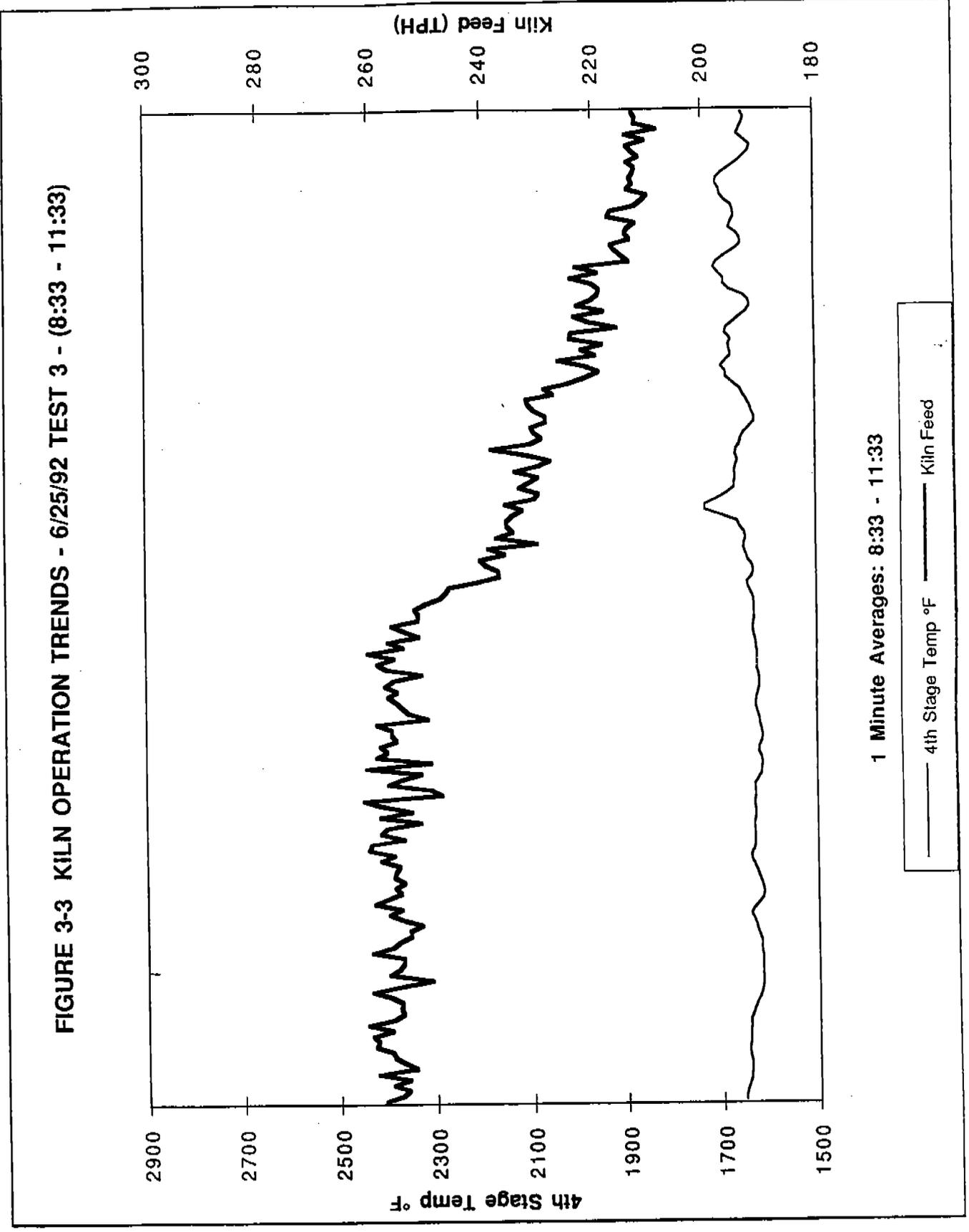


FIGURE 3-4 KILN OPERATION TRENDS - 6/25/92 TEST 4 - (17:48 - 20:48)

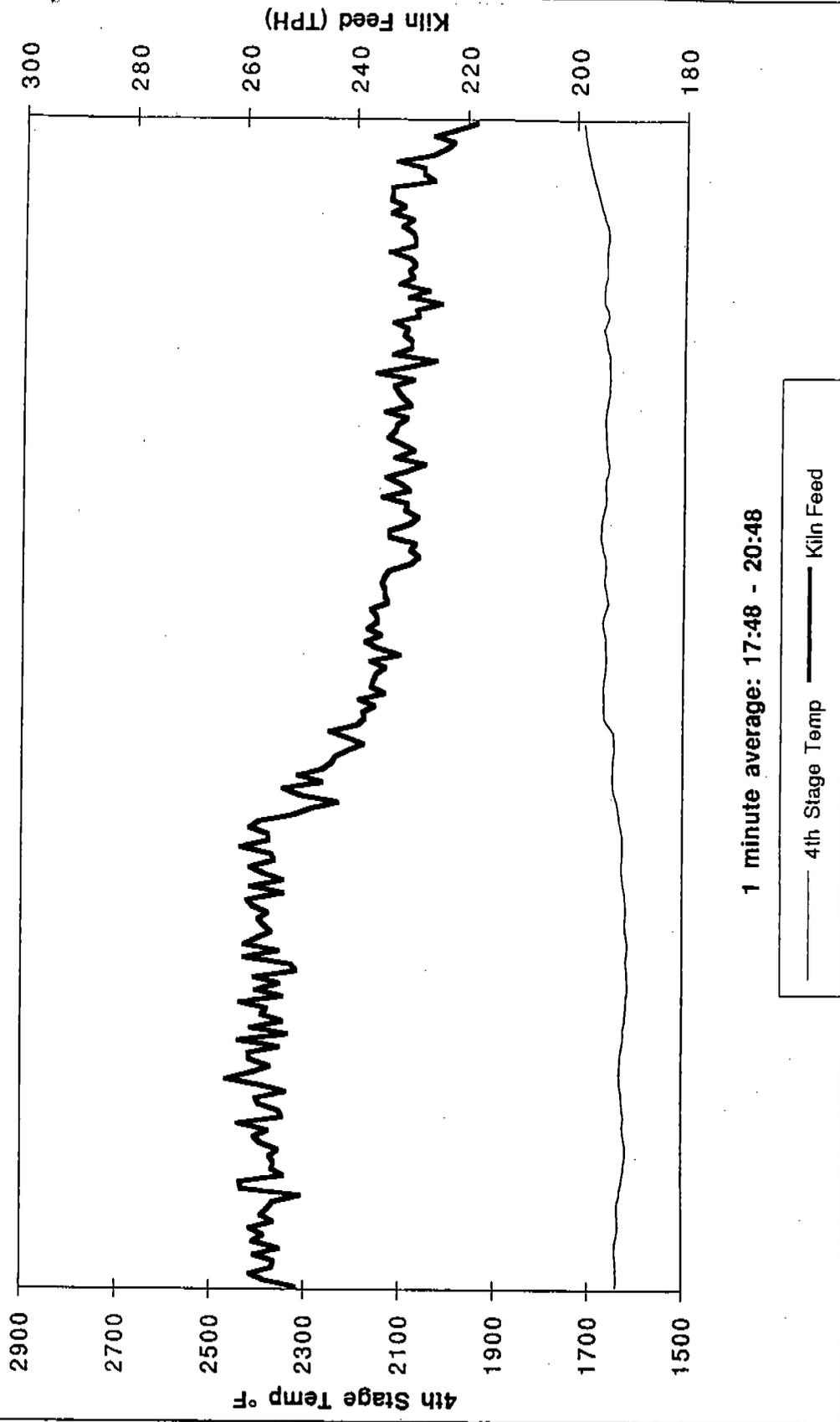


FIGURE 3-5 KILN OPERATION TRENDS - 6/25/92 TEST 5 - (21:48 - 00:48)

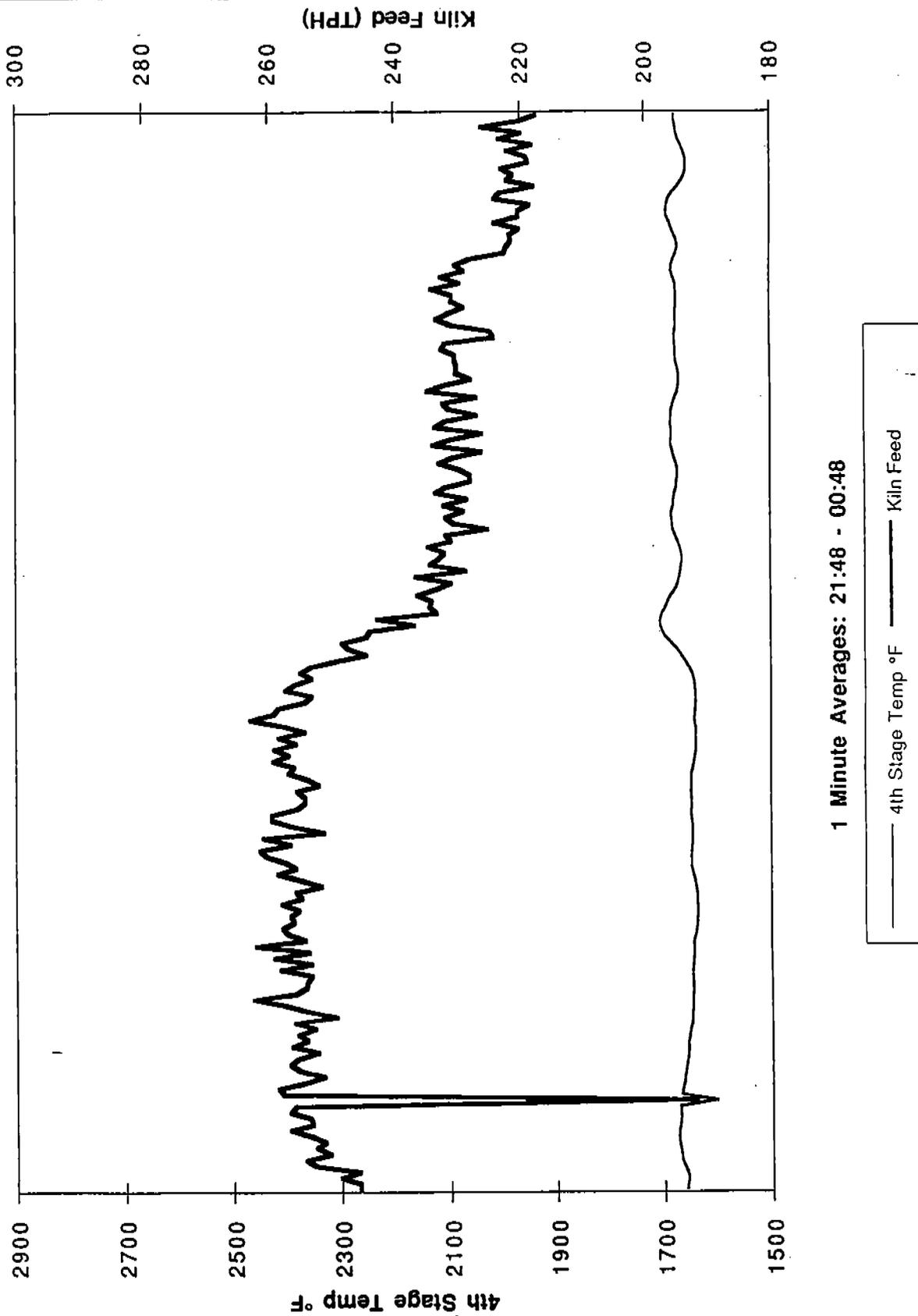


FIGURE 3-6 KILN OPERATION TRENDS - 6/26/92 TEST 7 - (13:49 - 16:49)

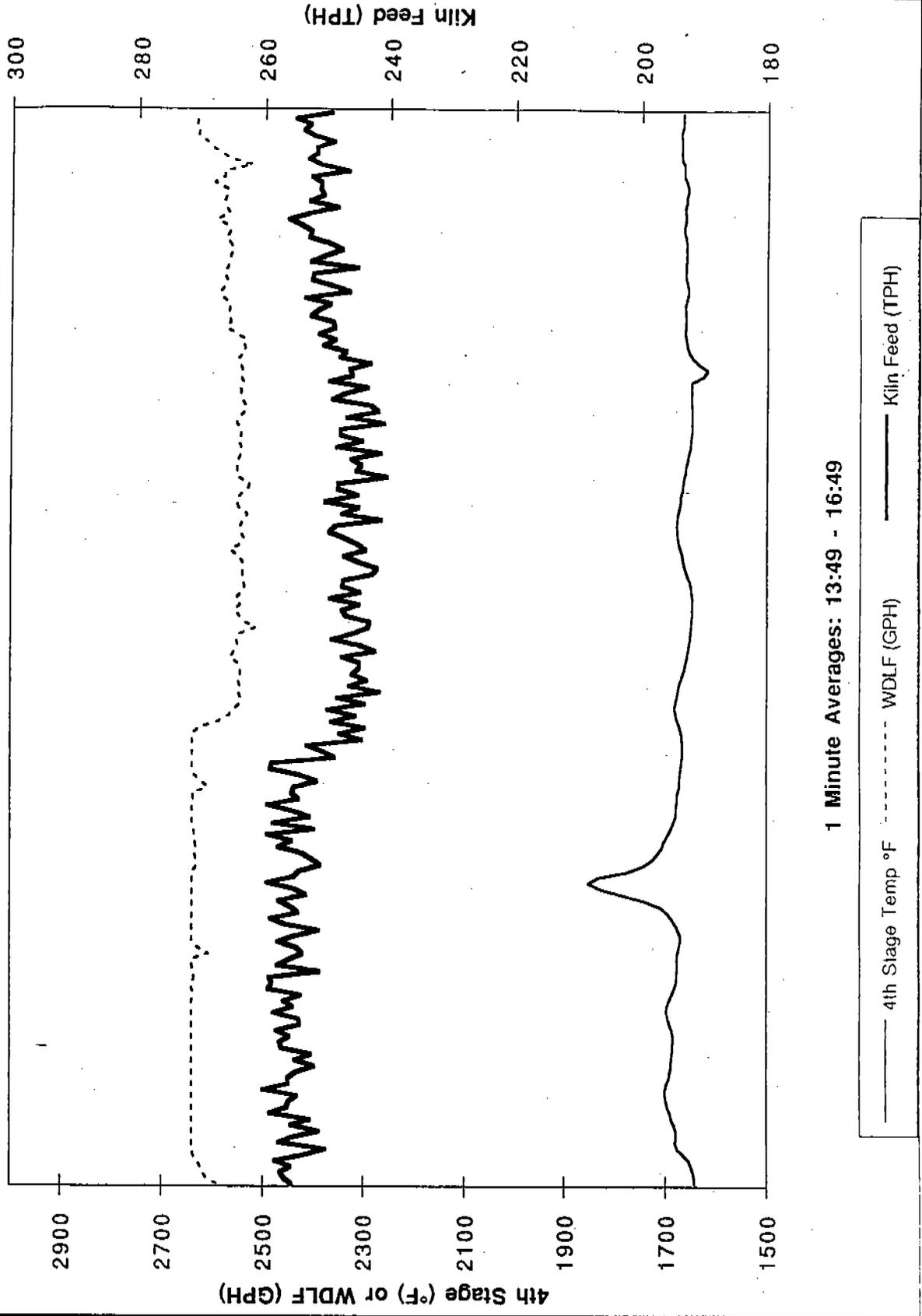


FIGURE 3-7 KILN OPERATION DATA - 6/26/92 TEST 8 - (18:04 - 20:34)

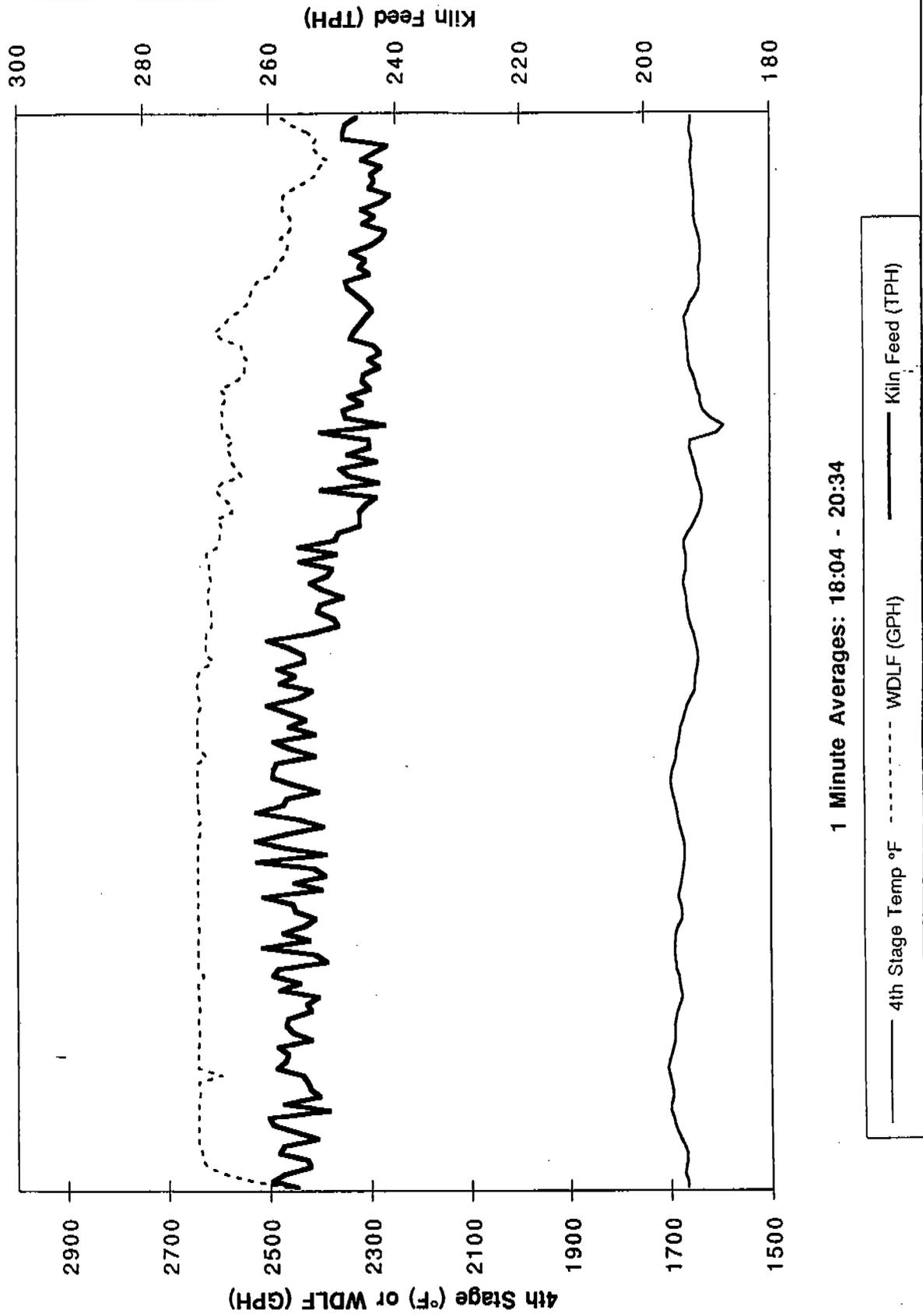
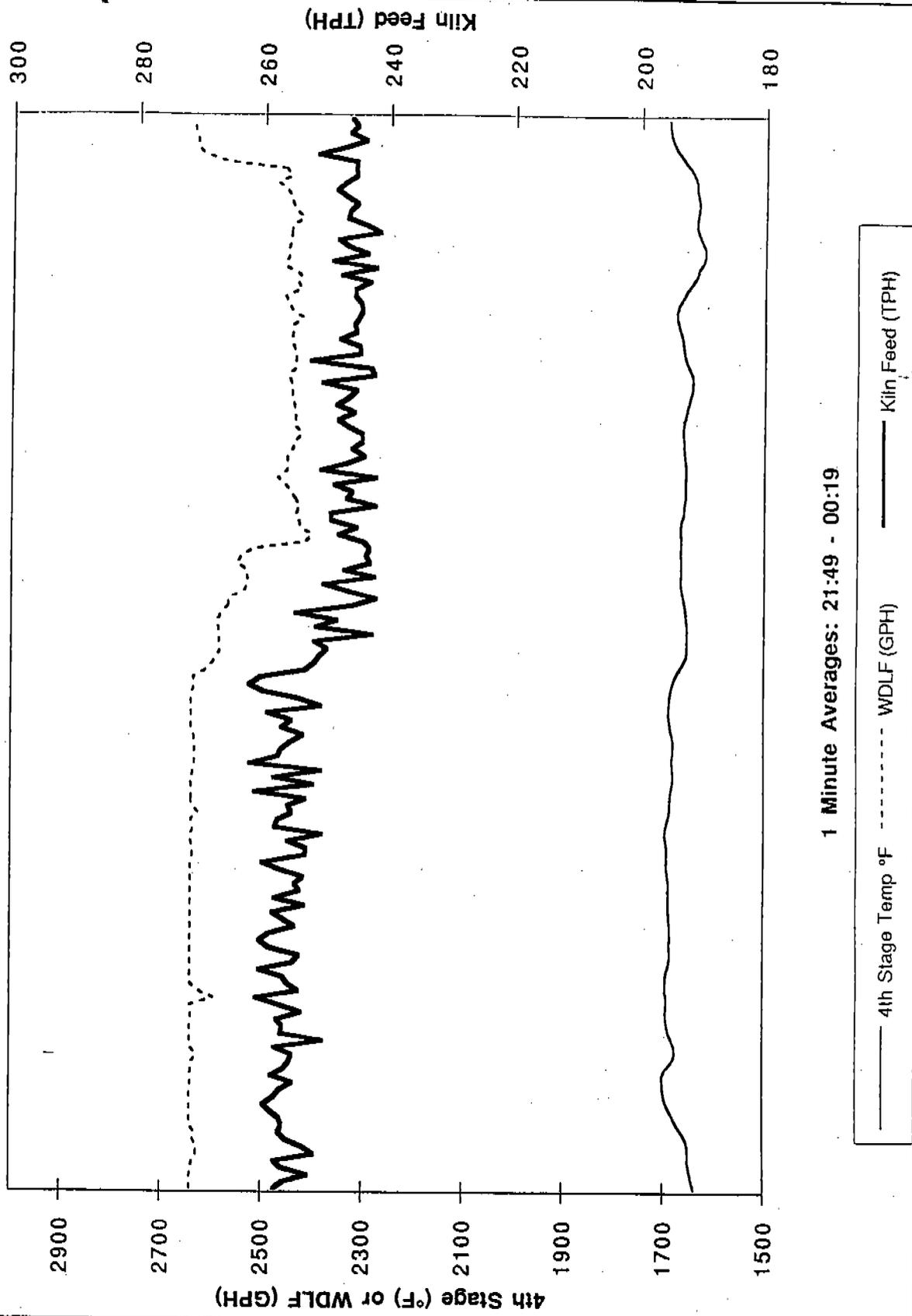


FIGURE 3-8 KILN OPERATION DATA - 6/26/92 TEST 9 - (21:49 - 00:19)



temperatures during each test run, without altering kiln feed following the establishment of the 60-minute rolling average . Due to these factors, it was possible to maintain more "steady state" operations throughout each test period.

3.6 METALS SPIKING

The Lone Star Cape Girardeau plant sampled for six metals under the BIF Tier III Criteria. These metals are Arsenic, Beryllium, Cadmium, Chromium III & VI, Lead, and Mercury. The maximum metals concentrations in the waste fuel as described in the Precompliance Certification are as follows:

| | |
|----------------|---------|
| Arsenic | 170 PPM |
| Beryllium | 3 PPM |
| Cadmium | 400 PPM |
| Chromium (III) | 900 PPM |
| Chromium (VI) | 100 PPM |
| Lead | 700 PPM |
| Mercury | 1.7 PPM |

Prior to the start of each phase of testing, the kiln was allowed to reach equilibrium while burning spiked fuels. Lone Star determine equilibrium by spiking the waste fuel with metals and taking half-hourly dust samples from the kiln. The samples was analyzed for the surrogate metals. When the plot of the lbs/hr inputs flattened, then equilibrium was reached. These data are presented in Appendix D:

With the exception of Cr⁺⁶, these metals were introduced into the pumpable hazardous waste feed stream and, therefore, represent the most conservative approach to obtain the maximum level of metals allowed in all feed streams. However, it was not possible to obtain the maximum level of all metals as a hazardous feed stream, and therefore it was necessary to spike some of the metal to achieve maximum metal feed rates. Cr⁺⁶ was spiked as a powder through the kiln coal injection system.

During the metal testing for BIF compliance the pumpable hazardous feed stream was sampled at 15 minute intervals, composited, and analyzed for metals for each test period. Prior to the start of the test, 80,000 gallons (2 tanks) were adjusted for the maximum metals concentrations.

Prior to and during each test the feed stream was adjusted for total metals input by spiking. The method of spiking was to add the metals in fine powered form to the coal system that blows coal in the front of the kiln. The metals were added through a rotary feeder directly into the pulverized coal transport pipe. The powdered metal was blown into the kiln directly into the flame. This represents a conservative approach since the metals in powered form entering the flame volatilize very rapidly. All Cr⁺⁶ were added like this.

The compounds used for spiking metal were:

Beryllium sulfate
Cadmium oxide
Potassium dichromate (Cr⁺⁶)

Lead oxide
Mercuric chloride
Chromium III oxide

The use of pumpable hazardous stream with maximum metal concentration and metal spiking began 12 hours before the stack test for metal removal efficiency. This was to ensure that the kiln system achieved equilibrium conditions with respect to metals. Samples of inputs and outputs were taken every 30 minutes during this period to establish when equilibrium was reached. Metal removal efficiency was determined while burning coal (precalciner), hazardous waste and tires.

Since the Lone Star Cape Girardeau plant also proposed to burn solid hazardous waste by injecting the pails into the burning zone of the kiln, pails were also injected into the kiln burning zone via an air cannon during the entire test. The injection was done during the same time interval as the metal spiking occurred. No spiked metal was introduced into these solid streams. The metals introduced by the solid stream were accounted for in the total metal input to the kiln system. The pails were injected into the kiln approximately 70-90 feet from the material discharge end of the kiln. The gas temperature at this point in the kiln is in excess of 3000° F. The material temperature is above 2300° F.

To ensure maximum volatilization of metals during this compliance testing maximum combustion zone temperature and maximum flue gas temperature entering the PM control device were achieved. The burning zone control for maximum temperature was the 4th stage gas inlet temperature which represents the position nearest the burning zone where temperature can be reliably measured. Temperature entering the main and bypass fabric filter APCD was monitored on a continual basis and maximized during this testing.

* 3.7 POHC SPIKING

The COC test meets the requirements of the State of Missouri Department of Air Management. This department required Lone Star to conduct performance testing within 60 days of achieving maximum hazardous fuel kiln rate and in no case later than 180 days after the initial burn date of April 28, 1992. The testing was to demonstrate the following destruction and removal efficiencies:

| | |
|-----------|--------|
| Lead | 98% |
| Mercury | 33% |
| Beryllium | 99% |
| VOC - | 99.99% |

To determine compliance with the organic emission limits, testing was performed with the kiln operating at minimum burning zone temperature conditions. To ensure this condition, the temperature was monitored at the 4th stage preheater inlet. This is the position nearest the burning zone where temperature can reliably be measured. This is the most conservative approach to prove thermal destruction of POHC.

To demonstrate 99.99% destruction of volatile organic compounds, principal organic hazardous constituents (POHC) were spiked in the liquid pumpable hazardous waste streams. The emissions of POHC were sampled in the stack in order to calculate the destruction and removal efficiency (DRE). Perchloroethylene (C₂Cl₄) and 1,1,1 trichloroethane (C₂H₃Cl₃) and 1,1,2 trichloroethane (C₂H₃Cl₃) were used as surrogate POHC for this program.

To ensure that sufficient POHC was introduced to the kiln, each POHC was planned to be burned at approximately 100 lbs/hr. This was assuming that the stack flow rate is 260,000 scfm and the POHC detection limit is 1 ng/l. Since this hazardous fuel stream was burned at approximately 44 gal/min during the testing, a blend tank containing approximately 1 % of each POHC was prepared prior to the test. This material was then burned for the duration of the DRE test for volatile organic compounds. The burning of the fuel containing the POHC began at least two hours prior to testing. This provided sufficient time to achieve equilibrium in the kiln.

The particular POHC were chosen to demonstrate the thermal destruction of cement kilns because:

1. According to the Thermal Stability Index and Heat of Combustion, these POHC's are difficult to destroy.
2. These compounds can be analyzed relatively free of interference, and therefore measured with precision.
3. These compounds are not known to be products of incomplete combustion from coal or hazardous waste. They are therefore indicators of performance independent of other compounds in the process.

3.8 PROCESS MASS BALANCE SAMPLING

A sample was drawn from the spiked WDLF mix tank after it had been circulated for a period of at least four hours and was well mixed. The sample was analyzed for POHC, metals, chlorine, total chloride and Burn Specifications prior to use. Samples of raw materials and product were taken during the COC emission tests at 15 minute intervals and composited for chlorides & metals analyses.

Raw Materials

- Coal feed belts (2)
- Water for the Conditioning Tower
- Raw material feed
- Tire feed
- WDLF feed
- WDSF feed
- Spent kiln brick (not available during COC)

Product

- Clinker cooler conveyer
- Kiln dust
- Bypass baghousehopper

4.0 SAMPLING AND ANALYTICAL METHODS

Air pollution emission measurements were performed during the COC at the single exhaust stack to determine emission concentrations and rates of particulate matter (PM), heavy metals (HM), chlorides (HCl), chlorine (Cl₂), Principal Organic Hazardous Constituents (POHC) and Hexavalent Chromium (Cr⁺⁶). Carbon monoxide (CO), Total Hydrocarbons (THC) and oxygen (O₂) measurements were performed at the main stack (APCC CEMS) as well as the kiln bypass (Lone Star CEMS) to determine compliance with BIF regulations.

In addition to the air pollution measurements, product samples were drawn from the dust collector, kiln dust duct, and clinker cooler discharge conveyer. Raw feed samples were taken at the entrance to the kiln at the back end. WDLF samples were drawn from the feed loop pipe on the burner floor. Pails were opened prior to injection into the air cannon and samples drawn. Coal samples were taken from the coal transport pipes to the pre-calciner. Tires were sampled from the feed bin. Water samples were taken from the conditioning tower. Samples were analyzed for metals, chloride and chlorine content in order to perform a mass balance of the kiln system.

4.1 STACK EMISSION MEASUREMENTS

Emission measurements were performed to determine emission concentrations and rates of PM, heavy metals, Cr⁺⁶, chloride, chlorine, POHC, THC, CO, O₂ and CO₂. Sampling was performed in accordance with EPA Reference Methods 1, 2, 3, 3A, 4, 5 (modified), 10, 25A and SW 846 0012, 0030, and 0050.

4.1.1 Particulate, HCl, and Chlorine Emission Measurements

Emissions of Particulate, Hydrogen Chloride (HCl) and Chlorine (Cl₂) were determined in accordance with EPA Methods 1-5 and SW 846 Method 0050 as published in the December 1990, Methods Manual For Compliance With The BIF Regulations. Sampling and analyses were performed in strict accordance with the method using a sampling train schematically similar to the one presented in Appendix E.

The glass nozzle is attached to a glass-lined probe which is heated to 248±25°F to prevent condensation. Pall quartz filter paper supported in a 4-1/2 inch Teflon filter holder is used as the collection media. The filter assembly is enclosed in a heated box to maintain temperatures of 248±25°F to prevent condensation. A thermocouple is located inside the back half of the filter holder to monitor the gas stream temperature. An ice bath containing six impingers is attached to the back end of the filter via a flexible Teflon sample line.

The first impinger (optional) contains 50 ml of 0.1N sulfuric acid and is used as an additional moisture knockout. The second and third impingers each contain 100 ml of 0.1N sulfuric acid. The fourth and fifth impingers each contain 100 ml of 0.1N sodium hydroxide. The sixth contains 200 g indicating silica gel to remove any remaining moisture from the sampling train. Flexible tubing, vacuum gauge, needle

valves, leakless vacuum pump, bypass valve, dry gas meter, calibration orifice and inclined manometer complete the sampling train. The stack velocity pressure is measured using an S-type pitot and inclined manometer. The stack temperature is monitored by a thermocouple connected to a potentiometer.

A nomograph is used to quickly determine the orifice pressure drop required for a pitot velocity pressure and stack temperature in order to maintain isokinetic sampling conditions. Sampling flow is adjusted by means of the bypass valve. Before and after each particulate test run, the sampling train is leak checked (acceptable at less than 0.02 cfm).

Sample recovery was performed in a relatively clean, environmentally controlled shelter constructed on the pre-heater tower. After the probe has been removed from the stack and allowed to cool, particulate matter is wiped from the exterior of the nozzle and the nozzle capped to prevent loss (or gain) of sample. The Teflon sample line is then removed from the filter holder and impinger train. The filter outlet is sealed with Para-film. The Teflon sample line is sealed at both ends. The impinger outlet vacuum line is then removed and the impinger train sealed. The impinger train is inspected and abnormal conditions noted before disassembly. Samples are recovered and placed in Teflon sealed glass containers as follows:

- Container No. 1 - The 4-1/2 inch quartz filter is removed from its holder and placed in a petri dish, sealed, and labeled.
- Container No. 2 - The probe, nozzle, and front half of the filter holder are brushed and rinsed three times with acetone. The wash is deposited in a 500 ml sample jar and labeled.
- Container No. 3 - The volume of the first, second and third impinger solutions are measured and recorded. The solutions are then deposited in a 500 ml or 1000 ml glass sample jar. The impinger, Teflon line, and the back half of the filter holder are then rinsed three times DI water and the rinse added to the impinger solutions. The jar is sealed and labeled, and the liquid level marked.
- Container No. 4 - The volume of the fourth and fifth impinger solutions are measured and recorded. The solutions are then deposited in a 500 ml glass sample jar. The impingers are then rinsed three times with DI water and the rinse added to the impinger solutions. The jar is sealed and labeled, and the liquid level marked.
- Container No. 5 - The silica gel is replaced in its original container.

The samples will be transported to the laboratory and analyzed utilizing EPA Methods 5 and 9057 (ion chromatography) in accordance with the sampling method 0050.

- Container No. 1- Desiccate and weigh to constant weight.
- Container No. 2- Evaporate at ambient pressure and temperature. Desiccate and weigh to constant weight.
- Container No. 3- Analyze chloride content by Ion Chromatography
- Container No. 4- Analyze chlorine content by Ion Chromatography
- Container No. 5 - Weigh silica gel to the nearest 0.5 g. The weight of the moisture entrapped in the silica gel, along with the weight of moisture which is condensed in the impingers, is used to calculate the moisture content of the flue gas.

Computer programs developed for the Macintosh computer and HP-41CX hand held calculator are used to calculate emission rates in grains per dry standard cubic foot, $\mu\text{g}/\text{m}^3$ and pounds per hour. The program also calculates percent moisture, molecular weight of the stack gas at stack conditions, and the percent isokinetic.

4.1.2 O₂, CO₂ and CO Manual Determination

An integrated gas sample is drawn from the main exhaust stack into a Tedlar bag at approximately 0.25 lpm simultaneously with each reference method test performed as described in Sections 3.1.1, and 3.1.3. These samples are drawn through a probe integral with the main sampling probe and analyzed on a dry basis in accordance with EPA Method 3A using combustion gas analyzers as described below in Section 4.1.6. Percent CO₂ and O₂, as well as ppm CO and the molecular weight of the gas stream, are determined from the analyses, which were used only as a QA check on the CEMS.

4.1.3 Heavy Metals Emission Measurement

Sampling was performed to determine emissions of heavy metals utilizing a modified EPA Method 5 sampling train and the SW Method 0012, "Methodology for the Determination of Metals Emissions in Exhaust Gases from Hazardous Waste Incineration and Similar Combustion Processes" as presented in 40 CFR 266.106, Appendix IX. Samples were analyzed for As, Be, Cd, Cr, Pb, & Hg.

Sample Collection

Sampling was performed isokinetically at traverse points as presented in Section 5. A typical sample volume 80 to 90 dscf in order to achieve minimum desired detection limits.

Metals sampling was performed using the modified EPA Method 5 collection train, described in the July 1, 1984 edition of the Federal Register as well as the method referenced above. It is shown schematically in Appendix E and consists of a quartz nozzle, probe, filter, a flexible Teflon umbilical line, seven impingers, vacuum pump, dry gas meter, and an orifice flow meter. The modification of this standard EPA

Method 5 train consists of placing a flexible Teflon sample line between the filter and the impingers. This modification makes the sampling equipment much less awkward. Complete sampling train calibrations are performed before and after every compliance test program.

A quartz nozzle is attached to a glass-lined probe which is heated to $248 \pm 25^\circ\text{F}$ to prevent condensation of moisture. Whatman glass fiber EPM 2000 filter paper supported in a 4-1/2 inch glass filter holder (Teflon frit) is used as the collection media. The filter assembly is enclosed in a heated box to maintain temperatures at $248 \pm 25^\circ\text{F}$. A thermocouple is located inside the back half of the filter holder, to monitor the gas stream temperature and verify that it is kept at $248 \pm 25^\circ\text{F}$. An ice bath containing seven impingers is attached to the back end of the filter via a flexible Teflon tube. The first impinger (optional) is left empty and is used as an additional moisture knockout in high moisture stack streams. The second and third impingers each contain 100 ml of 5% nitric acid/10% hydrogen peroxide solution. The fourth impinger is empty. The fifth and sixth each contain 100 ml 4% potassium permanganate / 10% sulfuric acid solution, and the seventh contains 200 g of indicating silica gel to remove any remaining moisture. Flexible tubing, vacuum gauge, needle valve, leakless vacuum pump, bypass valve, dry gas meter, calibrated orifice and inclined manometer complete the sampling train. The stack velocity pressure is measured using an S-type pitot tube and inclined manometer. The stack temperature is monitored by a thermocouple that is attached to the pitot and connected to a potentiometer. A check valve is not used in this sampling train.

A nomograph is used to quickly determine the orifice pressure drop required for any pitot velocity pressure and stack temperature in order to maintain isokinetic sampling conditions. Sampling flow is adjusted by means of the bypass valve. Before and after each test run the sampling train is leak checked (acceptable at less than 0.02 cfm). Test data is recorded on field data sheets as presented in the Appendix B.

Sample Recovery

Sample recovery was performed in a relatively clean, environmentally controlled shelter constructed on the pre-heater tower. After the probe has been removed from the stack and allowed to cool, particulate matter is wiped from the exterior of the nozzle and the nozzle capped with Parafilm to prevent loss (or gain) of sample. The Teflon sample line is then removed from the filter holder and impinger train. The filter outlet is sealed with Parafilm. The Teflon sample line is sealed at both ends. The impinger outlet vacuum line is then removed and the impinger train sealed. The impinger train is inspected and abnormal conditions noted before disassembly. Samples are recovered and placed in Teflon sealed glass containers as follows:

- Container No. 1 The 4-1/2 inch glass fiber filter is removed from its holder and placed in a 1000 ml sample jar and labeled. The probe, nozzle, and front half of the filter holder are brushed and rinsed three times with nitric acid solution. The wash is deposited into the same container.

- Container No. 2 The volumes of the first three impingers are measured and recorded. The solutions are then deposited in a 1000 ml glass sample jar. The impingers, Teflon line, and the back half of the filter holder are then rinsed three times with nitric acid solution and the rinse added to the impinger solutions. The jar is sealed and labeled, and the liquid level marked.
- Container No. 3 The volume of the fourth impinger is determined and the contents emptied into a 500 ml sample jar. The impinger is then rinsed in triplicate with 100 ml nitric acid solution. The jar is sealed and labeled, and the liquid level marked.
- Container No. 4 The volume of the fifth and sixth impinger is determined and the contents emptied into a 500 ml sample jar. The impinger is then rinsed in triplicate with potassium permanganate solution and added to the container. Any remaining residue is then removed by rinsing with DI water and also deposited into the container. The jar is sealed and labeled, and the liquid level marked.
- Container No. 5 Any remaining residue in the fifth and sixth impingers is removed by rinsing with 8N HCl, and deposited in the container. The jar is sealed and labeled and the liquid level marked. This container is optional and only for cleaning any remaining residue after the DI rinse.
- Container No. 6 The silica gel is replaced in its original container.

Sample Analysis

Sample analyses were performed by Triangle Laboratories (TL), Inc. at Research Triangle Park, NC following SW Method 0012, "Methodology for the Determination of Metals Emissions in Exhaust Gases from Hazardous Waste Incineration and Similar Combustion Processes" guidelines by graphite furnace atomic absorption spectroscopy (GF-AAS), inductively coupled argon plasmography (ICAP), or cold vapor atomic absorption spectroscopy (CV-AAS). The technique with the lowest analytical detection limit was utilized for each metal.

- Container No. 1 The filter is divided into 0.5 g portions and digested by microwave or Par bomb method and combined with the acid digestion of probe rinse.

The nitric acid wash is acidified to a pH 2, reduced to dryness and digested as Container No.1. The sample is then combined with Container No.1 filtered and diluted. A 50 ml aliquot is taken and analyzed for Hg by CV-AAS. The remainder of sample is then analyzed for heavy metals by GF-AAS or ICAP.

- Container No. 2 A 75 to 100 ml aliquot is taken and analyzed for Hg by CV AAS. The impinger solution is acidified with nitric acid to a pH 2, reduced to dryness and digested by conventional or microwave method. The sample is then analyzed for heavy metals by GF-AAS.
- Container No. 3 The volume of this container is measured. The sample is then analyzed for Hg by CV-AAS.
- Container No. 4 The volume of this container is measured. The sample is then analyzed for Hg by CV-AAS.
- Container No. 5 The volume of this container is measured and diluted to 500 ml. The sample is then analyzed for Hg by CV AAS.
- Container No. 6 The silica gel is weighed to the nearest 0.5 grams.

Blank filters and reagents taken prior to the test program and during the actual field test are analyzed in a manner identical to the actual samples in order to detect for background contamination.

4.1.4 Volatile POHC / DRE

Sampling was performed to determine the emission rate of Volatile POHC listed in Section 3.7 by utilizing the EPA Volatile Organic Sampling Train (VOST) procedure as outlined in EPA-SW 846 Method 0030, Destruction and Removal Efficiency (DRE) of volatile Principal Organic Hazardous Compounds (POHC). The slow VOST option was used. Four 40-minute samples comprise each test.

Sample Collection

A 20-liter (nominal) sample of effluent gas is drawn from the source at a flow rate of approximately 0.5 liters per minute for 40 minutes, using a heated (250±25°F) glass lined probe and a VOST sampling train. A schematic of the train is shown in Appendix E. The gas stream is cooled to <20°C by passage through a water cooled condenser and VOC are collected on a pair of sorbent resin traps. Liquid condensate is collected in an impinger placed between the two resin traps. The first resin trap (front trap) contains approximately 1.6 grams Tenax and the second trap (back trap) contains approximately one gram each of Tenax and petroleum based charcoal, 3:1 by volume. A total of four pairs of sorbent traps will be used to collect volatile POHCs from the effluent gas stream for each test. Three pairs of traps for each test run will be analyzed in tandem, with the fourth pair of traps analyzed separately. A total of four tests (16 cartridge pairs) will be performed. A velocity traverse will be performed in accordance with EPA Methods 1 and 2 during each test in order to determine exhaust volumetric flowrate and mass emission rates.

Sample Recovery

All sample cartridges were sealed with Swage-lok fittings and kept on ice until ready for analysis. Condensate was recovered and combined for each test series. Only a few ml were collected in four test runs combined since most of the moisture was adsorbed by the Tenax.

Sample Analysis

Sample analysis was performed by Triangle Laboratories (TL), Inc. at Research Triangle Park, NC. The contents of the paired sorbent cartridges are spiked with an internal standard and thermally desorbed for 10 minutes at 180°C with the carrier gas flow reversed so that the effluent flow from the analytical trap is directed into the GC/MS. The VOC are separated by temperature programmed gas chromatography and detected by low resolution mass spectrometry. The concentrations of VOC are calculated using the internal standard technique. Condensate samples are analyzed in a similar manner. Results are typically in the nanogram range. VOC concentrations were determined by analyzing the cartridges separately in the first sample and when not found in the range of suspected breakthrough, the remaining cartridges were analyzed in pairs.

4.1.5 Hexavalent Chromium

Sampling was performed to determine the emission rate of hexavalent chromium (Phase 2 only) by utilizing the EPA Method Cr⁺⁶ - Determination of Hexavalent Chromium Emissions From Stationary Sources. A sampling train schematically similar to the one presented in Appendix E was used.

Sample Collection

All portions of the Cr⁺⁶ sampling train that come in contact with the gas sample are either glass, quartz, Tygon or Teflon. The metering system used in this sampling train is identical to that specified by EPA Method 5 described above.

The probe nozzle is glass with a sharp, tapered leading edge. A Teflon union-T is connected behind the nozzle to provide the absorbing reagent / sample gas mix. A peristaltic pump is used to recirculate the absorbing reagent at a flow rate of at least 50 ml/min. Fittings, recirculating line, and sample line to the union-T are Teflon. 3/8" O.D. Teflon tubing is used to connect the union-T to the first Teflon impinger and recirculating pump. Three impingers are constructed of Teflon, with the fourth and fifth (silica gel) impingers made of glass. A schematic of this train is found in Appendix E.

Approximately 150 ml of 0.5N KOH reagent is placed in the first Teflon impinger. This is a variation from the 0.1N solution specified in the method necessary to maintain an alkaline solution while sampling acidic stack gases. The second and third impingers have approximately 75 ml of the same 0.5N KOH. The fourth impinger is left empty. The fifth impinger (glass) contains a preweighed 200g portion of indicating silica gel. Reagent blanks are retained for analyses. Flexible tubing, vacuum gauge, needle valves, leakless vacuum pump, bypass valve, dry gas meter, calibration orifice

and inclined manometer complete the sampling train. The stack velocity pressure is measured using an S-type pitot and inclined manometer. The stack temperature is monitored by a thermocouple connected to a potentiometer.

A post-nitrogen purge of the impinger train is used as a safeguard against the conversion of hexavalent chromium to the trivalent oxidation state. The purge is effective in the removal of SO₂ from the impinger contents. The nitrogen is purged at an approximate rate of 10 lpm for 30 minutes.

A nomograph is used to quickly determine the orifice pressure drop required for a pitot velocity pressure and stack temperature in order to maintain isokinetic sampling conditions. Sampling flow is adjusted by means of the bypass valve. Before and after each test run, the sampling train is leak checked (acceptable at less than 0.02 CFM). At the end of the sampling run, the pH of the reagent in the first impinger is measured using a pH indicator strip. The pH of the solution must be greater than 8.5.

Sample recovery was performed in a relatively clean, environmentally controlled shelter constructed on the pre-heater tower. The probe assembly is allowed to cool prior to sample recovery. When the probe assembly can be safely handled, all external particulate matter near the tip of the nozzle is wiped off and the nozzle capped prior to transporting the sample train to the cleanup area. The impinger train is inspected and abnormal conditions noted before disassembly. Samples are recovered and placed in containers as follows:

- Container No. 1 - Impingers 1 - 3 are disconnected and drained into a precleaned graduated cylinder. The volume of the liquid is measured to within 1 ml.
- Container No. 2- Note the color of the silica gel to determine if it has been completely spent. Quantitatively transfer the silica gel from its impinger to the original container, and seal the container.

For determination of hexavalent chromium, the sample is filtered immediately following recovery to remove any insoluble matter. Nitrogen gas is used as a pressure assist to the filtration process (see figure in the Appendix). The entire sampling train is then cleaned by rinsing three times with 0.5N HNO₃ prior to reuse.

Sample Analysis

The Cr⁺⁶ content of the sample filtrate is determined by ion chromatography coupled with a post column reactor (IC/PCR). Sample analysis was performed by Research Triangle Institute (RTI), Inc at Research Triangle Park, NC.

4.1.6 Continuous Emission Monitoring of CO, THC, O₂, and CO₂

Continuous emission monitoring (CEM) was performed at the exhaust stack to determine concentrations and emission rates of CO and THC as well as diluent concentrations of O₂ and CO₂. Lone Star also monitored CO, THC and O₂

concentrations with their in-plant analyzers located at the kiln bypass. These data were used to set CO operational limits. An additional in-plant system monitors at the outlet of the preheater and at the exhaust stack.

All APCC CEM data was recorded using a Tracor/Westronics automatic digital data logger. The CEM system was housed in the APCC Environmental Monitoring Laboratory (EML) at the base of the exhaust stack.

Sample Conditioning System

An in-stack thimble filter serves to remove large particulate matter from the sample gas stream. The thimble filter is mounted on the front end of a heated ($250^{\circ}\text{F} \pm 25^{\circ}\text{F}$) stainless steel sampling probe with a stainless steel nozzle facing away from the stack gas flow. The sample stream is then drawn through heated (300°F nominal) Teflon sample line to four modified Greenburg-Smith type impingers (with impingement stems broken off) immersed in an ice-bath to remove the moisture from the gas stream. The sample is then drawn through Teflon tubing by a leak-free Teflon double diaphragm pump to a stainless steel sample manifold with an atmospheric bypass rotameter. The CO, O₂, and CO₂ analyzers draw sample gas from this manifold. The THC sample is drawn prior to the condensor.

Continuous Emission Monitoring Analyzers

Emission parameters to be continuously monitored by APCC are CO, THC, O₂ and CO₂. Oxygen and carbon dioxide concentrations will be monitored in accordance with EPA Method 3A, carbon monoxide concentrations will be monitored in accordance with EPA Method 10 and THC will be monitored in accordance with EPA Method 25A..

A TECO gas filter correlation nondispersive infrared gas analyzer was used to continuously monitor concentrations of CO in the exhaust stream. The analyzer operates on the measurement principle based on CO having a characteristic absorption spectra in the infrared range. It contains an infrared detector that uses the nondispersive single beam technique with alternate modulation of the sample and reference cells. Radiation absorbed by CO in the sample cell produces a capacitance change in the detector which is proportional to the CO concentration.

A RATFISCH Model RS55 Total Hydrocarbon Analyzer, which utilizes a flame ionization detector (FID) to measure, as carbon, hydrocarbons C₁ through C₁₈; was calibrated as propane. Approximately 5.0 lpm of sample gas is drawn from the stack through 50 feet of Teflon sample line heated to 350° F (nominal). The sample gas is drawn through a heated filter and valving by a heated pump. The sample gas then enters the heated detector bench which contains the FID. Flame ionization is a process of continuously creating ions by flame, whereby, upon combustion, hydrocarbon molecules and carbon atoms are separated into positive ions and free electrons. The positive ions are attracted to the burner (-); the free electrons are attracted to the collector cylinder (+). An electron flow is established from the burner to the collector cylinder, proportional to the ionization created by the flame. The resulting

current is detected and amplified by an electrometer/amplifier circuit. The output of the amplifier provides a signal to a recorder for real-time continuous monitoring.

A Westinghouse/Maihak OXIGOR O₂ analyzer was used to monitor concentrations of oxygen in the exhaust stream. This instrument utilizes the magnetic dumbbell sphere (paramagnetic) principle, which comparatively measures the magnetic susceptibility of a gas volume by the force acting upon a non-magnetic test body suspended in a disproportionate magnetic field. Output current is linearly proportional to the oxygen concentration.

A Westinghouse/Maihak FINOR CO₂ analyzer was used to monitor carbon dioxide emissions. This instrument operates on the principle of carbon dioxide having a known characteristic absorption spectra in the infrared range. Radiation absorbed by CO₂ in the sample cell produces a capacitance change in the detector which is proportional to the CO₂ concentration.

Data Acquisition and Handling

All CEM data was monitored by a Tracor/Westronics 3000 digital data logger which will record using its integral color printer. Trends will be monitored using the strip chart mode for CO, THC, O₂, CO₂ and stack temperature with averages printed digitally for 15-minute intervals and/or the test period. Emission data will be "viewed" by the data logger at 10-second intervals. This will enable real-time emission data to be available on-site.

Stratification Check

Prior to the CEM system coming on-line for the COC, a stratification check was performed at the sampling location. Twenty-four traverse points as described in Section 5.1 were sampled for CO and oxygen to detect the presence of stratification and to determine a point of average concentration for sampling. The plant CEM system was used as the point of reference. The CEM probe was then positioned at the point of average concentration for the remainder of the test program. Significant stratification was not detected.

CEM System Calibrations

Calibrations of the CEM system were performed at the beginning and end of each test using either EPA Protocol 1 and/or NBS Traceable calibration gases. Calibration gases (zero, mid range and span) were introduced to the CEM system through a 3-way heated valve located at the back of the sampling probe. Each analyzer was also multi-point calibrated prior to the trial burn to establish instrument linearity. A three point calibration of each analyzer (four point for THC), along with system leak and bias checks was performed at the beginning and end of each test day.

4.2 COMBUSTION EFFICIENCY

The combustion efficiency of the kiln cannot be determined using the CO and CO₂ concentrations as used for a typical combustion source. The calcination of limestone

and the clinkering process release a significant amount of CO₂ as well as CO that renders this calculation impractical.

4.3 RAW MATERIAL AND PRODUCT SAMPLES

Samples of raw materials (raw feed, WDLF, WDSF, tires, water, coal) and product (clinker baghouse and kiln dusts) were taken by plant personnel to evaluate levels and to attempt a metals, chloride and chlorine mass balance on the kiln. Samples were drawn on a grab sample basis at 15 minute intervals during each test and composited for all parameters except the WDLF. The WDLF sample was collected by a continuous drip methodology described below.

One glass sample jar was filled at each of the following sample locations as shown in Figure 5-2.

Raw Materials:

- Raw Material Feed
- Coal Feed Belts (2)
- Water for Conditioning Tower
- Shredded Tires
- WDLF Feed Pipe
- WDSF Pails
- Spent kiln brick (if available)

Product:

- Kiln Dust
- Clinker Cooler Conveyer
- By-pass Baghouse Hopper

WDLF samples were drawn using Method S-004. This method is designed for collecting integrated liquid samples from moving streams through a submerged fill pipe. The sample was kept on ice during sampling to reduce evaporation.

Analyses of composite samples of kiln raw materials and products drawn by Lone Star personnel were performed for the corresponding parameters by the methodologies indicated in Table 4-1. Additional analyses were performed on-site by ECL (metals and Btu).

A total of 12 composite samples plus audits of each type were analyzed. Triangle Labs performed metals analyses, Environmental Health Laboratories of Hartford, CT chlorides analyses, and Gould Engineering the chloride and Btu analyses on WDLF, WDSF and coal samples.

Bypass dust mass flowrate was quantified by measuring the weight collected dust in the silos at the beginning and end of each test day.

TABLE 4-1

MASS BALANCE METHODS OF ANALYSES
COMPLIANCE TEST PROGRAM
LONESTAR INDUSTRIES

| Sample Matrix | Analytical Parameter | Preparation Method | Analytical Method |
|--------------------|---|--------------------|--|
| INPUT Raw Mix | Metals* Chloride | SW 3050 | SW 6010/7000 series ASTM C-114-19 |
| WDSF | FOHC Metals* Chloride Ultimate/BTU ASH | SW 3050 | 624 SW 6010/7000 series ASTM D-808-D512D ASTM D-240/3178/3179/462/129 |
| WDF | FOHC Metals* Chloride Ultimate/BTU Viscosity, Ash | SW 3050 | 624 SW 6010/7000 series ASTM D-808-D512D ASTM D-240/3178/3179/462/129 |
| Metals Spike | Metals* | SW 3050 | SW 6010/7000 series |
| Coal (Precalciner) | Metals* Chloride Ultimate/BTU | SW 3050 | SW 6010/7000 series ASTM D-4606 ASTM D-2015/3178/3179/3174/4239 |
| Coal (Kiln) | Metals* Chloride Ultimate/BTU | SW 3050 | SW 6010/7000 series ASTM D-4606 ASTM D-2015/3178/3179/3174/4239 |
| Tires | Metals* Chloride Ultimate/BTU | SW 3050 | SW 6010/7000 series ASTM D-4606 ASTM D-2015/3178/3179/3174/4239 |
| OUTPUT Clinker | Metals* Chloride | SW 3050 | SW 6010/7000 series ASTM C-114-19 |
| Kiln Dust | Metals* Chloride | SW 3050 | SW 6010/7000 series ASTM C-114-19 |
| Bypass Dust | Metals* Chloride | SW 3050 | SW 6010/7000 series ASTM C-114-19 |

SW 846/3050 - Acid Digestion of Sediments, Sludges and Soils
SW 946/6010 - Inductively Coupled Plasma Atomic Emissions
SW 846/7000 series - Atomic Absorption Methods
As, Sb, Ba, Be, Cr, Cd, Ag, Pb, Ti, Zn and Hg
ASTM C-114-19 Total Chloride
Potentiometric Titration with Silver Nitrate

5.0 SCOPE OF THE SAMPLING PROGRAM BY SITE

The COC Sampling Matrix is shown in Table 5-1. Two phases of tests were performed to determine the acceptability of firing WDF. First, a background emissions determination test was performed while firing coal only in April 1992. A second phase was performed during the firing of 100% WDF and 1.5 tph of tires. Coal was fired in the pre-calciner during each phase. Sampling was performed at the exhaust stack to determine concentrations and emission rates of particulate matter (PM), chlorides (HCl), chlorine (Cl₂), Volatile POHC, Cr⁺⁶, and heavy metals (HM). Additional measurements of carbon dioxide (CO₂), oxygen (O₂), carbon monoxide (CO) and total hydrocarbons (THC) were performed. Raw material and product samples were drawn for metals, total chloride and chlorine analyses during the COC.

5.1 STACK EMISSION SAMPLES

Emissions of PM, HCl, Cl₂, HM, POHC, Cr⁺⁶, CO, THC, O₂ and CO₂ were determined at sampling ports, on two levels of the exhaust stack. The sampling ports are located 90° apart and 27 to 37 feet above the inlet breeching in the 11 foot ID stack. All isokinetic sampling was performed at the upper level. In accordance with EPA Method 1, 24 traverse points were sampled at each location to measure stack gas velocity, temperature and moisture content in order to determine volumetric flowrate. A schematic of these locations and traverse point locations is presented in Figure 5-1.

At the exhaust stack, emissions of particulate, chlorides, chlorine and Volatile POHC were determined concurrently. On separate test days, emissions of heavy metals and Cr⁺⁶ were determined (no Cr⁺⁶ measurements were performed during the coal only background test in Phase I). Continuous emission monitoring was performed concurrent with all tests on the stack, utilizing one of the lower level ports. Additional CEM was performed at the kiln bypass duct utilizing the Lone Star CEMS to set operating limits.

5.1.1 Particulate, Chloride, and Chlorine Emission Measurements

Particulate, Chloride (HCl) and Chlorine sampling was performed on the upper platform at 24 traverse points in the exhaust stack. Each point was sampled for 5 minutes for a total test time of 120 minutes. A total of 3 tests for PM, HCl and Cl₂ were performed during each phase of testing, for a total of 6 tests. Sampling and analytical methods are presented in Section 4.0.

5.1.2 CO, O₂ and CO₂ Integrated Measurements

Integrated gas samples were drawn through a probe integral with the sampling probe at 24 traverse points simultaneously with each test described in Section 4.0. Sampling and analyses were in accordance with EPA Methods 3 and 3A as described in Section 4.0 to determine concentrations of CO, O₂, CO₂ as a measure of CEMS QA/QC. Integrated samples were introduced into the APCC CEMS at the end of each test day.

Lead oxide
Mercuric chloride
Chromium III oxide

The use of pumpable hazardous stream with maximum metal concentration and metal spiking began 12 hours before the stack test for metal removal efficiency. This was to ensure that the kiln system achieved equilibrium conditions with respect to metals. Samples of inputs and outputs were taken every 30 minutes during this period to establish when equilibrium was reached. Metal removal efficiency was determined while burning coal (precalciner), hazardous waste and tires.

Since the Lone Star Cape Girardeau plant also proposed to burn solid hazardous waste by injecting the pails into the burning zone of the kiln, pails were also injected into the kiln burning zone via an air cannon during the entire test. The injection was done during the same time interval as the metal spiking occurred. No spiked metal was introduced into these solid streams. The metals introduced by the solid stream were accounted for in the total metal input to the kiln system. The pails were injected into the kiln approximately 70-90 feet from the material discharge end of the kiln. The gas temperature at this point in the kiln is in excess of 3000° F. The material temperature is above 2300° F.

To ensure maximum volatilization of metals during this compliance testing maximum combustion zone temperature and maximum flue gas temperature entering the PM control device were achieved. The burning zone control for maximum temperature was the 4th stage gas inlet temperature which represents the position nearest the burning zone where temperature can be reliably measured. Temperature entering the main and bypass fabric filter APCD was monitored on a continual basis and maximized during this testing.

3.7 POHC SPIKING

The COC test meets the requirements of the State of Missouri Department of Air Management. This department required Lone Star to conduct performance testing within 60 days of achieving maximum hazardous fuel kiln rate and in no case later than 180 days after the initial burn date of April 28, 1992. The testing was to demonstrate the following destruction and removal efficiencies:

| | |
|-----------|--------|
| Lead | 98% |
| Mercury | 33% |
| Beryllium | 99% |
| VOC - | 99.99% |

To determine compliance with the organic emission limits, testing was performed with the kiln operating at minimum burning zone temperature conditions. To ensure this condition, the temperature was monitored at the 4th stage preheater inlet. This is the position nearest the burning zone where temperature can reliability be measured. This is the most conservative approach to prove thermal destruction of POHC.

Lead oxide
Mercuric chloride
Chromium III oxide

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Lead oxide
Mercuric chloride
Chromium III oxide

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| Mercury | 33% |
| Beryllium | 99% |
| VOC | 99.99% |

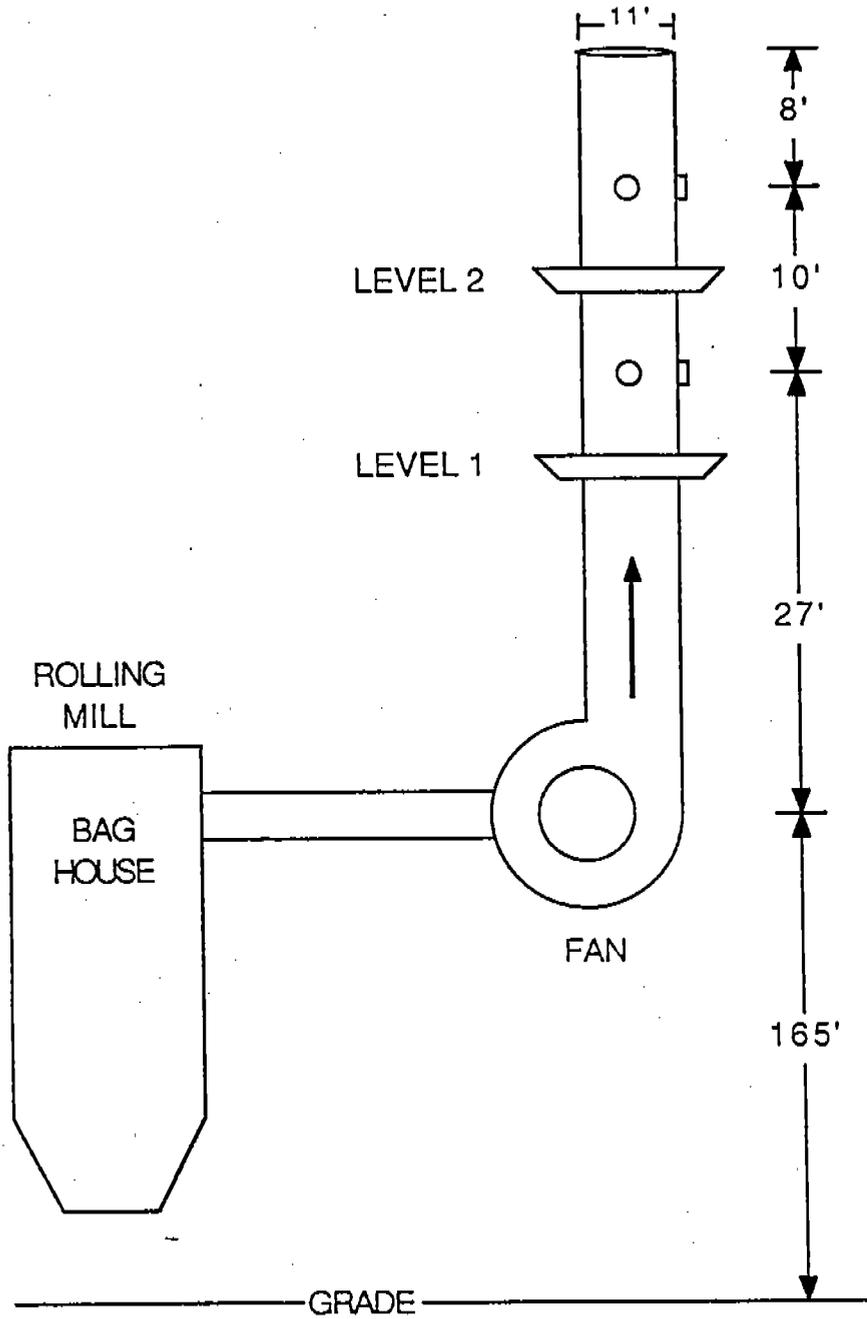
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TABLE 5-1
 SAMPLING MATRIX
 COMPLIANCE TEST PROGRAM
 LONE STAR INDUSTRIES
 CAPE GIRARDEAU, MISSOURI

| SAMPLE LOCATION | SAMPLE MATRIX | TOTAL | | PM | Metals | POHC | Gas Flow | CO OXYGEN THC | VISCOSITY Btu/ASH SOLIDS | ULTIMATE Btu |
|--------------------|---------------|----------|----------|----|--------|------|----------|------------------|--------------------------------|-----------------|
| | | CHLORIDE | CHLORINE | | | | | | | |
| Stack | Exhaust Gas | 6 | 6 | 6 | 6 (a) | 6 | 12 | 12 | | |
| Bypass Baghouse | Dust | 12 | | | 6 (b) | | | | | |
| Kiln Dust | Dust | 12 | | | 6 (b) | | | | | |
| Cooler Conveyor | Clinker | 12 | | | 6 (b) | | | | | |
| Conditioning Tower | Water | 12 | | | 6 (b) | | | | | |
| Raw Feed | Crush Rock | 12 | | | 6 (b) | | | | | 12 |
| Coal Mill-Precal. | Coal | 12 | | | 6 (b) | | | | | |
| WDLF Feed Line | WDLF | 12 | | | 6 (b) | 6 | | | 6 | |
| WDSF Pails | WDSF | 12 | | | 6 (b) | 6 | | | | 6 |
| Metals Spike (c) | Spike | 12 | | | 6 (c) | | | | | |
| Tire Feed | Tires | 6 | | | 3 (b) | | | | | 3 |

(a) Pb, As, Cr, Be, Cd, Hg, Zn, Cr+6
 (b) Sb, Pb, As, Ba, Be, Cr, Cd, Hg, Ag, Ti, Zn, Cr+6
 (c) Pb, As, Cr, Be, Cd, Hg, Cr+6

FIGURE 5 - 1
STACK TEST
SAMPLE LOCATIONS AND TRAVERSE POINTS
LONE STAR INDUSTRIES
CAPE GIRARDEAU, MISSOURI



| LEVEL 1 & 2 TRAVERSE POINT PER PORT | |
|-------------------------------------|--------|
| 1 | 2.7" |
| 2 | 8.8" |
| 3 | 15.6" |
| 4 | 23.4" |
| 5 | 33.0" |
| 6 | 45.0" |
| 7 | 85.0" |
| 8 | 99.0" |
| 9 | 108.6" |
| 10 | 116.4" |
| 11 | 123.2" |
| 12 | 129.2" |

APCC AIR POLLUTION CHARACTERIZATION and CONTROL, LTD.

5.1.3 Heavy Metal Emission Measurements

Heavy metals sampling was performed on the upper level at 24 traverse points in the exhaust stack. Each point was sampled for 5 minutes for a total time of 120 minutes. A total of 3 tests were performed during each phase of testing, for a total of 6 tests. Sampling and analytical methods are presented in Section 4.0.

5.1.4 Volatile POHC Emission Measurements

POHC emission measurements utilizing the EPA Slow VOST procedure were performed on the lower level platform of the exhaust stack. Single point samples, 40 minutes in duration, were taken at a point approximately centered in the stack. Four VOST runs, each utilizing one pair of cartridges, were performed during each test. A total of four tests were performed during each phase of testing, for a total of 8 tests. One set of field and trip blank cartridges were taken during each phase. A velocity traverse was performed concurrently with each test performed in accordance with EPA Methods 1 and 2 to determine the exhaust volumetric flowrate.

5.1.5 Cr⁺⁶ Emission Measurement

Cr⁺⁶ sampling was performed on the upper level platform at 24 traverse points on the exhaust stack. Each point was sampled for 5 minutes for a total time of 120 minutes. A total of 3 tests were performed during the second phase of testing. Sampling and analytical methods are presented in Section 4.0.

5.1.6 Continuous Emission Monitoring

Continuous emission monitoring for CO, THC, O₂ and CO₂ was performed at the lower level of the exhaust stack during each emission test. Monitoring was performed concurrent with each manual emission test performed. Calibrations were performed at the beginning and end of each test. System leak checks and system bias checks were performed at the beginning and end of each test day.

5.2 RAW MATERIAL AND PRODUCT SAMPLES

Samples of raw material and product were drawn at 15 minute intervals during each test run and composited for the test period. A glass sample jar was filled with sample from each of the following locations:

INPUTS

- Coal feed belts
- Water for the Conditioning Tower
- Raw material feed belt
- WDLF feed pipe
- WDSF buckets
- Shredded tires
- Spent kiln brick (if available)

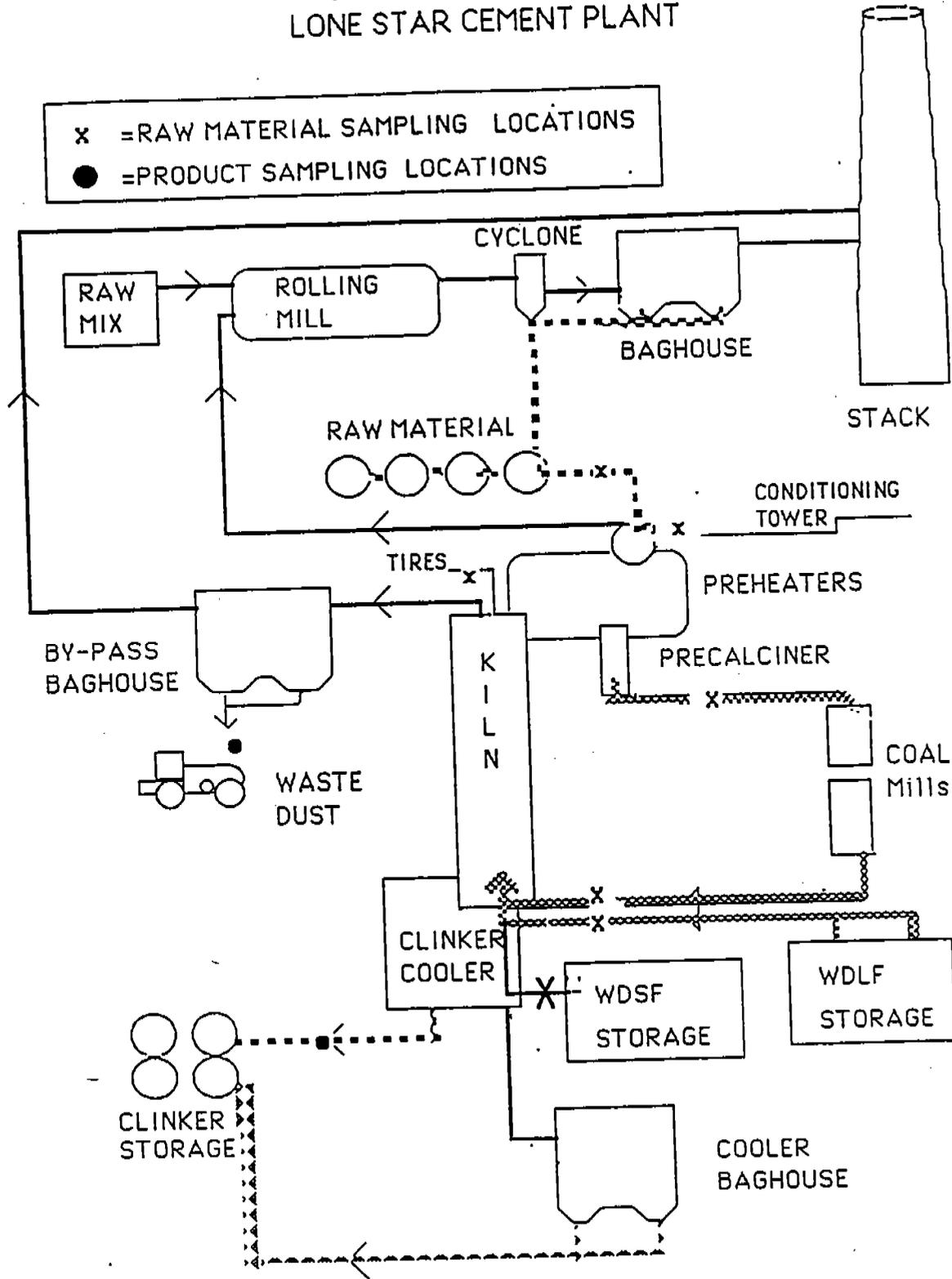
OUTPUTS

- Kiln Dust
- Clinker Cooler Conveyer
- By-pass Baghouse Hopper

Further details of this sampling are presented in Section 4.3. Sampling locations are presented in Figure 5-2. A total of 3 tests were performed for metals and a total of 3 tests were performed for chlorine and chloride mass balance during each phase, for a total of 12 chloride samples and 6 metals samples for each parameter. Analyses of composite samples of kiln raw materials and products drawn by Lone Star personnel were performed for the following constituents for the corresponding parameters.

| Constituents | Parameters |
|------------------------------|--|
| Kiln Coal (Only if fired) | Chlorides/Chlorine Btu & Ultimate Metals |
| Pre-calciner Coal | Chlorides/Chlorine Btu & Ultimate Metals |
| Kiln Feed | Chlorides/Chlorine Metals |
| Kiln Dust | Chlorides/Chlorine Metals |
| Clinker | Chlorides/Chlorine Metals |
| Tires | Chlorides/Chlorine Btu Metals |
| WDLF | Chlorides/Chlorine Btu Metals |
| WDSF | Chlorides/Chlorine Btu Metals |

FIGURE 5-2
 SAMPLING LOCATIONS
 LONE STAR CEMENT PLANT



5.3 TEST SCHEDULE

This COC was performed during the weeks of 13 April (Phase I) and 22 June (Phase II) 1992. Spiked (POHC, metals) WDLF at 5% chloride was fired for the particulate, chloride, chlorine and metals tests during Phase 2.

CERTIFICATION OF COMPLIANCE TEST SCHEDULE

Phase I

Kiln & Precalciner Firing Coal

April 13
Monday

Performed 3 background tests for PM, POHC, HCl, and Cl₂. CEM for CO₂, O₂, CO and THC.

April 14
Tuesday

Performed 3 background tests for HM. CEM for CO₂, O₂, CO and THC.

Phase II

Kiln Firing WDLF/WDSF/Tires Pre-calciner Fire Coal

June 22
Monday

Mobilize on-site and performed preliminary tests.

June 25
Thursday

Performed 3 tests for PM, POHC, HCl and Cl₂. Mass balance for chlorides. CEM for CO₂, O₂, CO and THC.

June 26
Friday

Performed three tests for HM and Cr⁺⁶. Mass balance for metals. CEM for CO₂, O₂, CO and THC.

6.0 QUALITY ASSURANCE PROGRAM

Quality Assurance (QA) and Quality Control (QC) guidelines required by Environmental Protection Agency to ensure the sampling program activities and analyses are performed in a manner as to achieve quality / accurate data. The QA/QC guideline summary presented in this section are detailed in the "Quality Assurance Handbook for Air Pollution Measurement Systems", Volume III (EPA-600/4-7-027b) and Test Methods for Evaluating Solid Waste, Volume 1A: Laboratory Manual Physical/Chemical Methods. Also detailed QA/QC procedures are found in each test method utilized in the test program.

6.1 PROJECT ORGANIZATION AND RESPONSIBILITY

The following individuals were responsible for implementation of the Quality Assurance Program as applied to the project. A schematic of the project organization chart can be seen in Figure 6-1.

- Program Manager
- Quality Assurance Manger
- Field Operation Manger
- Sampling and Analytical Manager
- Data Manager
- Laboratory Managers

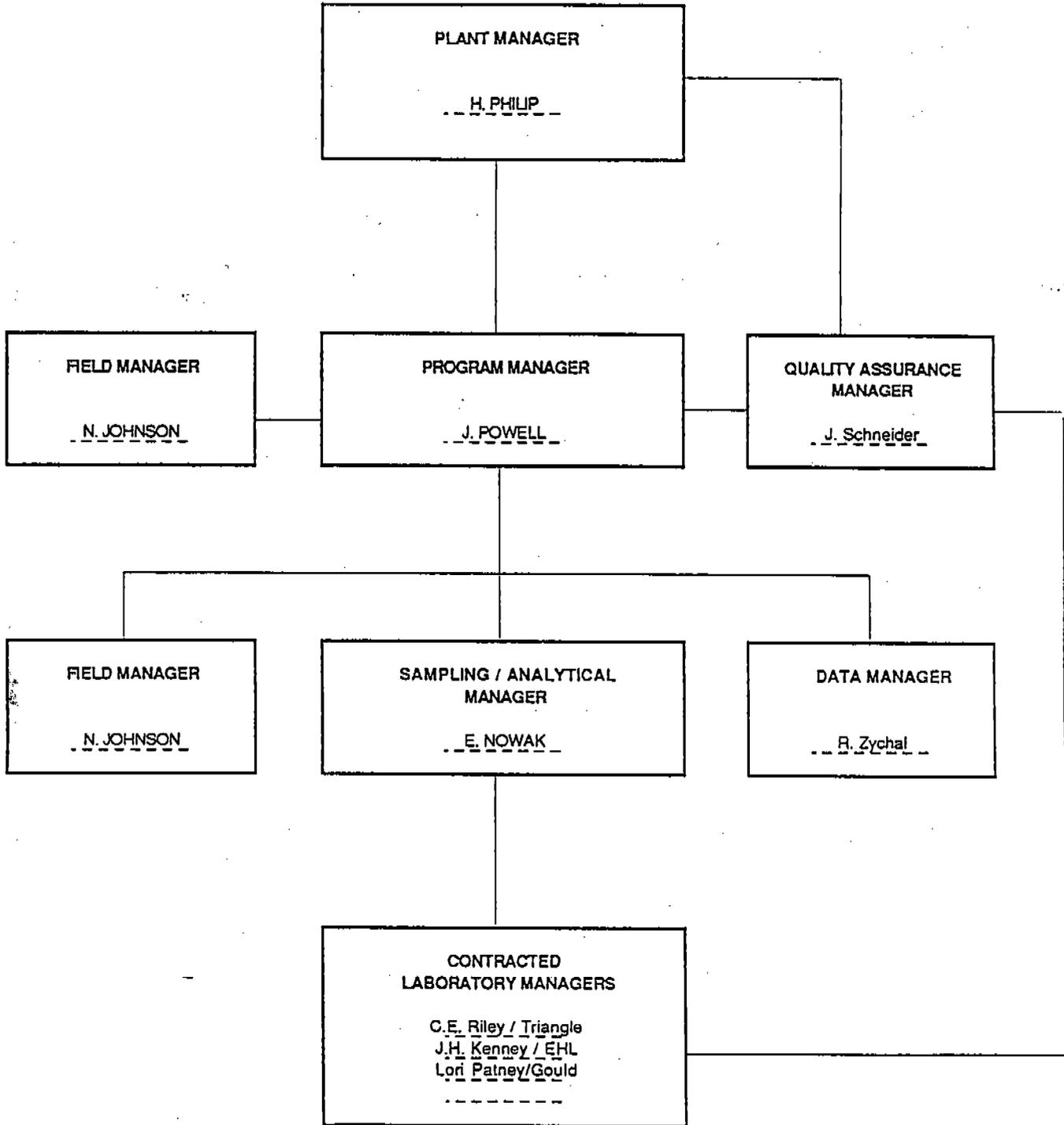
The above managers are a project team consisting of key personnel to coordinate all functions of the sampling program to ensure open communications with all parties involve. The responsibilities and functions of each manager is presented below.

Program Manager for the project is the overall supervisor for the project and to ensure all work is performed in accordance to approved protocols and test plans. All other parties report to the Program Manager with the status of their assigned areas. The Program Manager regularly meets with the Plant Manager for review and updates of the test program.

Quality Assurance Manager reviews and advises on all areas of concern related to QA/QC procedures. The QA Manager makes QC evaluations of field sampling methods, analytical analyses and data validation. Auditing of samples and QC procedures outlined are also performed.

Field Operations Manager is a facility person to instruct other facility personnel before and during field operations of the test program. The Field Operations

FIGURE 6-1
PROJECT ORGANIZATION
CHART



Manager ensures the facility is operating at the proposed test conditions, coordinates the test program and records process data.

Sampling and Analytical Manager processes and coordinates all field samples and data recovery. The Sampling and Analytical Manager ensures sampling methods and analytical procedures are implemented and that supplies needed are available.

Data Manager reviews all data (sampling and process) from the test program. He evaluates data for accuracy, precision, sensitivity and completeness. The Data Manager develops a system to perform calculations, setup and present results and storage of files.

Laboratory Managers are individual managers of the contracted laboratories to perform sample analyses. The Laboratory Managers implement QA/QC procedures in accordance with their laboratory and analytical sampling methods performed.

6.2 SAMPLING QUALITY ASSURANCE

Implementation of quality assurance procedures for source measurement programs is designed so that the work is done:

1. By competent, trained individuals experienced in the specific methodologies being used.
2. Using properly calibrated equipment.
3. Using approved procedures for sample handling and documentation.

Measurement devices, pitot tubes, dry gas meters, thermocouples and portable gas analyzers are uniquely identified and calibrated with documented procedures and acceptance criteria before and after each field effort. Records of all calibration data are maintained in the files.

Data are recorded on standard forms. Bound field notebooks are used to record observations and miscellaneous elements affecting data, calculations, or evaluation.

Prior to the test program APCC provided the following:

1. Filter numbers and tare weights of all filters available for the test.
2. The results of reagent blank runs on the reagents to be used during the test.
3. Calibrations of all pitot tubes, dry gas meters, orifice meters, sampling nozzles, and thermocouples which used during the test. All calibrations are performed within four months prior to the test date.

Specific details of APCC's QA program for stationary air pollution sources may be found in "Quality Assurance Handbook for Air Pollution Measurement Systems", Volume III (EPA-600/4-7-027b). Sampling methods are presented in Section 4 of the protocol.

6.2.1 EPA & SW Manual Methods

All particulate and metal sampling was $100\% \pm 10\%$ isokinetic. Probe and filter temperatures were within the specified temperatures.

Prior to sampling, a clean-up evaluation of each sampling train was performed to ensure the accuracy of the sampling equipment and to determine the level of background contamination (if any). A clean-up evaluation was performed on each sampling train to be used in the test program. These tests were performed prior to testing on each fuel type and upon the conclusion of testing in the sample recovery area. The sampling train was precharged as if ready to test and then recovered and analyzed as specified for the actual test program. Results can be found in Section 6.8 of this report. In summary, these evaluation tests were designed to precondition the sample train, establish background values, evaluate sample recovery efficiencies and educate sample recovery personnel in the specific procedures.

In addition to the above, blank samples of each collection media (reagents and filters) were collected at the test site for background analyses. All clean-up evaluation and blank samples were analyzed in conjunction with actual test samples. Sampling results were corrected for these backgrounds as required.

Appropriate sample recovery data was recorded on the sample identification and handling logs, chain of custody forms and analytical data forms. Methods preparation and recovery sheets used are presented in the Appendix.

Recovered samples were stored in shock-proof containers for storage and shipment for analyses.

6.2.2 CEM System

The CEM system was calibrated at the beginning and end of each test and leak and bias checked twice daily. All calibration gases were either NBS certified or EPA Protocol 1. Multi-point calibrations were performed on each analyzer to establish linearity prior to sampling and then throughout the test program.

6.2.3 VOST- Method

Field Blanks - Blank Tenax and Tenax/Charcoal cartridges were taken to the sampling site and the end caps removed for the period of time required to exchange two pairs of traps on the sampling train (approximately 5 minutes). After the two traps had been exchanged, the end caps were replaced on the blank tubes which were returned to storage on ice. This procedure was repeated a second time approximately 40 minutes later on the same traps. The pair was then returned to storage on ice until analysis. One pair of field blanks was included with each set of 8

VOST cartridge pairs collected. For Phase I, the field blank did not have any contaminants present above the method detection limit. The field blank for Phase II had only three compounds detected above the detection limit of 0.1 µg. The compounds detected and their respective concentrations were as follows: 0.7 µg of n-Hexane, 0.6 µg of Methylene Chloride, and 1.7 µg of Toluene.

Trip Blanks - One pair of blank cartridges (Tenax and Tenax/Charcoal) was included with shipment of cartridges to the site. These blanks are treated as any other cartridge except that the end caps are not removed. These cartridges were then analyzed to monitor potential contamination which occurred prior to shipment. For Phase I, the trip blank did not have any contaminants present above the method detection limit. The trip blank for Phase II had only two compounds detected above the detection limit of 0.1 µg. The compounds detected and their respective concentrations were as follows: 0.6 µg of Methylene Chloride, and 0.6 µg of Toluene.

The final blank for the VOST analysis were the condensate blanks. These blanks were performed by filling a 40 ml Volatile Organic Analysis (VOA) vile with zero head space using the same DI water as was utilized for the testing program. These blanks were performed on site and in the same manner as the actual samples. The results of the condensate blank for Phase I were as follows: 0.5 µg Methylene Chloride, 0.2 µg Toluene, and 2.0 µg Acetone. The results of the condensate blank for Phase II were as follows: 0.1µg 1,1,1-Trichloroethane, 3.1 µg Methylene Chloride, 0.1 µg Toluene, and 7.1 µg Acetone. Methylene Chloride, Toluene and Acetone are all solvents used in the recovery of the sampling trains and are the most likely source of the contamination. These levels of contamination are not considered to be abnormal.

Audit - Audit gas was not provided by MO DNR.

6.3 ANALYTICAL QUALITY CONTROL

APCC maintains a vigorous quality control program for all samples analyzed. This program is based on the general guidelines given in "Handbook for Analytical Quality Control in Water and Wastewater Laboratories" (EPA-600/4-79-019; March 1979). This program suggests guidelines in the areas of:

- Laboratory services
- Instrument selection
- Glassware
- Reagents
- Solvents
- Gases
- Analytical performance
- Data handling and reporting
- Water and wastewater sampling
- Laboratory safety

APCC has made additions to the EPA program which include the following:

1. Duplicate analysis performed on 10 percent of samples.
2. Ten percent of the samples are spiked by the laboratory manager with known amounts of the parameter of interest and re-analyzed to determine the percent recovery. A Shewhart control chart is used for the percent recovery control (EPA, Handbook of Analytical Quality Control in Water and Wastewater Laboratories, 1979).
3. Standards and curves are determined for each analysis using the appropriate standard. Least squares linear regressions calculations are used in determining the "best fit" to the data. Correlation coefficients are also calculated.

6.4 SAMPLE CHAIN OF CUSTODY PROCEDURES

The sample and analytical custody procedures were implemented and maintained in accordance with SW 846, Section 2 and APCC procedures. The Sampling Manager was responsible for maintaining and filing of the Chain of Custody.

Field samples were labeled with the field label. Sampling train operators filled out the field labels in detail with the appropriate information corresponding to the sampling method detailed in Section 4 of this protocol. Process sample labels were filled out as per the instructions of the Sampling and Analytical Manager. The train operators and samplers are responsible for collecting the sample, logging each container and securing the sample until transferred to the Sampling and Analytical Manager.

A data assessment of sampling results was performed by the Quality Assurance Manager and the Program Manager. The data assessment was performed during scheduled time periods to ensure quality data was collected and processed. Corrective action was implemented if warranted to ensure QA/QC procedures were met.

The Sampling and Analytical Manager filled out the sample Chain of Custody forms and logged each sample from the receiver. Chain of Custody forms are presented in the Appendix. The Chain of Custodies were used to verify sample ID's, sample conditions and volumes. The Sampling and Analytical Manager logged in blanks and audit samples on to the chain of custody. The samples were secured for storage until they were shipped to the laboratory.

6.5 LABORATORY QA/QC PROCEDURES

The Sampling and Analytical Manager worked with the individual Laboratory Managers to implement procedures that were performed on samples submitted based on the Chain of Custody, analytical methods, specific sampling method requirements and laboratory QA/QC procedures.

Information submitted to the Sampling and Analytical Manager from the Laboratory Manager was scrutinized for the following laboratory measurements: limits of detection, accuracy and precision prior to the field effort.

6.6 DATA REDUCTION AND REPORTING

The Data Manager develops a data reduction system to conform to the collection of field data to be reduced and quantitative result for the final report. The methods for data reduction was specified and presented to the Program Manager before the field effort.

Raw data was recorded on field data sheets, bound laboratory books and data logger strip charts which are presented in the Appendix. Parts of the data capture are checked manually or with QC check programs.

6.7 DATA VALIDATION

Validation of data was reviewed by the Quality Assurance Manager against the QA/QC criteria of the specific methods. The data was assessed to the quality / accuracy as required to meet the objectives of the sampling program. Audit samples were checked for accuracy and precision. Sample calculations were performed with raw data separate from the reported calculations and results. All documentation was be checked for correctness, completeness and verified as checked.

6.8 QUALITY ASSURANCE / QUALITY CONTROL RESULTS

Listed below is a summary of the quality assurance/quality control (QA/QC) laboratory data for this testing program. This synopsis includes an interpretation of reagent blanks and blank train results. Also included is where in the Appendix this data can be found along with the location of all audit sample data.

All the laboratories used for this testing program were accredited and have extensive experience in the analysis performed. The testing laboratories followed appropriate QA/QC procedures including blank runs, duplicates and three (or more) point calibrations. Additional QA/QC data can be found in the Addendum Appendix.

A summary of the chlorine, HCL, and particulate QA/QC data is presented in Table 6-1. This table illustrates the results of the blank trains from both phases, along with audit sample results. A summary of the metals QA/QC data is presented in Table 6-2, including blank train results for both phases, audit sample data, and reagent blank data. Table 6-3 presents the hexavalent chrome QA/QC data, consisting of reagent blank and blank train data. The sections below provide the location of the supportive data located in the Appendix.

6.8.1 Phase I: Coal Only

| <u>Test /AUDIT#</u> | <u>Parameter</u> | <u>Appendix Page</u> |
|---------------------|----------------------------------|------------------------------------|
| 1 | Particulate/Cl ₂ /HCl | C-1 Train Data C-9 Reagent Data |
| 5 | Metals | C-42 |
| J1689 | EPA chlorine Audit Filter | C-4 |
| L-77, H-99 | Metal Audit Samples | C-41 |

6.8.2 Phase II: Coal, WDF & Tires

| <u>Test /AUDIT #</u> | <u>Parameter</u> | <u>Appendix Page</u> |
|----------------------|----------------------------------|------------------------------------|
| 1 | Particulate/Cl ₂ /HCl | C-3 Train Data C-4 Reagent Data |
| 6 | Metals | C-44 |
| 6 | Hexavalent Chrome | C-45 |
| J1072, J1320 | EPA chlorine Audit Filters | C-9 |
| L-78, H-16 | Metal Audit Samples | C-44 |

TABLE 6-1
CHLORINE, HCL, AND PARTICULATE Q.C. DATA
CERTIFICATION OF COMPLIANCE TEST
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| SAMPLE NUMBER | TOTAL PARTICULATE CATCH (mg) | CHLORINE CATCH (mg) | HYDROCHLORIC ACID CATCH (mg) |
|----------------------|-------------------------------------|----------------------------|-------------------------------------|
| BLANK PHASE I | 9.7 | 1.0 | <0.70 |
| BLANK PHASE II | 2.9 | <0.60 | <0.017 |
| J1689 | * | 40 (mg/L) | * |
| J1072 | * | 49 (mg/L) | * |
| J1320 | * | 707 (mg/L) | * |

* Not applicable, audit sample were for chlorine only. All data is within desired limits.

**TABLE 6-2
METALS Q.C. DATA
CERTIFICATION OF COMPLIANCE TEST
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

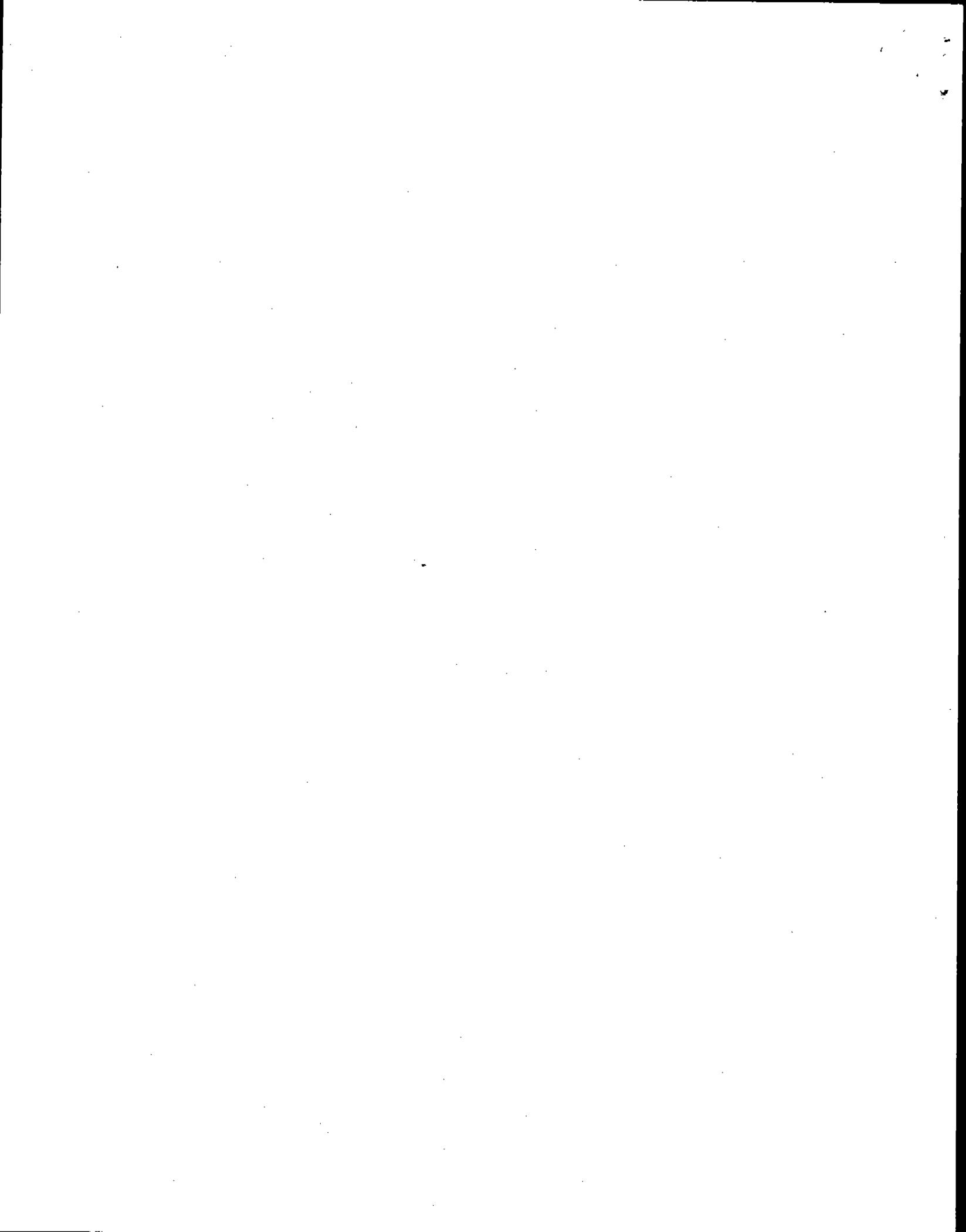
| <u>Element</u> | <u>Blank Train Phase I Total (ug)</u> | <u>Blank Train Phase II Total (ug)</u> | <u>Audit Sample L77 Total (ug)</u> | <u>Audit Sample H99 Total (ug)</u> | <u>Audit Sample L78 Total (ug)</u> | <u>Audit Sample H16 Total (ug)</u> | <u>Reagent Blanks Total (ug)</u> |
|----------------|---|--|--|--|--|--|--|
| Antimony (Sb) | 0.670 | • | 4.02 | 8.22 | 3.63 | 5.10 | • |
| Arsenic (As) | 0.990 | <0.473 | 9.00 | 16.60 | 7.57 | 20.30 | 1.00 |
| Barium (Ba) | 14.000 | • | • | • | 13.70 | 134.00 | • |
| Beryllium (Be) | <0.050 | <0.237 | 3.32 | 104.00 | 5.41 | 60.40 | <0.20 |
| Cadmium (Cd) | <0.100 | 3.390 | 8.19 | 69.30 | 14.10 | 67.50 | <0.20 |
| Chromium (Cr) | 9.150 | 37.700 | 8.87 | 85.50 | 16.10 | 73.80 | 9.98 |
| Copper (Cu) | • | • | 22.80 | 77.60 | • | • | • |
| Manganese (Mn) | • | • | 10.10 | 77.10 | • | • | • |
| Nickel (Ni) | • | • | 20.40 | 341.00 | • | • | • |
| Phosphorus (P) | • | • | 79.40 | 42.00 | • | • | • |
| Lead (Pb) | 3.970 | 14.083 | 41.70 | 328.00 | 38.40 | 192.00 | <.760 |
| Silver (Ag) | <0.100 | • | <0.7 | 4.08 | 18.30 | 29.50 | • |
| Thallium (Tl) | <0.200 | • | 4.69 | 579.00 | 3.25 | 809.00 | • |
| Zinc (Zn) | 21.320 | 83.770 | 85.20 | 213.00 | 399.00 | 532.00 | 7.16 |
| Mercury (Hg) | <1.12 | <4.736 | 0.01 | 0.006 | <0.40 | <0.40 | <0.800 |

*Not Applicable

TABLE 6-3
HEXAVALENT CHROME Q.C. DATA
CERTIFICATION OF COMPLIANCE
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| <u>TEST NUMBER</u> | <u>HEXAVALENT CHROME (ug)</u> | <u>DESCRIPTION</u> |
|--------------------|-------------------------------|---------------------------|
| 6-1 CR | <0.683 | Blank train solution |
| 6-3 CR | <0.444 | Potassium hydroxide blank |
| 6-4 CR | <0.432 | DI Water blank |
| 6-5 CR | 0.5 | Nitric Acid blank |

All the results were at or just above the detection limit, indicating no problems due to contamination.



LONESTAR APPENDIX LIST

PAGE

| | | |
|------|---|------|
| A-1 | Particulate/Chlorine/HCl Data Summary/Phase 1 | A-2 |
| A-2 | Summary of Chloride Mass Balance Data/Phase 1 | A-3 |
| A-3 | Metals Data Summary/Phase 1 | A-4 |
| A-4 | Summary of Mass Balance Metals Data/Phase 1 | A-5 |
| A-5 | VOST Train Worksheet/Phase 1 | A-6 |
| A-6 | APCC CEM Data Summary/Phase 1 | A-7 |
| A-7 | Particulate/Chlorine/HCl Data Summary/Phase 2 | A-13 |
| A-8 | Summary of Chloride Mass Balance Data/Phase 2 | A-14 |
| A-9 | Metals Data Summary/Phase 2 | A-15 |
| A-10 | Cr6 Data Summary/Phase 2 | A-16 |
| A-11 | Mass Balance Metals Data/Phase 2 | A-17 |
| A-12 | VOST Train Worksheet/Phase 2 | A-18 |
| A-13 | APCC CEM Data Summary/Phase 2 | A-19 |

TABLE A-1
PARTICULATE/CHLORINE/HCl DATA SUMMARY
BIF COC TEST PROGRAM/PHASE 1
LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST NO. | 2 CL | 3 CL | 4 CL |
|--|--------------|---------------|---------------|
| DATE: | 4/13/92 | 4/13/92 | 4/13/92 |
| TIME : | 9:24 - 11:31 | 13:08 - 15:13 | 16:55 - 19:00 |
| TEST DATA INPUT | | | |
| Barometric Pressure (in. Hg) | 29.84 | 29.84 | 29.72 |
| Stack Area (ft ²) | 95.03 | 95.03 | 95.03 |
| Nozzle Diameter (in.) | 0.191 | 0.191 | 0.191 |
| Total Sampling Time (min.) | 120 | 120 | 120 |
| Calibration Factor (Y) | 0.97 | 0.97 | 0.97 |
| Pitot Coefficient | 0.84 | 0.84 | 0.84 |
| Average Square Root of Velocity Head (in. wc) | 1.09 | 1.11 | 1.09 |
| Average Orifice Pressure Drop (in. wc) | 1.192 | 1.225 | 1.2 |
| Average Meter Temp. (°F) | 62 | 86 | 94 |
| Average Stack Pressure (in. wc) | -0.47 | -0.51 | -0.45 |
| Average Stack Temp. (°F) | 240 | 238 | 239 |
| Meter Volume @ Meter Conditions (ft ³) | 68.44 | 69.28 | 70.64 |
| Total Water Collected (ml) | 208 | 240 | 224 |
| CO ₂ in Stack Gas (%) | 18 | 17.4 | 17.7 |
| O ₂ in Stack Gas (%) | 10.2 | 10.3 | 10.6 |
| CO in Stack Gas (%) | 0.1 | 0.05 | 0.07 |
| Total Particulate Catch (mg) | 74.2 | 81.5 | 64.6 |
| Total Chlorine Catch (mg) | 0.7 | 0.39 | 0.9 |
| Total HCl Catch (mg) | 6.083 | 3.583 | 1.483 |
| CALCULATED VALUES | | | |
| Meter Volume (dscf) | 67.17 | 65.01 | 65.06 |
| Water Vapor in Stack Gas (%) | 12.72 | 14.80 | 13.95 |
| Molecular Weight of Stack Gas (dry) | 31.288 | 31.196 | 31.256 |
| Molecular Weight of Stack Gas (wet) | 29.60 | 29.24 | 29.41 |
| Average Velocity of Stack Gas (fpm) | 4,184 | 4,280 | 4,202 |
| Actual Stack Gas Flowrate (acfm) | 397,564 | 406,747 | 399,357 |
| Stack Gas Flowrate (dscfm) | 260,724 | 261,101 | 257,569 |
| Isokinesis (%) | 102.59 | 99.15 | 100.59 |
| EMISSION CONCENTRATION | | | |
| Particulate Concentration (gr/acf) | 0.011 | 0.012 | 0.010 |
| Particulate Concentration (gr/dscf) | 0.017 | 0.019 | 0.015 |
| Particulate Concentration (lbs/dscf) | 2.43E-06 | 2.76E-06 | 2.19E-06 |
| Particulate Concentration (µg/m ³) | 25600 | 28438 | 22629 |
| EMISSION RATE | | | |
| Particulate Emission Rate (lbs/hr) | 38.06 | 43.26 | 33.80 |
| Particulate Emission (gr/dscf@7%) | 0.022 | 0.025 | 0.021 |
| Chlorine Emission Rate (g/hr) | 163.440 | 95.340 | 213.380 |
| HCl Emission Rate (g/hr) | 1416.480 | 862.600 | 354.120 |

A-

TABLE A-2
SUMMARY OF CHLORIDE MASS BALANCE DATA
BACKGROUND TEST/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| <u>SAMPLE IDENTIFICATION</u> | <u>% CHLORIDE WET BASIS</u> |
|------------------------------|-----------------------------|
| 2-1 MB (Raw Feed) | 0.035 |
| 2-2 MB (Coal-Kiln) | 0.11 |
| 2-3 MB (Coal-Precalciner) | 0.09 |
| 2-4 MB (Quench Water) | 0.0056 |
| 2-6 MB (Bypass Dust) | 0.99 |
| 2-7 MB (Clinker) | 0.0063 |
| 2-8 MB (Kiln Dust) | 0.47 |
| 3-1 MB (Raw Feed) | 0.035 |
| 3-2 MB (Coal-Kiln) | 0.11 |
| 3-3 MB (Coal-Precalciner) | 0.11 |
| 3-4 MB (Quench Water) | 0.0058 |
| 3-6 MB (Bypass Dust) | 3.00 |
| 3-7 MB (Clinker) | 0.0047 |
| 3-8 MB (Kiln Dust) | 0.27 |
| 4-1 MB (Raw Feed) | 0.034 |
| 4-2 MB (Coal-Kiln) | 0.10 |
| 4-3 MB (Coal-Precalciner) | 0.12 |
| 4-4 MB (Quench Water) | 0.0054 |
| 4-6 MB (Bypass Dust) | 1.60 |
| 4-7 MB (Clinker) | 0.0063 |
| 4-8 MB (Kiln Dust) | 0.26 |

**TABLE A-3
METALS DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 1
LONE STAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST NO. | 6 ME | 7 ME | 8 ME |
|--|---------------|---------------|---------------|
| DATE: | 4/14/92 | 4/14/92 | 4/14/92 |
| TIME: | 11:28 - 14:10 | 16:10 - 18:35 | 20:30 - 22:44 |
| TEST DATA INPUT | | | |
| Barometric Pressure (in. Hg) | 29.68 | 29.58 | 29.52 |
| Stack Area (ft ²) | 95.03 | 95.03 | 95.03 |
| Nozzle Diameter (in.) | 0.191 | 0.191 | 0.191 |
| Total Sampling Time (min.) | 120 | 120 | 120 |
| Calibration Factor (Y) | 0.97 | 0.97 | 0.97 |
| Pitot Coefficient | 0.84 | 0.84 | 0.84 |
| Average Square Root of Velocity Head (in. wc) | 1.102 | 1.122 | 1.119 |
| Average Orifice Pressure Drop (in. wc) | 1.22 | 1.262 | 1.25 |
| Average Meter Temp. (°F) | 77 | 84 | 77 |
| Average Stack Pressure (in. wc) | -0.6 | -0.58 | -0.66 |
| Average Stack Temp. (°F) | 238 | 237 | 235 |
| Meter Volume @ Meter Conditions (ft ³) | 70.78 | 72.92 | 71.93 |
| Total Water Collected (ml) | 234 | 234 | 218 |
| CO ₂ in Stack Gas (%) | 17.8 | 17.5 | 17.2 |
| O ₂ in Stack Gas (%) | 10.2 | 10.6 | 10.6 |
| CO in Stack Gas (%) | 0.1 | 0.1 | 0.1 |
| Total Catch Sb (mg) | 0.0005 | 0.0009 | 0.00066 |
| Total Catch As (mg) | 0.00331 | 0.00451 | 0.00384 |
| Total Catch Ba (mg) | 0.0588 | 0.0664 | 0.307 |
| Total Catch Be (mg) | 0.00032 | 0.00012 | 0.00019 |
| Total Catch Cd (mg) | 0.00068 | 0.00079 | 0.00059 |
| Total Catch Cr (mg) | 0.0309 | 0.0305 | 0.0704 |
| Total Catch Pb (mg) | 0.0245 | 0.0256 | 0.0218 |
| Total Catch Ag (mg) | 0.00019 | 0.0002 | 0.00023 |
| Total Catch Tl (mg) | 0.00224 | 0.00149 | 0.00145 |
| Total Catch Zn (mg) | 0.0826 | 0.0624 | 0.183 |
| Total Catch Hg (mg) | 0.00813 | 0.00559 | 0.00557 |
| CALCULATED VALUES | | | |
| Meter Volume (dscf) | 67.17 | 68.08 | 67.90 |
| Water Vapor in Stack Gas (%) | 14.09 | 13.92 | 13.13 |
| Molecular Weight of Stack Gas (dry) | 31.256 | 31.224 | 31.176 |
| Molecular Weight of Stack Gas (wet) | 29.39 | 29.38 | 29.45 |
| Average Velocity of Stack Gas (fpm) | 4,251 | 4,332 | 4,315 |
| Actual Stack Gas Flowrate (acfm) | 403,942 | 411,704 | 410,029 |
| Stack Gas Flowrate (dscfm) | 260,019 | 265,017 | 266,550 |
| Isokinesis (%) | 102.87 | 102.31 | 101.44 |
| EMISSION CONCENTRATION | | | |
| Concentration Sb (µg/Nm ³) | 0.27337 | 0.46677 | 0.34325 |
| Concentration As (µg/Nm ³) | 1.74012 | 2.33902 | 1.99706 |
| Concentration Ba (µg/Nm ³) | 30.91215 | 34.43694 | 159.66100 |
| Concentration Be (µg/Nm ³) | 0.16823 | 0.06224 | 0.09881 |
| Concentration Cd (µg/Nm ³) | 0.35749 | 0.40972 | 0.30684 |
| Concentration Cr (µg/Nm ³) | 16.24465 | 15.81817 | 36.61282 |
| Concentration Pb (µg/Nm ³) | 12.88006 | 13.27689 | 11.33749 |
| Concentration Ag (µg/Nm ³) | 0.09989 | 0.10373 | 0.11962 |
| Concentration Tl (µg/Nm ³) | 1.17761 | 0.77276 | 0.75410 |
| Concentration Zn (µg/Nm ³) | 43.42421 | 32.36243 | 95.17252 |
| Concentration Hg (µg/Nm ³) | 4.27408 | 2.89913 | 2.89678 |
| EMISSION RATE | | | |
| Emission Rate Sb (g/hr) | 0.12078 | 0.21019 | 0.15546 |
| Emission Rate As (g/hr) | 0.76883 | 1.05330 | 0.90451 |
| Emission Rate Ba (g/hr) | 13.65776 | 15.50756 | 72.31391 |
| Emission Rate Be (g/hr) | 0.07433 | 0.02803 | 0.04475 |
| Emission Rate Cd (g/hr) | 0.15795 | 0.18450 | 0.13897 |
| Emission Rate Cr (g/hr) | 7.17729 | 7.12320 | 16.58273 |
| Emission Rate Pb (g/hr) | 5.69073 | 5.97882 | 5.13499 |
| Emission Rate Ag (g/hr) | 0.04413 | 0.04671 | 0.05418 |
| Emission Rate Tl (g/hr) | 0.52030 | 0.34799 | 0.34155 |
| Emission Rate Zn (g/hr) | 19.18590 | 14.57337 | 43.10569 |
| Emission Rate Hg (g/hr) | 1.88839 | 1.30553 | 1.31201 |

TABLE A-4
 SUMMARY OF MASS BALANCE METALS DATA
 CERTIFICATION OF COMPLIANCE TEST/PHASE 1
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

| TEST NUMBER (MATRIX) | ELEMENT | | | | | | | | | | | | | |
|----------------------|---------------|--------------|-------------|----------------|--------------|---------------|-----------|-------------|---------------|-----------|--------------|-------|-------|-------|
| | Antimony (Sb) | Arsenic (As) | Barium (Ba) | Beryllium (Be) | Cadmium (Cd) | Chromium (Cr) | Lead (Pb) | Silver (Ag) | Thallium (Tl) | Zinc (Zn) | Mercury (Hg) | | | |
| | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG | MG/KG |
| 8 (RAW MIX) | 0.458 | 1.220 | 19.400 | 0.060 | 0.608 | 5.540 | 10.500 | <0.066 | 0.756 | 12.600 | 0.260 | | | |
| 6 (COAL KILN) | <0.277 | 2.070 | 23.300 | 0.603 | 1.830 | 9.650 | 9.030 | 0.105 | <0.111 | 37.800 | 0.167 | | | |
| 6 (COAL PRECAL) | <0.353 | 3.450 | 46.700 | 0.508 | 2.790 | 6.340 | 11.200 | <0.071 | <0.141 | 51.200 | 0.230 | | | |
| 6 (QUENCH H2O)* | <0.005 | <0.002 | 0.090 | <0.001 | <0.001 | <0.005 | 0.048 | <0.001 | <0.002 | <0.001 | <0.001 | | | |
| 6 (BYPASS DUST) | <0.368 | 1.600 | 40.300 | 0.388 | 2.120 | 19.400 | 87.900 | 0.465 | 0.372 | 21.200 | 0.100 | | | |
| 6 (CLINKER) | <0.442 | 1.950 | 51.300 | 0.468 | 1.400 | 45.700 | 12.300 | <0.088 | 0.177 | 23.700 | <0.080 | | | |
| 6 (KILN DUST) | <0.361 | 2.190 | 23.300 | 0.159 | 0.658 | 7.010 | 21.300 | 0.116 | 45.400 | 12.300 | 0.415 | | | |
| 7 (RAW MIX) | 0.410 | 1.340 | 19.500 | 0.104 | 0.632 | 5.900 | 30.300 | <0.075 | 1.200 | 13.100 | 0.228 | | | |
| 7 (COAL KILN) | <0.327 | 1.020 | 15.300 | 0.321 | 1.620 | 9.690 | 4.540 | 0.131 | <0.131 | 43.800 | 0.127 | | | |
| 7 (COAL PRECAL) | <0.396 | 4.290 | 46.200 | 0.460 | 2.610 | 7.520 | 13.700 | <0.079 | <0.158 | 51.500 | 0.121 | | | |
| 7 (QUENCH H2O)* | <0.005 | 0.003 | 0.087 | <0.001 | <0.001 | <0.005 | 0.022 | <0.001 | <0.002 | 0.001 | 0.005 | | | |
| 7 (BYPASS DUST) | <0.305 | 1.790 | 40.400 | 0.396 | 2.810 | 18.100 | 109.000 | 0.646 | 0.457 | 24.700 | <0.078 | | | |
| 7 (CLINKER) | <0.275 | 2.580 | 49.400 | 0.487 | 1.350 | 50.300 | 14.000 | <0.055 | <0.110 | 18.700 | <0.066 | | | |
| 7 (KILN DUST) | <0.335 | 1.690 | 23.400 | 0.168 | 0.819 | 7.760 | 24.300 | 0.107 | 46.500 | 18.800 | 0.335 | | | |
| 8 (RAW MIX) | <0.371 | 1.210 | 18.400 | 0.126 | 0.476 | 5.870 | 14.700 | 40.100 | 2.210 | 9.200 | 0.473 | | | |
| 8 (COAL KILN) | <0.335 | 2.740 | 22.800 | 0.817 | 1.870 | 9.190 | 8.250 | 0.080 | <0.134 | 52.800 | 0.119 | | | |
| 8 (COAL PRECAL) | <0.396 | 3.820 | 48.100 | 0.736 | 2.660 | 8.250 | 1.240 | <0.079 | <0.158 | 55.000 | 0.136 | | | |
| 8 (QUENCH H2O)* | <0.005 | 0.004 | 0.094 | <0.001 | <0.001 | <0.005 | <0.004 | <0.001 | <0.002 | 0.002 | 0.004 | | | |
| 8 (BYPASS DUST) | <0.364 | 1.660 | 37.700 | 0.460 | 2.720 | 18.200 | 105.000 | 0.837 | 0.582 | 28.400 | <0.079 | | | |
| 8 (CLINKER) | <0.298 | 1.790 | 46.800 | 0.524 | 1.400 | 48.100 | 15.700 | 0.077 | <0.119 | 23.600 | <0.083 | | | |
| 8 (KILN DUST) | <0.454 | 1.310 | 21.200 | 0.245 | 0.516 | 8.960 | 21.500 | 0.118 | 58.900 | 25.500 | 0.275 | | | |

* RESULTS REPORTED IN MG/L

A5

TABLE A-5
VOST TRAIN WORKSHEET/PHASE 1
BIF COC TEST PROGRAM
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Apr-92

| Test Number | 2A | 2B | 2C | 2D | Total/Avg. | Normal Liters | Concentration ug/l | Emission Rate g/hr |
|------------------------------|-----------|-----------|-----------|-----------|------------|------------------|-----------------------|-----------------------|
| Sample Volume (l) | 20.1 | 20.45 | 19.6 | 20.07 | 80.22 | 77.58 | | |
| Meter Temperature (°C) | 23 | | | | 23 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.84 | | | |
| Flowrate (dscfm) | | | | | 260724 | | | |
| Dry Gas Meter % | | | | | 0.98 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00129 | 0.571 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00129 | 0.571 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00129 | 0.571 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00129 | 0.571 |
| Test Number | 3A | 3B | 3C | 3D | | | | |
| Sample Volume (l) | 19.73 | 19.8 | 20 | 20.07 | 79.6 | 74.47 | | |
| Meter Temperature (°C) | 33 | | | | 33 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.84 | | | |
| Flowrate (dscfm) | | | | | 261101 | | | |
| Dry Gas Meter % | | | | | 0.98 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00134 | 0.596 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00134 | 0.596 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00134 | 0.596 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00134 | 0.596 |
| Test Number | 4A | 4B | 4C | 4D | | | | |
| Sample Volume (l) | 20 | 19.8 | 19.96 | 19.93 | 79.69 | 74.99 | | |
| Meter Temperature (°C) | 30 | | | | 30 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.72 | | | |
| Flowrate (dscfm) | | | | | 257569 | | | |
| Dry Gas Meter % | | | | | 0.98 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00133 | 0.583 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00133 | 0.583 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00133 | 0.583 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00133 | 0.583 |

TABLE A-6-1

**APCC CEM DATA SUMMARY
BACKGROUND TEST/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

Apr-92

| DATE | TIME | | CO (ppm) | OXYGEN (%) | CO ₂ (%) | CO @ 7% O ₂ (ppm) |
|--------------|-------|-------|-------------|---------------|------------------------|---------------------------------|
| | From | To | | | | |
| 4/13/92 | | | | | | |
| START TEST 2 | 9:28 | 9:43 | 900 | 10.0 | 18.2 | 1148 |
| | 9:43 | 9:59 | 875 | 10.2 | 17.8 | 1137 |
| | 9:59 | 10:15 | 787 | 10.2 | 18.0 | 1022 |
| | 10:15 | 10:31 | 980 | 10.1 | 18.0 | 1261 |
| | 10:31 | 10:47 | 950 | 9.9 | 18.3 | 1200 |
| | 10:47 | 11:03 | 950 | 10.1 | 18.1 | 1223 |
| | 11:03 | 11:19 | 850 | 10.0 | 18.3 | 1084 |
| | 11:19 | 11:35 | 800 | 11.5 | 16.2 | 1183 |
| | 11:35 | 11:51 | 500 | 10.3 | 17.7 | 656 |
| | 11:51 | 12:07 | 518 | 11.4 | 16.3 | 758 |
| | 12:07 | 12:23 | 1000 | 10.0 | 17.6 | 1275 |
| | 12:23 | 12:39 | 1000 | 10.1 | 15.5 | 1287 |
| STOP TEST 2 | 12:39 | 12:55 | 933 | 9.9 | 19.0 | 1179 |
| TEST AVERAGE | | | 849 | 10.3 | 41.5 | 1112 |

Note: CO averages of 1000 are actually over range.

TABLE A-6-2
APCC CEM DATA SUMMARY
BACKGROUND TEST/PHASE 1
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Apr-92

| DATE | TIME | TIME | CO | OXYGEN | CO2 | CO @ 7% O2 |
|--------------|-------|-------|-------|--------|------|------------|
| TEST NO. | From | To | (ppm) | (%) | (%) | (ppm) |
| 4/13/92 | | | | | | |
| START TEST 3 | 13:11 | 13:26 | 1000 | 10.5 | 17.1 | 1337 |
| | 13:26 | 13:41 | 950 | 10.0 | 17.9 | 1211 |
| | 13:41 | 13:56 | 673 | 10.4 | 17.3 | 891 |
| | 13:56 | 14:11 | 675 | 10.1 | 17.7 | 869 |
| | 14:11 | 14:26 | 669 | 10.2 | 17.5 | 869 |
| | 14:26 | 14:41 | 670 | 10.3 | 17.4 | 879 |
| | 14:41 | 14:56 | 528 | 10.3 | 17.4 | 692 |
| | 14:56 | 15:11 | 800 | 10.3 | 17.3 | 1049 |
| | 15:11 | 15:26 | 695 | 10.2 | 17.4 | 903 |
| | 15:26 | 15:41 | 800 | 10.1 | 17.6 | 1030 |
| | 15:41 | 15:56 | 751 | 10.1 | 17.4 | 967 |
| STOP TEST 3 | 15:56 | 16:11 | 900 | 10.1 | 17.5 | 1158 |
| TEST AVERAGE | | | 759 | 10.2 | 17.5 | 988 |

Note: CO averages of 1000 are actually over range.

TABLE A-6-3

APCC CEM DATA SUMMARY
 BACKGROUND TEST/PHASE 1
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

Apr-92

| DATE | TIME | | CO | OXYGEN | CO ₂ | CO @ 7% O ₂ |
|--------------|-------|-------|-------|--------|-----------------|------------------------|
| | From | To | | | | |
| 4/13/92 | | | | | | |
| START TEST 4 | 16:52 | 17:03 | 708 | 10.5 | 17.7 | 946 |
| | 17:03 | 17:19 | 586 | 10.8 | 17.5 | 806 |
| | 17:19 | 17:35 | 678 | 10.6 | 17.7 | 915 |
| | 17:35 | 17:51 | 566 | 10.5 | 17.4 | 756 |
| | 17:51 | 18:07 | 880 | 10.4 | 18.0 | 1165 |
| | 18:07 | 18:23 | 900 | 10.6 | 17.6 | 1215 |
| | 18:23 | 18:39 | 1000 | 10.5 | 17.7 | 1337 |
| | 18:39 | 18:55 | 1000 | 10.5 | 17.9 | 1337 |
| | 18:55 | 19:11 | 1000 | 10.5 | 17.8 | 1337 |
| | 19:11 | 19:27 | 680 | 10.5 | 17.6 | 909 |
| | 19:27 | 19:43 | 542 | 10.6 | 17.4 | 731 |
| | 19:43 | 19:59 | 584 | 10.4 | 17.9 | 773 |
| STOP TEST 4 | 19:59 | 20:15 | 572 | 10.6 | 17.6 | 772 |
| TEST AVERAGE | | | 745.8 | 10.5 | 17.7 | 1000 |

Note: CO averages of 1000 are actually over range.

TABLE A-6-4

APCC CEM DATA SUMMARY
 BACKGROUND TEST/PHASE 1
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

Apr-92

| DATE | TIME | | CO | OXYGEN | CO ₂ | CO @ 7% O ₂ |
|--------------|-------|-------|------|--------|-----------------|------------------------|
| | From | To | | | | |
| 4/13/92 | | | | | | |
| START TEST 6 | 11:28 | 11:49 | 990 | 10.2 | 17.7 | 1286.1 |
| | 11:49 | 12:05 | 1000 | 10.2 | 17.5 | 1299 |
| | 12:05 | 12:21 | 1100 | 10.2 | 17.7 | 1429 |
| | 12:35 | 12:51 | 1200 | 10.5 | 17.5 | 1604 |
| | 12:51 | 13:07 | 1150 | 10.1 | 17.9 | 1480 |
| | 13:07 | 13:23 | 1300 | 10.3 | 17.8 | 1705 |
| | 13:23 | 13:39 | 1350 | 10.2 | 17.8 | 1754 |
| | 13:39 | 13:55 | 1400 | 10.1 | 17.8 | 1802 |
| STOP TEST 6 | 13:55 | 14:11 | 1150 | 10.1 | 17.7 | 1480 |
| TEST AVERAGE | | | 1182 | 10.2 | 17.7 | 1538 |

TABLE A-6-5

APCC CEM DATA SUMMARY
 BACKGROUND TEST/PHASE 1
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

Apr-92

| DATE | TIME | TIME | CO | OXYGEN | CO2 | CO @ 7% O2 |
|--------------|-------|-------|-------|--------|------|------------|
| TEST NO. | From | To | (ppm) | (%) | (%) | (ppm) |
| 4/13/92 | | | | | | |
| START TEST 7 | 16:12 | 16:30 | 1400 | 10.4 | 17.7 | 1853 |
| | 16:30 | 16:46 | 1300 | 10.6 | 17.5 | 1754 |
| | 16:46 | 17:02 | 1000 | 10.4 | 17.6 | 1324 |
| | 17:02 | 17:18 | 585 | 10.8 | 17.3 | 805 |
| | 17:18 | 17:34 | 780 | 10.8 | 17.3 | 1073 |
| | 17:34 | 17:50 | 1200 | 10.5 | 17.6 | 1604 |
| | 17:50 | 18:06 | 880 | 10.7 | 17.4 | 1199 |
| | 18:06 | 18:22 | 1200 | 10.5 | 17.6 | 1604 |
| STOP TEST 7 | 18:22 | 18:38 | 800 | 10.6 | 17.4 | 1080 |
| TEST AVERAGE | | | 1016 | 10.6 | 17.5 | 1370 |

TABLE A-6-6

APCC CEM DATA SUMMARY

BACKGROUND TEST/PHASE 1

LONESTAR INDUSTRIES, INC.

CAPE GIRARDEAU, MISSOURI

Apr-92

| DATE | TIME | TIME | CO | OXYGEN | CO2 | CO @ 7% O2 |
|--------------|-------|-------|-------|--------|------|------------|
| TEST NO. | From | To | (ppm) | (%) | (%) | (ppm) |
| 4/13/92 | | | | | | |
| START TEST 8 | 20:30 | 20:49 | 1100 | 11.0 | 17.1 | 1544 |
| | 20:49 | 21:04 | 1250 | 10.3 | 17.5 | 1639 |
| | 21:04 | 21:20 | 1250 | 10.8 | 16.9 | 1720 |
| | 21:20 | 21:36 | 900 | 10.5 | 17.2 | 1203 |
| | 21:36 | 21:51 | 801 | 10.8 | 17.0 | 1102 |
| | 21:51 | 22:07 | 1020 | 10.6 | 17.2 | 1377 |
| | 22:07 | 22:23 | 1000 | 10.4 | 17.3 | 1324 |
| | 22:23 | 22:38 | 1000 | 10.4 | 17.3 | 1324 |
| STOP TEST 8 | 22:38 | 22:44 | 1020 | 10.3 | 17.2 | 1338 |
| TEST AVERAGE | | | 1038 | 10.6 | 17.2 | 1397 |

**TABLE A-7
PARTICULATE/CHLORINE/HCl DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST NO. | 3-CL | 4-CL | 5-CL |
|---|------------|-------------|-------------|
| DATE: | 6/25/92 | 6/25/92 | 6/25/92 |
| TIME : | 8:38-10:46 | 17:50-19:56 | 22:02-00:10 |
| TEST DATA INPUT | | | |
| Barometric Pressure (in. Hg) | 29.2 | 29.2 | 29.25 |
| Stack Area (ft ²) | 95.03 | 95.03 | 95.03 |
| Nozzle Diameter (in.) | 0.19 | 0.188 | 0.188 |
| Total Sampling Time (min.) | 120 | 120 | 120 |
| Calibration Factor (Y) | 1.02 | 1.02 | 1.02 |
| Pitot Coefficient | 0.84 | 0.84 | 0.84 |
| Average Square Root of Velocity Head (in. wc) | 1.132 | 1.163 | 1.15 |
| Average Orifice Pressure Drop (in. wc) | 1.187 | 1.254 | 1.225 |
| Average Meter Temp. (°F) | 87 | 100 | 86 |
| Average Stack Pressure (in. wc) | -0.7 | -0.7 | -0.7 |
| Average Stack Temp. (°F) | 246 | 246 | 242 |
| Meter Volume @ Meter Conditions (ft ³) | 69.78 | 72.91 | 71.04 |
| Total Water Collected (ml) | 248 | 250 | 250 |
| CO ₂ in Stack Gas (%) | 17.1 | 16.9 | 16.9 |
| O ₂ in Stack Gas (%) | 10.6 | 11 | 10.8 |
| CO in Stack Gas (%) | 0.2 | 0.1 | 0.1 |
| Total Particulate (mg) | 82.5 | 77.3 | 74.1 |
| Total Chlorine (mg) | 0.1 | 0.2 | 0.3 |
| Total HCl (mg) | 15.3 | 17.3 | 28.3 |
| CALCULATED VALUES | | | |
| Meter Volume (dscf) | 67.25 | 68.65 | 68.71 |
| Water Vapor in Stack Gas (%) | 14.79 | 14.63 | 14.62 |
| Molecular Weight of Stack Gas (dry) | 31.16 | 31.144 | 31.136 |
| Molecular Weight of Stack Gas (wet) | 29.21 | 29.22 | 29.22 |
| Average Velocity of Stack Gas (fpm) | 4,441 | 4,562 | 4,495 |
| Actual Stack Gas Flowrate (acfm) | 422,041 | 433,547 | 427,157 |
| Stack Gas Flowrate (dscfm) | 262,015 | 269,655 | 267,690 |
| Isokinesis (%) | 103.29 | 104.64 | 105.51 |
| EMISSION CONCENTRATION | | | |
| Particulate Concentration (gr/acf) | 0.012 | 0.011 | 0.010 |
| Particulate Concentration (gr/dscf) | 0.019 | 0.017 | 0.017 |
| Particulate Concentration (lbs/dscf) | 2.70E-06 | 2.48E-06 | 2.38E-06 |
| Particulate Concentration (µg/m ³) | 26912.352 | 24748.511 | 23880.358 |
| EMISSION RATE | | | |
| Particulate Emission Rate (lbs/hr) | 42.48 | 40.13 | 38.15 |
| Particulate Concentration (gr/dscf@7%O ₂) | 0.026 | 0.024 | 0.023 |
| Chlorine Emission Rate (g/hr) | 23.38 | 47.14 | 70.12 |
| HCL Emission Rate (g/hr) | 3,576.63 | 4,077.38 | 6,614.94 |

TABLE A-8
SUMMARY OF CHLORIDE MASS BALANCE DATA
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| SAMPLE IDENTIFICATION | % CHLORIDE WET BASIS | SAMPLE IDENTIFICATION | % CHLORIDE WET BASIS |
|---------------------------|-------------------------|---------------------------|-------------------------|
| 3-1 MB (Raw Feed) | 0.045 | 7-1 MB (Raw Feed) | 0.052 |
| 3-3 MB (Coal-Precalciner) | 0.11 | 7-3 MB (Coal-Precalciner) | 0.11 |
| 3-4 MB (Quench Water) | 0.0031 | 7-4 MB (Quench Water) | 0.0032 |
| 3-5 MB (Tires) | 0.11 | 7-5 MB (Tires) | 0.12 |
| 3-6 MB (Bypass Dust) | 7.4 | 7-6 MB (Bypass Dust) | 14.0 |
| 3-7 MB (Clinker) | 0.200 | 7-7 MB (Clinker) | 0.110 |
| 3-8 MB (Kiln Dust) | 0.31 | 7-8 MB (Kiln Dust) | 0.33 |
| 3-9 MB (WDSF) | 0.12 | 7-9 MB (WDSF) | 0.17 |
| 3-10 MB (WDLF) | 4.82 | 7-10 MB (WDLF) | 4.55 |
| 4-1 MB (Raw Feed) | 0.049 | 8-1 MB (Raw Feed) | 0.058 |
| 4-3 MB (Coal-Precalciner) | 0.09 | 8-3 MB (Coal-Precalciner) | 0.10 |
| 4-4 MB (Quench Water) | 0.0033 | 8-4 MB (Quench Water) | 0.0039 |
| 4-5 MB (Tires) | 0.10 | 8-5 MB (Tires) | 0.19 |
| 4-6 MB (Bypass Dust) | 10.0 | 8-6 MB (Bypass Dust) | 18.0 |
| 4-7 MB (Clinker) | 0.093 | 8-7 MB (Clinker) | 0.047 |
| 4-8 MB (Kiln Dust) | 0.29 | 8-8 MB (Kiln Dust) | 0.29 |
| 4-9 MB (WDSF) | 0.20 | 8-9 MB (WDSF) | 0.14 |
| 4-10 MB (WDLF) | 4.65 | 8-10 MB (WDLF) | 4.50 |
| 5-1 MB (Raw Feed) | 0.051 | 9-1 MB (Raw Feed) | 0.052 |
| 5-3 MB (Coal-Precalciner) | 0.08 | 9-3 MB (Coal-Precalciner) | 0.11 |
| 5-4 MB (Quench Water) | 0.0035 | 9-4 MB (Quench Water) | 0.0036 |
| 5-5 MB (Tires) | 0.14 | 9-5 MB (Tires) | 0.27 |
| 5-6 MB (Bypass Dust) | 9.3 | 9-6 MB (Bypass Dust) | 17.0 |
| 5-7 MB (Clinker) | 0.140 | 9-7 MB (Clinker) | 0.050 |
| 5-8 MB (Kiln Dust) | 0.30 | 9-8 MB (Kiln Dust) | 0.27 |
| 5-9 MB (WDSF) | 0.24 | 9-9 MB (WDSF) | 0.28 |
| 5-10 MB (WDLF) | 4.58 | 9-10 MB (WDLF) | 5.07 |

A14

**TABLE A-9
METALS DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI**

| TEST NO. | (6 BLANK) | 7-ME | 8-ME | 9-ME |
|--|-----------|-------------|-------------|-------------|
| DATE: | | 6/26/92 | 6/26/92 | 6/26/92 |
| TIME: | | 13:51-16:01 | 18:08-20:20 | 21:54-00:03 |
| TEST DATA INPUT | | | | |
| Barometric Pressure (in. Hg) | | 29.3 | 29.3 | 29.3 |
| Stack Area (ft ²) | | 95.03 | 95.03 | 95.03 |
| Nozzle Diameter (in.) | | 0.188 | 0.188 | 0.188 |
| Total Sampling Time (min.) | | 120 | 120 | 120 |
| Calibration Factor (Y) | | 1.01 | 1.01 | 1.01 |
| Pitot Coefficient | | 0.84 | 0.84 | 0.84 |
| Average Square Root of Velocity Head (in. wc) | | 1.075 | 1.1045 | 1.077 |
| Average Orifice Pressure Drop (in. wc) | | 0.909 | 1.003 | 0.996 |
| Average Meter Temp. (°F) | | 100 | 99 | 95 |
| Average Stack Pressure (in. wc) | | -0.7 | -0.7 | -0.7 |
| Average Stack Temp. (°F) | | 310 | 310 | 310 |
| Meter Volume @ Meter Conditions (ft ³) | | 62.47 | 65.17 | 64.73 |
| Total Water Collected (ml) | | 240 | 240 | 240 |
| CO ₂ in Stack Gas (%) | | 19 | 19.2 | 19.2 |
| O ₂ in Stack Gas (%) | | 9.5 | 9.3 | 9.2 |
| CO in Stack Gas (%) | | 0.2 | 0.2 | 0.2 |
| Total Catch As (mg) | | 0.00264 | 0.00431 | 0.00418 |
| Total Catch Be (mg) | | 0.00010 | 0.00010 | 0.00029 |
| Total Catch Cd (mg) | | 0.00342 | 0.03021 | 0.00010 |
| Total Catch Cr (mg) | | 0.02269 | 0.00010 | 0.00010 |
| Total Catch Pb (mg) | | 0.02632 | 0.02369 | 0.05572 |
| Total Catch Zn (mg) | | 0.05362 | 0.00010 | 0.03862 |
| Total Catch Hg (mg) | | 0.07514 | 0.06893 | 0.25039 |
| CALCULATED VALUES | | | | |
| Meter Volume (dscf) | | 58.39 | 61.04 | 61.06 |
| Water Vapor in Stack Gas (%) | | 16.21 | 15.62 | 15.61 |
| Molecular Weight of Stack Gas (dry) | | 31.42 | 31.444 | 31.44 |
| Molecular Weight of Stack Gas (wet) | | 29.24 | 29.34 | 29.34 |
| Average Velocity of Stack Gas (fpm) | | 4,395 | 4,508 | 4,396 |
| Actual Stack Gas Flowrate (acfm) | | 417,625 | 428,355 | 417,708 |
| Stack Gas Flowrate (dscfm) | | 234,563 | 242,293 | 236,295 |
| Isokinesis (%) | | 102.32 | 103.55 | 106.22 |
| EMISSION CONCENTRATION | | | | |
| Concentration As (µg/m ³) | | 1.59653 | 2.49342 | 2.41727 |
| Concentration Be (µg/m ³) | | 0.06047 | 0.05785 | 0.16771 |
| Concentration Cd (µg/m ³) | | 2.06823 | 17.47706 | 0.05783 |
| Concentration Cr (µg/m ³) | | 13.72167 | 0.05785 | 0.05783 |
| Concentration Pb (µg/m ³) | | 15.91689 | 13.70512 | 32.22254 |
| Concentration Zn (µg/m ³) | | 32.42643 | 0.05785 | 22.33371 |
| Concentration Hg (µg/m ³) | | 45.44055 | 39.87732 | 144.79902 |
| EMISSION RATE | | | | |
| Emission Rate As (g/hr) | | 0.63633 | 1.02655 | 0.97052 |
| Emission Rate Be (g/hr) | | 0.02410 | 0.02382 | 0.06733 |
| Emission Rate Cd (g/hr) | | 0.82433 | 7.19537 | 0.02322 |
| Emission Rate Cr (g/hr) | | 5.46903 | 0.02382 | 0.02322 |
| Emission Rate Pb (g/hr) | | 6.34398 | 5.64245 | 12.93721 |
| Emission Rate Zn (g/hr) | | 12.92418 | 0.02382 | 8.96689 |
| Emission Rate Hg (g/hr) | | 18.11121 | 16.41764 | 58.13620 |

TABLE A-10
Cr DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI

| TEST NO. (6 BLANK) | 7-Cr | 8-Cr | 9-Cr |
|--|-------------|-------------|-------------|
| DATE: | 6/26/92 | 6/26/92 | 6/26/92 |
| TIME: | 13:50-16:09 | 18:07-20:27 | 21:54-00:14 |
| TEST DATA INPUT | | | |
| Barometric Pressure (in. Hg) | 29.3 | 29.3 | 29.3 |
| Stack Area (ft ²) | 95.03 | 95.03 | 95.03 |
| Nozzle Diameter (in.) | 0.188 | 0.188 | 0.188 |
| Total Sampling Time (min.) | 120 | 120 | 120 |
| Calibration Factor (Y) | 1.01 | 1.01 | 1.01 |
| Pitot Coefficient | 0.84 | 0.84 | 0.84 |
| Average Square Root of Velocity Head (in. wc) | 1.077 | 1.091 | 1.094 |
| Average Orifice Pressure Drop (in. wc) | 0.942 | 0.959 | 0.969 |
| Average Meter Temp. (°F) | 93 | 92 | 89 |
| Average Stack Pressure (in. wc) | -0.7 | -0.7 | -0.7 |
| Average Stack Temp. (°F) | 310 | 310 | 310 |
| Meter Volume @ Meter Conditions (ft ³) | 63.96 | 64 | 64.09 |
| Total Water Collected (ml) | 240 | 240 | 240 |
| CO ₂ in Stack Gas (%) | 19 | 19.2 | 19.2 |
| O ₂ in Stack Gas (%) | 9.5 | 9.3 | 9.2 |
| CO in Stack Gas (%) | 0.2 | 0.2 | 0.2 |
| Total Cr6 Catch (mg) | 0.0007 | 0.0007 | 0.0007 |
| CALCULATED VALUES | | | |
| Meter Volume (dscf) | 60.54 | 60.69 | 61.11 |
| Water Vapor in Stack Gas (%) | 15.72 | 15.69 | 15.60 |
| Molecular Weight of Stack Gas (dry) | 31.42 | 31.444 | 31.44 |
| Molecular Weight of Stack Gas (wet) | 29.31 | 29.33 | 29.34 |
| Average Velocity of Stack Gas (fpm) | 4,398 | 4,453 | 4,465 |
| Actual Stack Gas Flowrate (acfm) | 417,936 | 423,191 | 424,291 |
| Stack Gas Flowrate (dscfm) | 236,100 | 239,161 | 240,041 |
| Isokinesis (%) | 105.41 | 104.31 | 104.65 |
| EMISSION CONCENTRATION | | | |
| Cr6 Concentration (gr/acf) | 0.000 | 0.000 | 0.000 |
| Cr6 Concentration (gr/dscf) | 0.000 | 0.000 | 0.000 |
| Cr6 Concentration (lbs/dscf) | 2.55E-11 | 2.54E-11 | 2.52E-11 |
| Cr6 Concentration (µg/Nm ³) | 4.09E-01 | 4.08E-01 | 4.05E-01 |
| EMISSION RATE | | | |
| Cr6 Emission Rate (g/hr) | 0.16 | 0.17 | 0.16 |

TABLE A-11
 MASS BALANCE METALS DATA
 CERTIFICATION OF COMPLIANCE TEST/PHASE 2
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI

ELEMENT

TEST NUMBER (MATRIX)

| TEST NUMBER (MATRIX) | Silver (Ag) mg/kg | Arsenic (As) mg/kg | Barium (Ba) mg/kg | Beryllium (Be) mg/kg | Cadmium (Cd) mg/kg | Chromium (Cr) mg/kg | Mercury (Hg) mg/kg | Lead (Pb) mg/kg | Antimony (Sb) mg/kg | Thallium (Tl) mg/kg | Zinc (Zn) mg/kg |
|----------------------|----------------------|-----------------------|----------------------|-------------------------|-----------------------|------------------------|-----------------------|--------------------|------------------------|------------------------|--------------------|
| 7(RAW FEED) | 0.665 | 0.764 | 14.100 | 0.517 | 3.510 | 18.700 | 0.414 | 8.890 | 0.295 | 4.760 | 20.300 |
| 7(COAL PRECAL) | 0.489 | 5.460 | 60.700 | 0.331 | 0.237 | 16.600 | 0.205 | 6.300 | 0.383 | 0.727 | 53.400 |
| 7(QUENCH-H2O)* | 0.007 | 0.005 | 0.104 | 0.004 | 0.001 | 0.150 | 0.004 | 0.008 | 0.005 | 0.002 | 0.066 |
| 7(TIRES) | 0.460 | 0.959 | 13.200 | 0.053 | 1.820 | 4.830 | 0.094 | 10.800 | 7.900 | 0.105 | 5584.000 |
| 7(BYPASS DUST) | 2.520 | 18.100 | 55.300 | 0.528 | 346.000 | 32.200 | 0.093 | 685.000 | 0.767 | 1.690 | 113.000 |
| 7(CLINKER) | 0.540 | 15.500 | 56.400 | 0.830 | 3.270 | 39.700 | 0.088 | 23.800 | 0.389 | 0.179 | 92.800 |
| 7(KILN DUST) | 0.364 | 2.220 | 14.700 | 0.210 | 3.640 | 8.550 | 0.624 | 19.400 | 0.274 | 49.200 | 26.300 |
| 7(WDSF) | 6.190 | 8.260 | 309.000 | 0.196 | 1.280 | 204.000 | 9.710 | 65.500 | 2.430 | 0.270 | 637.000 |
| 7(WDLF)* | 3.670 | 200.000 | 912.000 | 2.400 | 289.000 | 612.000 | 1.840 | 595.000 | 19.050 | 0.109 | 951.000 |
| 8(RAW FEED) | 0.411 | 1.430 | 12.400 | 0.608 | 1.590 | 20.400 | 0.510 | 14.600 | 0.281 | 3.940 | 20.900 |
| 8(COAL PRECAL) | 0.546 | 3.950 | 51.500 | 0.590 | 0.175 | 15.700 | 0.078 | 5.590 | 0.302 | 0.671 | 46.100 |
| 8(QUENCH-H2O)* | 0.007 | 0.001 | 0.100 | 0.004 | 0.001 | 0.283 | 0.004 | 0.009 | 0.005 | 0.002 | 0.062 |
| 8(TIRES) | 0.685 | 3.660 | 20.200 | 0.081 | 16.600 | 56.800 | 0.096 | 31.200 | 6.530 | 0.162 | 16200.000 |
| 8(BYPASS DUST) | 4.270 | 16.800 | 80.800 | 0.449 | 501.000 | 38.500 | 0.094 | 1060.000 | 0.588 | 2.260 | 128.000 |
| 8(CLINKER) | 0.444 | 16.500 | 60.200 | 0.771 | 4.480 | 33.000 | 0.083 | 14.900 | 0.368 | 0.147 | 84.800 |
| 8(KILN DUST) | 0.475 | 2.480 | 15.300 | 0.219 | 5.030 | 10.400 | 0.798 | 20.700 | 0.294 | 56.500 | 29.900 |
| 8(WDSF) | 0.503 | 6.660 | 368.000 | 0.237 | 2.060 | 187.000 | 9.840 | 54.600 | 1.750 | 0.525 | 658.000 |
| 8(WDLF)* | 3.940 | 185.000 | 826.000 | 2.420 | 280.000 | 605.000 | 1.420 | 611.000 | 11.650 | 0.123 | 441.000 |
| 9(RAW FEED) | 0.408 | 0.754 | 11.400 | 0.536 | 1.330 | 16.900 | 0.495 | 11.500 | 0.350 | 4.440 | 20.700 |
| 9(COAL PRECAL) | 0.535 | 3.190 | 70.800 | 0.254 | 0.242 | 20.400 | 0.135 | 3.960 | 0.303 | 0.418 | 65.200 |
| 9(QUENCH-H2O)* | 0.007 | 0.002 | 0.109 | 0.002 | 0.001 | 0.012 | 0.004 | 0.006 | 0.005 | 0.002 | 0.080 |
| 9(TIRES) | 0.684 | 1.070 | 6.430 | 0.039 | 35.100 | 99.800 | 0.085 | 25.800 | 1.240 | 0.179 | 8650.000 |
| 9(BYPASS DUST) | 4.230 | 17.800 | 82.200 | 0.551 | 467.000 | 32.900 | 0.154 | 1000.000 | 2.550 | 5.230 | 126.000 |
| 9(CLINKER) | 0.440 | 17.900 | 63.900 | 0.894 | 4.090 | 32.200 | 0.078 | 30.200 | 0.754 | 0.149 | 86.400 |
| 9(KILN DUST) | 0.559 | 3.120 | 16.700 | 0.296 | 4.320 | 6.190 | 0.825 | 33.400 | 0.399 | 88.800 | 29.300 |
| 9(WDSF) | 0.495 | 15.200 | 356.000 | 0.269 | 2.470 | 277.000 | 11.500 | 60.700 | 3.410 | 0.774 | 806.000 |
| 9(WDLF)* | 3.130 | 168.000 | 490.210 | 2.590 | 277.000 | 589.000 | 1.860 | 621.000 | 10.810 | 0.155 | 297.000 |

*RESULTS REPORTED IN MG/L

Corrected

TABLE A-12
 VOST TRAIN WORKSHEET
 BIF COC TEST PROGRAM/PHASE 2
 LONESTAR INDUSTRIES, INC.
 CAPE GIRARDEAU, MISSOURI
 Jun-92

| Test Number | 3A | 3B | 3C | 3D | Total/Avg. | Normal Liters | Concentration ug/l | Emission Rate g/hr |
|----------------------------|-------|-------|-------|-------|------------|---------------|--------------------|--------------------|
| Sample Volume (l) | 20.61 | 21.58 | 21.37 | 21.05 | 84.61 | 75.31 | | |
| Meter Temperature (°C) | 34 | | | | 34 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.2 | | | |
| Flowrate (dscfm) | | | | | 262015 | | | |
| Dry Gas Meter % | | | | | 0.956 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00133 | 0.591 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00133 | 0.591 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00133 | 0.591 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00133 | 0.591 |
| Test Number | 4A | 4B | 4C | 4D | | | | |
| Sample Volume (l) | 21.46 | 20.64 | 20.87 | 20.79 | 83.76 | 73.13 | | |
| Meter Temperature (°C) | 40 | | | | 40 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.2 | | | |
| Flowrate (dscfm) | | | | | 269655 | | | |
| Dry Gas Meter % | | | | | 0.956 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00137 | 0.626 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00137 | 0.626 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00137 | 0.626 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00137 | 0.626 |
| Test Number | 5A | 5B | 5C | 5D | | | | |
| Sample Volume (l) | 20.57 | 20.7 | 20.9 | 22.3 | 84.47 | 75.56 | | |
| Meter Temperature (°C) | 33 | | | | 33 | | | |
| Barometric Press. (in.Hg.) | | | | | 29.25 | | | |
| Flowrate (dscfm) | | | | | 267690 | | | |
| Dry Gas Meter % | | | | | 0.956 | | | |
| Target Compounds (ug) | | | | | | | | |
| Perchloroethylene | | | | | 0.1 | | 0.00132 | 0.602 |
| Trichlorotrifluoromethane | | | | | 0.1 | | 0.00132 | 0.602 |
| 1,1,1 Trichloroethane | | | | | 0.1 | | 0.00132 | 0.602 |
| 1,1,2 Trichloroethane | | | | | 0.1 | | 0.00132 | 0.602 |

TABLE A-13-1
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# DATE | TIME From | TIME To | CO (ppm) | CO2 (%) | O2 (%) | NOX (ppm) | SO2 (ppm) | THC (ppm) | CO Corr. (ppm) | THC Corr. (ppm dry) | CO Corr. Rolling Avg | THC Corr. Rolling Avg |
|---------------|--------------|------------|-------------|------------|-----------|--------------|--------------|--------------|-------------------|------------------------|-------------------------|--------------------------|
| 6/25/92 | | | | | | | | | | | | |
| Start #3 | 8:33 | 8:48 | 4144 | 17.3 | 10.6 | 137 | 131 | 25 | 5578 | 40 | | |
| | 8:48 | 9:03 | 3617 | 17.6 | 10.3 | 136 | 111 | 23 | 4733 | 35 | | |
| | 9:03 | 9:18 | 3409 | 18.1 | 10 | 115 | 93 | 22 | 4339 | 33 | 5143 | 42 |
| | 9:18 | 9:33 | 3446 | 18 | 10.2 | 103 | 88 | 23 | 4467 | 35 | 4779 | 36 |
| | 9:33 | 9:48 | 3458 | 17.9 | 10.2 | 95 | 87 | 22 | 4483 | 34 | 4505 | 34 |
| | 9:48 | 10:03 | 3696 | 17.7 | 10.2 | 92 | 84 | 23 | 4791 | 35 | 4520 | 34 |
| | 10:03 | 10:18 | 2405 | 17.5 | 10.1 | 104 | 73 | 23 | 3089 | 35 | 4207 | 35 |
| | 10:18 | 10:33 | 1668 | 16.9 | 10.4 | 106 | 58 | 24 | 2203 | 37 | 3641 | 35 |
| | 10:33 | 10:48 | 1743 | 16.1 | 11 | 110 | 50 | 24 | 2440 | 40 | 3131 | 37 |
| | 10:48 | 11:03 | 1114 | 16.1 | 11.3 | 111 | 42 | 26 | 1608 | 44 | 2335 | 39 |
| | 11:03 | 11:18 | 809 | 16.2 | 11.2 | 111 | 37 | 24 | 1156 | 40 | 1852 | 40 |
| | 11:18 | 11:33 | 787 | 15.8 | 11.2 | 107 | 32 | 23 | 1124 | 39 | 1582 | 41 |
| End #3 | 11:33 | 11:48 | 563 | 15.7 | 11.6 | 107 | 30 | 24 | 839 | 42 | 1182 | 41 |
| | 11:48 | 12:03 | 258 | 14.6 | 12.1 | 104 | 25 | 23 | 406 | 43 | 881 | 41 |
| TEST AVG. | | | 2223 | 16.8 | 10.7 | 110 | 67 | 24 | 2947 | 38 | 3147 | 38 |

TABLE A-13-2
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# | TIME | TIME | OO | CO2 | O2 | NOx | SO2 | THC | CO Corr. | THC Corr. | CO Corr. | THC Corr. |
|-----------|-------|-------|--------|------|------|-------|-------|-------|----------|-----------|-------------|-------------|
| DATE | From | To | (ppm) | (%) | (%) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm dry) | Rolling Avg | Rolling Avg |
| 6/25/92 | | | | | | | | | | | | |
| Start #4 | 17:48 | 18:03 | 1856 | 17.7 | 10.7 | 190 | 101 | 22 | 2523 | 35 | 2198 | 34 |
| | 18:03 | 18:18 | 1430 | 17.2 | 11 | 203 | 99 | 22 | 2002 | 36 | 2176 | 34 |
| | 18:18 | 18:33 | 1449 | 17.6 | 10.9 | 185 | 103 | 22 | 2009 | 36 | 2129 | 34 |
| | 18:33 | 18:48 | 1691 | 17.4 | 11 | 170 | 111 | 22 | 2367 | 36 | 2225 | 36 |
| | 18:48 | 19:03 | 2226 | 17.6 | 10.8 | 148 | 117 | 21 | 3055 | 34 | 2358 | 36 |
| | 19:03 | 19:18 | 1621 | 17.2 | 10.8 | 172 | 102 | 22 | 2225 | 36 | 2414 | 35 |
| | 19:18 | 19:33 | 882 | 16.6 | 11 | 218 | 92 | 22 | 1235 | 36 | 2221 | 35 |
| | 19:33 | 19:48 | 766 | 16.8 | 11 | 250 | 92 | 22 | 1072 | 36 | 1897 | 35 |
| | 19:48 | 20:03 | 538 | 16.4 | 11.1 | 290 | 97 | 21 | 761 | 35 | 1323 | 36 |
| | 20:03 | 20:18 | 442 | 16.1 | 11.4 | 309 | 96 | 21 | 645 | 36 | 928 | 36 |
| | 20:18 | 20:33 | 535 | 16.4 | 11.3 | 240 | 93 | 21 | 772 | 36 | 812 | 36 |
| End #4 | 20:33 | 20:48 | 445 | 15.7 | 11.6 | 219 | 87 | 20 | 663 | 35 | 710 | 35 |
| TEST AVG. | | | 1156.8 | 16.9 | 11.1 | 216 | 99 | 22 | 1611 | 36 | 1783 | 35 |

TABLE A-13-3
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# DATE | TIME From | TIME To | CO (ppm) | CO2 (%) | O2 (%) | NOX (ppm) | SO2 (ppm) | THC (ppm) | CO Corr. (ppm) | THC Corr. (ppm dry) | CO Corr. Rolling Avg | THC Corr. Rolling Avg |
|---------------|--------------|------------|-------------|------------|-----------|--------------|--------------|--------------|-------------------|------------------------|-------------------------|--------------------------|
| | | | | | | | | | | | | |
| 6/25/92 | | | | | | | | | | | | |
| Start #5 | 21:48 | 22:03 | 1823 | 17 | 10.9 | 206 | 89 | 21 | 2527 | 34 | 1339 | 35 |
| | 22:03 | 22:18 | 1417 | 17.6 | 10.5 | 210 | 93 | 20 | 1889 | 31 | 1529 | 34 |
| | 22:18 | 22:33 | 1388 | 17.5 | 10.7 | 178 | 98 | 20 | 1887 | 32 | 1824 | 33 |
| | 22:33 | 22:48 | 1860 | 17.4 | 10.6 | 172 | 98 | 20 | 2504 | 32 | 2202 | 32 |
| | 22:48 | 23:03 | 1732 | 17.6 | 10.3 | 174 | 93 | 20 | 2266 | 31 | 2136 | 31 |
| | 23:03 | 23:18 | 1981 | 17.4 | 10.7 | 175 | 91 | 20 | 2693 | 32 | 2337 | 32 |
| | 23:18 | 23:33 | 1163 | 17.7 | 10.2 | 203 | 86 | 21 | 1508 | 32 | 2243 | 32 |
| | 23:33 | 23:48 | 699 | 16.4 | 11 | 227 | 78 | 21 | 979 | 35 | 1861 | 32 |
| | 23:48 | 0:03 | 930 | 16.5 | 11.1 | 229 | 85 | 21 | 1315 | 35 | 1623 | 33 |
| | 0:03 | 0:18 | 640 | 16.4 | 11.1 | 254 | 93 | 21 | 905 | 35 | 1177 | 34 |
| | 0:18 | 0:33 | 515 | 16.4 | 11.2 | 263 | 104 | 20 | 736 | 34 | 984 | 35 |
| | 0:33 | 0:48 | 324 | 15.8 | 11.5 | 304 | 93 | 20 | 477 | 35 | 858 | 35 |
| End #5 | 0:48 | 1:03 | 409 | 16.3 | 11.1 | 283 | 76 | 19 | 578 | 32 | 674 | 34 |
| TEST AVG. | | | 1144.7 | 16.9 | 10.8 | 221 | 91 | 20 | 1559 | 33 | 1599 | 33 |

TABLE A-13-4
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# DATE | TIME | | CO (ppm) | CO2 (%) | O2 (%) | NOx (ppm) | SO2 (ppm) | THC (ppm) | CO Corr. (ppm) | THC Corr. (ppm dry) | CO Corr. Rolling Avg | THC Corr. Rolling Avg |
|---------------|-------|-------|-------------|------------|-----------|--------------|--------------|--------------|-------------------|------------------------|-------------------------|--------------------------|
| | From | To | | | | | | | | | | |
| 6/26/92 | | | | | | | | | | | | |
| Start #7 | 13:49 | 14:04 | 3800 | 19.5 | 9.1 | 171 | 216 | 43 | 4471 | 60 | 3614 | 54 |
| | 14:04 | 14:19 | 4359 | 20.4 | 8.5 | 204 | 215 | 48 | 4882 | 63 | 4086 | 58 |
| | 14:19 | 14:34 | 3831 | 20.2 | 8.7 | 221 | 215 | 43 | 4360 | 58 | 4236 | 59 |
| | 14:34 | 14:49 | 3074 | 19.6 | 8.9 | 232 | 232 | 65 | 3557 | 88 | 4317 | 67 |
| | 14:49 | 15:04 | 1948 | 20.7 | 8.8 | 255 | 217 | 43 | 2235 | 58 | 3759 | 67 |
| | 15:04 | 15:19 | 1620 | 20.1 | 9.1 | 223 | 187 | 41 | 1906 | 57 | 3015 | 65 |
| | 15:19 | 15:34 | 1269 | 17.4 | 10.7 | 181 | 109 | 36 | 1725 | 58 | 2356 | 65 |
| | 15:34 | 15:49 | 1654 | 17.5 | 10.4 | 188 | 83 | 33 | 2185 | 51 | 2013 | 56 |
| | 15:49 | 16:04 | 1173 | 17.1 | 10.6 | 186 | 84 | 31 | 1579 | 49 | 1849 | 54 |
| | 16:04 | 16:19 | 1423 | 17.2 | 10.4 | 197 | 89 | 32 | 1879 | 50 | 2877 | 81 |
| | 16:19 | 16:34 | 1452 | 17.3 | 10.6 | 205 | 89 | 30 | 1955 | 48 | 1900 | 50 |
| End #7 | 16:34 | 16:49 | 1295 | 17.4 | 10.4 | 230 | 93 | 30 | 1710 | 47 | 1781 | 48 |
| TEST AVG. | | | 2242 | 18.7 | 9.7 | 208 | 152 | 40 | 2704 | 57 | 2983 | 60 |

TABLE A-13-5
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# | TIME | TIME | CO | O2 | NOx | SO2 | THC | CO Corr. | THC Corr. | CO Corr. | THC Corr. |
|-----------|-------|-------|-------|------|-------|-------|-------|----------|-----------|-------------|-------------|
| DATE | From | To | (ppm) | (%) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm dry) | Rolling Avg | Rolling Avg |
| 6/26/92 | 17:49 | 18:04 | 1942 | 20 | 245 | 211 | 41 | 2266 | 56 | 2133 | 55 |
| Start #8 | 18:04 | 18:19 | 3475 | 20.7 | 220 | 220 | 43 | 3923 | 57 | 2633 | 56 |
| | 18:19 | 18:34 | 3135 | 20.5 | 263 | 219 | 46 | 3483 | 60 | 3026 | 58 |
| | 18:34 | 18:49 | 2979 | 20.2 | 280 | 223 | 47 | 3363 | 62 | 3259 | 59 |
| | 18:49 | 19:04 | 2556 | 20.3 | 309 | 223 | 43 | 2909 | 58 | 3420 | 59 |
| | 19:04 | 19:19 | 1718 | 20.2 | 349 | 232 | 43 | 1940 | 57 | 2924 | 59 |
| End #8 | 19:19 | 19:34 | 1579 | 20 | 328 | 239 | 41 | 1812 | 55 | 2506 | 58 |
| | 19:34 | 19:49 | 931 | 18.4 | 303 | 170 | 37 | 1153 | 54 | 1954 | 56 |
| | 19:49 | 20:04 | 1185 | 17.4 | 264 | 223 | 34 | 1565 | 53 | 1618 | 55 |
| | 20:04 | 20:19 | 1126 | 17.1 | 254 | 117 | 32 | 1487 | 50 | 1504 | 53 |
| | 20:19 | 20:34 | 1074 | 17.2 | 239 | 103 | 31 | 1446 | 49 | 1413 | 51 |
| | 20:34 | 20:49 | 1300 | 17.3 | 235 | 100 | 32 | 1750 | 51 | 1562 | 51 |
| TEST AVG. | | | 1917 | 19.1 | 274 | 190 | 39 | 2258 | 55 | 2329 | 56 |

TABLE A-13-6
CEM DATA SUMMARY
CERTIFICATION OF COMPLIANCE TEST PROGRAM/PHASE 2
LONESTAR INDUSTRIES, INC.
CAPE GIRARDEAU, MISSOURI
Jun-92

| TEST# | TIME | TIME | CO | CO2 | O2 | NOx | SO2 | THC | CO Corr. | THC Corr. | CO Corr. | THC Corr. |
|-----------|-------|-------|-------|------|------|-------|-------|-------|----------|-----------|-------------|-------------|
| DATE | From | To | (ppm) | (%) | (%) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm dry) | Rolling Avg | Rolling Avg |
| 6/26/92- | | | | | | | | | | | | |
| Start #9 | 21:34 | 21:49 | 1308 | 17.1 | 18.8 | 214 | 164 | 28 | 8324 | 210 | 3454 | 87 |
| | 21:49 | 22:04 | 2605 | 19.5 | 9.3 | 229 | 218 | 36 | 3117 | 51 | 3822 | 88 |
| | 22:04 | 22:19 | 4047 | 20.6 | 8.3 | 212 | 229 | 42 | 4461 | 54 | 4434 | 90 |
| | 22:19 | 22:34 | 4185 | 20.4 | 8.5 | 239 | 236 | 46 | 4687 | 61 | 5147 | 94 |
| | 22:34 | 22:49 | 3406 | 20.5 | 8.4 | 287 | 243 | 44 | 3784 | 58 | 4012 | 56 |
| | 22:49 | 23:04 | 2827 | 20.4 | 8.2 | 319 | 250 | 43 | 3092 | 55 | 4006 | 57 |
| | 23:04 | 23:19 | 1187 | 20 | 9 | 340 | 245 | 42 | 1385 | 58 | 3237 | 58 |
| | 23:19 | 23:34 | 917 | 18.5 | 9.4 | 307 | 184 | 36 | 1107 | 51 | 2342 | 55 |
| | 23:34 | 23:49 | 973 | 17.4 | 10.3 | 271 | 132 | 34 | 1273 | 52 | 1714 | 54 |
| | 23:49 | 0:04 | 1120 | 17.5 | 10.5 | 255 | 119 | 35 | 1493 | 55 | 1314 | 54 |
| End #9 | 0:04 | 0:19 | 1614 | 17.4 | 10.4 | 231 | 115 | 33 | 2132 | 51 | 1501 | 52 |
| | 0:19 | 0:34 | 2159 | 17.5 | 10.1 | 204 | 109 | 33 | 2773 | 50 | 1918 | 52 |
| TEST AVG. | | | 2196 | 19 | 10 | 259 | 187 | 38 | 3136 | 67 | 3075 | 66 |