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AP42 Section: 11.1

Reference Number: 278

**Title: Source Sampling For Particulate Emissions, R. E.
Hazard Contracting Co., San Diego, CA,**

**San Diego County Air Pollution Control District,
San Diego, CA,**

October 3, 1990.

apcd

County of San Diego



AP-42 Section Reference	11.1
Report Sect.	4
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R. J. Sommerville
Air Pollution Control Officer

May 13, 1991

R. E. Hazard Contracting Co.
Attention: Plant Superintendent
P.O. Box 229000
San Diego, CA 92122

SUBJECT: RENEWAL TEST REPORT

The enclosed test report is the result of testing done at your facility.

If you have any questions, please call me at (619) 694-3359.

A handwritten signature in cursive script, appearing to read "C. W. Ridenour".

C. W. Ridenour
C. W. Ridenour
Senior Air Pollution Chemist

CWR:jo

Enclosures

AIR POLLUTION CONTROL DISTRICT
9150 Chesapeake Drive, San Diego, California 92123-1095
(619) 694-3307 FAX (619) 694-2730

SAN DIEGO AIR POLLUTION CONTROL DISTRICT
 9150 CHESAPEAKE DRIVE
 SAN DIEGO, CA. 92123

SUMMARY:
 SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE

TEST SITE: R.E. Hazard
 10050 Black Mountain Rd.
 San Diego, CA 92126

TEST #: 90276 P.O.# 442 TEST DATE 10/3/90

EQUIPMENT: Asphalt batch plant, Hot-mix (300-Ton/hr cap), Dryer, 109m btu/hr.
 Input capacity; Standard Havens baghouse, 9660 ft² cloth area; 50,000 scfm blower;
 suspended oil particle control; enclosure for three (3) astec hb 200 ton storage silos
 enclosed conveyor to silo load-in area; three silo batchers; one 10,000 cfm blower; a
 associated vent ducting to the plant knock-out box.

UNIT TESTED: Baghouse

SITE PERSONNEL: AL TILLY
 APCD PERSONNEL: J. CAWYER, D. SHINA
 REPORT BY: J. CAWYER DATE 1/7/91
 APPROVED BY: *C.W. Ridenour* DATE: *1/91*
 C.W. RIDENOUR
 SENIOR AIR POLLUTION CHEMIST

PARAMETERS:	MEASURED:
STACK GAS FLOW RATE (DSCFM):	<u>27996</u>
STACK GAS TEMPERATURE °F (AVG):	<u>224</u>
PRODUCTION RATE (AVG): tons/hr	<u>285</u>

RESULTS: Based upon APCD Method 5 Standards relating to the entire impinger catch.

TEST	PERMIT LIMIT	MEASURED	PERFORMANCE
RULE 54 DUST AND FUME	40.00 lb/hr	11.69 lbs/hr	PASSED

TEST REFERENCE:
 San Diego Air Pollution Control District Quality Assurance Manual Method 5 for Particulate
 Emissions from Stationary Sources.

TEST DESCRIPTION

Introduction: This report presents the results of particulate loading and gas volume tests at R.E. Hazard . The test was performed on the baghouse exhaust.

System Description:

This asphalt plant combines crushed rock and sand with hot asphalt oil in batch loads of 7000 lbs. The rock and sand are dried in a rotary dryer which is heated by natural gas. The exhaust from this dryer is vented through a baghouse the emissions to the atmosphere from this baghouse are the subject of this report.

Procedures:

The procedures and equipment utilized in performing these tests are based on EPA New Source Performance Standards Method 5. The sampling train was modified to exclude the front-end filter and include a back-end filter, per the San Diego Air Pollution Control District Method 5 testing guidelines. The calculations were designed to include the impinger catch so that the test results can be compared to Rule 54 of SDAPCD.

Velocity Traverse:

Preliminary calculations were based upon data from previous tests. Temperature and pitot tube data collected during actual sampling were used to calculate stack volume.

Particulate Sampling:

This sample consisted of 24 traverse points, 12 from each of 2 sample ports as shown in Figure 1. The sample was collected 48 inches below the top of the stack. Field data associated with sample collection has been transferred to computer printout and is shown in the report. Calculations were done by computer and are also shown within the report.

Gas Analysis:

An integrated bag sample was collected on site and measured. The oxygen and carbon dioxide content of the stack gas was measured using electronic instrumentation.

SITE: R.E. Hazard

OPERATOR J. CAWYER

TEST DATE: 10/3/90

TEST: 90276

DATA SUMMARY: #

TRAVERSE POINT NUMBER	GAS METER READING (Vm), ft3	PRESS. DIFF. ACROSS PITOT TUBES	PRESS. DIFF. ACROSS ORIF. ACTUAL	DRY GAS METER TEMPERATURE		STACK TEMP	IMP. TEMP	STACK FLOW (velocity)
				INLET	OUTLET			
	787.500							
1	789.341	1.00	1.60	84	112	218	60	67.59
2	791.183	1.00	1.55	84	115	219	56	67.64
3	792.96	1.10	1.80	83	119	212	56	70.58
4	794.783	1.10	1.80	84	110	213	60	70.63
5	796.571	1.00	1.60	84	110	213	59	67.34
6	798.394	1.00	1.60	85	116	217	58	67.54
7		0.85	1.40	85	118	219	59	62.36
8	801.809	0.80	1.30	85	119	219	60	60.50
9	803.388	0.75	1.20	85	119	218	60	58.54
10	804.964	0.75	1.20	85	120	220	60	58.62
11	806.506	0.70	1.10	86	120	217	59	56.51
12	807.84	0.50	0.80	86	120	214	59	47.65
13	809.266	0.65	1.00	86	100	228	66	54.89
14	810.69	0.65	1.00	87	112	217	57	54.45
15	812.149	0.65	1.00	86	116	229	57	54.93
16	813.608	0.70	1.10	86	117	229	56	57.01
17	815.257	0.70	1.10	86	119	230	57	57.05
18	817.02	0.90	1.40	86	120	230	56	64.69
19	819.235	1.45	2.30	86	123	248	55	83.17
20	821.627	1.65	2.60	87	125	256	55	89.22
21	823.966	1.60	2.60	88	126	230	55	86.25
22	826.038	1.30	2.10	88	125	230	54	77.75
23	828.105	1.15	1.80	88	125	222	55	72.70
24	829.891	0.80	1.30	88	124	217	57	60.41

Pressures are in inches of water, temperatures are in degrees Fahrenheit, velocities are in ft/sec. All measurements are actual - uncorrected - values.

Average: Vm ΔP ΔH t1 t2 ts tl vs
 42.391 0.95 1.51 85.75 117.92 223.54 57.75 65.34

DATA SUMMARY:

PRESSURES

P bar 29.52 in Hg
P static -0.80 in H2O
Ps 29.46 in Hg

AVERAGE TEMPERATURES

ts = 224 F
tm = 1/2(avg.t1+avg.t2) = 102 F
ti = 58 F

VOLUMES

Vm, meter 42.391 ft³
Vic, Impingers 258.6 ml

VAPOR PRESSURES

Vpw @ Imp = 0.4858 inHg

METER BOX PARAMETERS

$\Delta H@$ = 2.6123 inH2O
 ΔP = 0.95 inH2O
 ΔH = 1.51 inH2O
METER BOX I.D.# D337

NOZZLE AND PROBE

Dn = 0.205 in
An = Dn²* π /4 = .0330 in²
Cp = 0.848
Y = .9796

STACK MEASUREMENTS

%CO2 4.80
%CO 0.00
%O2 14.20
%N2 81.00

STACK PARAMETERS

Stack Diameter = 4.00 ft
Ao=Area stack = 12.57 ft²

\emptyset = sampling time 72 minutes

mn=particulate collect'd 0.1200 grams

CALCULATIONS:

	UNITS	EQUATION NUMBER
$\text{corr } V_{wm} = ((V_m' \cdot V_{pw@imp}/P_s) \cdot P_m \cdot T_{std}) / (T_m \cdot P_{std})$ = water volume correction at meter w/o silica gel =	0.64 ft ³	1
$V_m \text{ std} = (V_m' \cdot T_{std} \cdot P_m / (P_{std} \cdot T_m)) - \text{corr } V_{wm}$ = dry meter volume corrected to STP =	38.01 ft ³	2
$P_m = P_{bar} + (\Delta H / 13.6)$ = corrected pressure of meter =	29.63 in Hg	3
$T_m = (t_1 + t_2) / 2 + 460$ = meter temperature =	561.8 °R	4
$T_s = t_s + 460$ = corrected stack temperature =	683.5 °R	5
$P_s = P_{bar} + (P_{static} / 13.6)$ = corrected stack pressure =	29.46 in Hg	6
$V_w \text{ std} = V_{lc} \cdot \rho \cdot R \cdot T_{std} / (P_{std} \cdot M_{wH_2O}) + \text{corr } V_{wm}$ = water volume at STP =	12.84 ft ³	7
$B_{ws} = (V_w \text{ std}) / (V_w \text{ std} + V_m \text{ std}) \cdot 100$ = percent moisture =	25.25 %	8
$m_n = \text{grams of particulate (from laboratory sheet)}$ =	0.1200 grams	9
$C_s = 15.43 \cdot m_n / V_m \text{ std}$ = grain loading (dry) =	0.049 grains/d dscf	10
$V_m' = V_m \cdot Y = \text{Corrected dry gas meter volume}$ =	41.53 ft ³	11
$M_d = 0.440(\%CO_2) + 0.320(\%O_2) + 0.280(N_2 + \text{inerts} + CO)$ Dry gas molecular weight =	29.34 g/g*mole	12
$M_s = M_d \cdot (1 - B_{ws}) + 18.0 \cdot (B_{ws})$ Stack gas molecular weight-wet basis =	26.47 g/g*mole	13

	UNITS	EQUATION NUMBER
$vs = 85.49 \cdot Cp \cdot ((Ts \cdot \Delta P) / (Ps \cdot Ms))^{.5}$ = stack velocity	65.34 (ft/s)	14
$Qs = (vs) \cdot Ao \cdot 60$ = stack flow rate	49262 (acfm)	15
$Qstd = 17.64 \cdot Qs \cdot (1 - Bws) \cdot Ps / Ts$ = flow rate at STP	27996 (dscfm)	16
$I = \frac{144 \cdot 100 \cdot Ts \cdot (.002669 \cdot Vlc + (Vm' / Tm) \cdot Pm)}{(60 \cdot \emptyset \cdot vs \cdot Ps \cdot An)}$ = isokinetic	103.29 (%)	17
$E = (0.00857) \cdot (Qstd) \cdot Cs$ = particulate emission rate	11.69 (lbs/hr)	18

SUMMARY OF CALCULATIONS:

Enter the type of plant. (Asphalt/Combustion)

I = % isokinetics = 103.3 %

Cs = grain loading (dry) = 0.049 grains/dscf

E = particulate emission rate = 11.69 lbs/hr

% CO2 = 4.80 %

NOMENCLATURE:

- multiplication
- / division
- ^ exponentiation
- Vm sample gas volume, uncorrected = (ft³)
- Vm sample gas volume, corrected = Vm*Y = ft³
- ΔP root mean pitot tube differential pressure
= (summation(press.diff. across pitot tubes^{.5})/number entries)² = (in H₂O)
- ΔH average differential pressure across the orifice = (in H₂O)
- t1 dry gas meter inlet temperature = (°F)
- t2 dry gas meter outlet temperature = (°F)
- ts stack temperature = (°F)
- ti impinger out temperature = (°F)
- vs stack gas velocity = $85.49 \cdot C_p \cdot (T_s \cdot \Delta P / (P_s \cdot M_s))^{.5}$ = (ft/s)
- Pbar = barometric pressure = (in Hg)
- Pstatic = stack static pressure = (in Hg)
- Ps = Absolute stack pressure = Pbar + (Pstatic/13.6) = (in Hg)
- tm = dry gas meter temperature = (t1+t2)/2 = (°F)
- Vlc = collected water, impingers = (ml)
- Vpw = Vapor pressure of water = (in Hg)
- ΔH @ = orifice pressure differential that equates to 0.75 cfm of air @ 68°F and 29.92 in Hg
- Dn = nozzle diameter = (in)
- An = nozzle area = $\pi \cdot D_n^2 / 4$ = (in²)
- π = the ratio of circumference of a circle to its diameter = 22/7 (dimensionless)
- Cp = pitot tube coefficient = (dimensionless)
- Y = meter box coefficient = (dimensionless)
- CO₂ = carbon dioxide = (%)
- CO = carbon monoxide = (%)
- O₂ = oxygen = (%)
- N₂ = nitrogen = (%)
- Ø = sampling time = (minutes)
- mn = particulate found in sample train = (grams)
- Ao = stack area = stack diameter² * π/4 if round; length * width if rectangular = (ft²)
- Corr Vwm = $((V_m \cdot V_{pw@imp} / P_s) \cdot P_m \cdot T_{std}) / (T_m \cdot P_{std})$ = (ft³)
- Pm = absolute meter pressure = Pbar + (ΔH/13.6) = (in Hg)
- Tstd = temperature at standard conditions = (528°R)
- Tm = dry gas meter temperature = (t1+t2)/2 + 460 = (°R)
- Pstd = pressure at standard condition = (29.92 in. Hg)
- Vm std = dry corrected volume of meter = $V_m \cdot T_{std} \cdot P_m / (P_{std} \cdot T_m) - \text{corr Vwm}$ = (ft³)
- Ts = stack temperature = (°R)
- Vw std = water volume at STP = $V_{lc} \cdot \partial \cdot R \cdot T_{std} / (P_{std} \cdot M_{wH_2O})$ = (ft³)

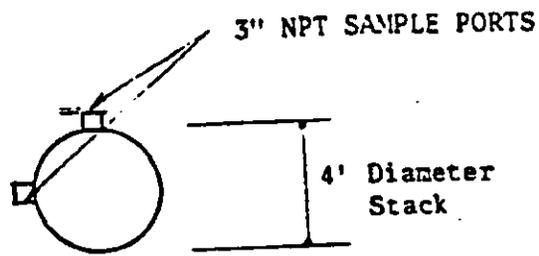
NOMENCLATURE: cont.

ρ = density of water at STP = 0.002201 = (lb/ml)
R = ideal gas constant = 21.85 in. Hg³/°R³·lb³/mole
Md = dry stack gas molecular weight = 0.32%O₂+0.44%CO₂+0.28(100-%O₂-%CO₂)
= (g/g³·mole)
Bws = fractional stack gas moisture content = (Vw std+Corr Vwm)/(Vwstd+Corr Vwm+Vm std)
= (%/100)
Cs = grain loading = 15.430³·mn/Vm std = (grains/dscf)
Mw = molecular weight = (g/g³·mole)
Ms = wet stack gas molecular weight = Md*(1-Bws)+Bws*18 = (g/g³·mole)
Qs = flow rate = vs³·Ao³·60 = (acfm)
Qstd = flow rate at standard conditions = 17.68³·Qs*(1-Bws)*Ps/Ts = (dscfm)
I = isokinetics = 144³·100³·Ts*(.002669³·Vic+Vm³/Tm)*Pm/(60³·Ø³·vs³·Ps³·An) = (%)
E = particulate emissions rate = 0.00847³·Cs³·Qstd = (lbs/hr)
MwH₂O = molecular weight of water = 17.98 (g/g³·mole)

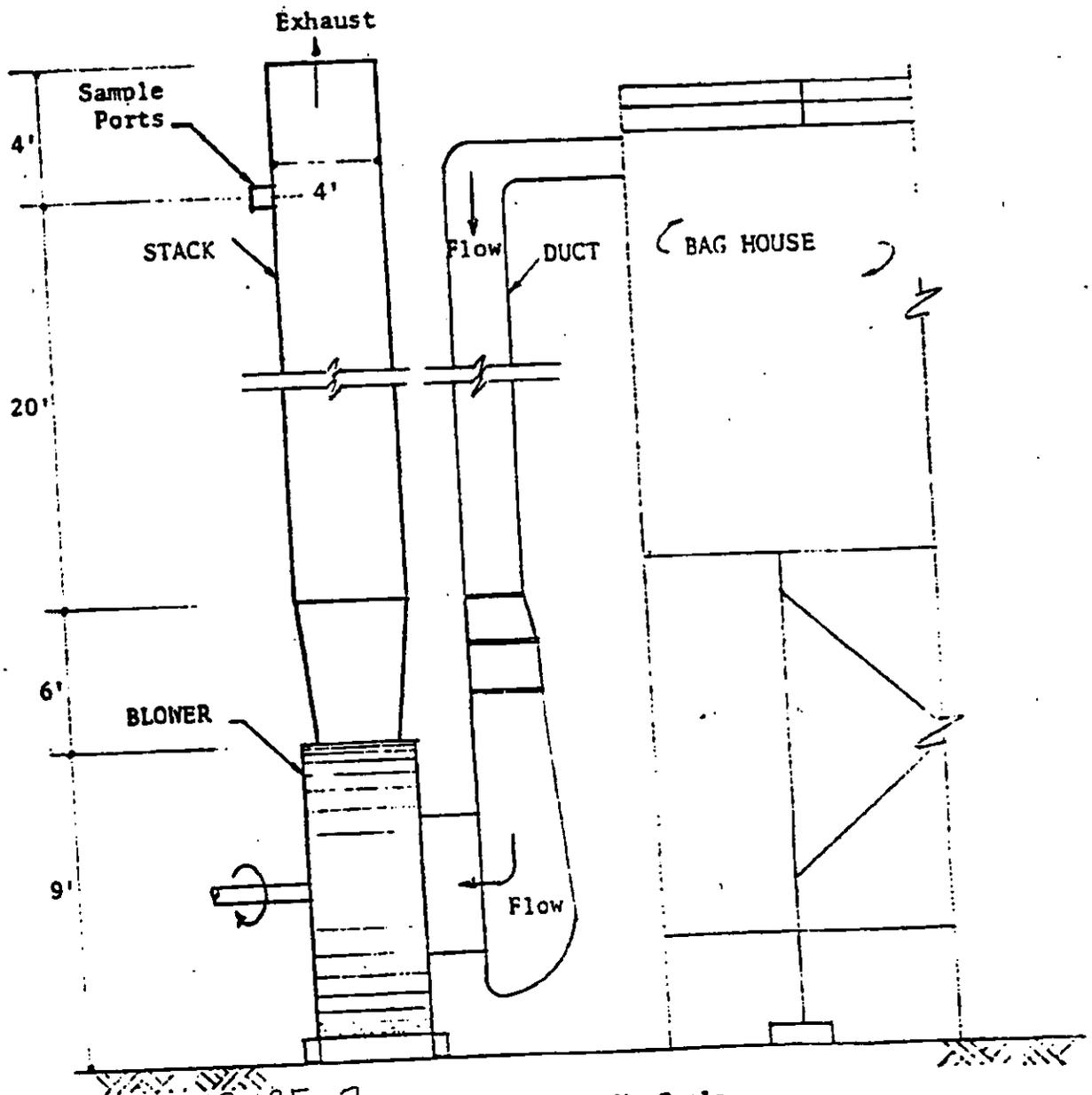
CONSTANTS:

0.00847 lb/(gr³·min/hr) = 1 lb/7000grains³·60 min/hr
13.6 in H₂O/in Hg
17.68 °R/in Hg
60 sec/min
32 g/g³·mole = O₂ molecular weight
44 g/g³·mole = CO₂ molecular weight
28 g/g³·mole = N₂ molecular weight
18 g/g³·mole = H₂O molecular weight
85.49 (ft/sec)³·(lb³·in Hg/(lb³·mole³·°R³·in H₂O))³·.5
0.04707 = ft³/ml
460 (demensionless) = conversion °F to °R
144 in²/ft²
15.43 gr/g
0.002669 in Hg³/((°R³·ml))

SITE DESCRIPTION
HAZARD ASPHALT



Top View



QC DNS.

SITE = _____

TEST # = _____

VOLUMES

(1) IMPINGER VOLUMES

	final	initial	=	Δ
# 1	561.10 g	437.20 g	=	123.90 g
# 2	571.80 g	441.90 g	=	129.90 g
# 3	339.25 g	335.30 g	=	3.95 g
# 4	359.12 g	358.30 g	=	0.82 g

† TOTAL VOLUME LIQUID COLLECTED = 258.57 ml

comments:

The acetone and DI water rinses were kept separate by front and back half.
Blanks were run on both the acetone and DI water solvents.

† The density of water is 1 g/ml

SITE = _____

TEST # = _____

(2) BEAKER RINSES

ACETONE

BKR ID = 174/172

FRONT HALF = 100.00 ml

F.H. RINSES = 30.00 ml

BACK HALF = 200.00 ml

B.H. RINSES = 15.00 ml

SEPARATORY

FUNNEL RINSE = 0.00 ml

WATER

BKR ID = 188&191/218

FRONT HALF = 250.00 ml

F.H. RINSES = 100.00 ml

BACK HALF = 350.00 ml

B.H. RINSES = 84.00 ml

IMPINGERS = 200.00 ml

BKR ID = _____

FRONT HALF = _____ ml

F.H. RINSES = _____ ml

BACK HALF = _____ ml

B.H. RINSES = _____ ml

total acetone = 345.0 ml

total water = 984.0 ml

total Pet Ether = 0.0 ml

* All data and calculations may be found on file at the San Diego County Air Pollution Control District.

SITE = _____

TEST # = _____

(3) CORRECTIONS- (volume used)*(std wt)

ACETONE

WATER

FRONT HALF = 0.00071531 g

FRONT HALF = 0.00081105 g

FRONT HALF = 0.000000 g

BACK HALF = 0.00118301 g

BACK HALF = 0.00100570 g

BACK HALF = 0.000000 g

SEP. FUNNEL = 0.00000000 g

IMPINGERS = 0.00046346 g

tot. front half = 0.001526 g

total back half = 0.002189 g

sep. funnel + impingers = 0.000463 g

total grams = 0.0042 g
from solvents

SITE = _____

TEST # = _____

FRONT HALF

BACK HALF

ACETONE

) BKR ID = 174

BKR ID = 172

f: 29.0641 g

f: 30.4677 g

i: 29.0572 g

i: 30.4632 g

Δ: 0.0069 g

Δ: 0.0045 g

) WATER

BKR ID = 188

BKR ID = 218

BKR ID = 191

f: 28.3783 g

f: 48.5069 g

f: 27.1414 g

i: 28.3418 g

i: 48.4489 g

i: 27.1241 g

Δ: 0.0365 g

Δ: 0.0580 g

Δ: 0.0173 g