

DATE: Jan 14, 1992

File Code: 4530

PRELIMINARY STACK TEST REVIEW

received 12/2/92

By: Joe Perez JWP Test Date: Nov 13, 1991
Name of Source: Kennedy & Sons FID #: 999523470
Address: Townline Rd & HWY 51 Stack #: 01
City: Beloit, WI 53511 Process #: 01
Permit #: 87-POY-037A Date Issued: 1987

Description of Source Tested: Bitum 300 drum mix asphalt plant rated at 300 T/Hr. During test, the plant was using 70% virgin and 30% recycle.

Description of Control Equipment: Venturi scrubber using 420 GPM. ΔP was 19" H₂O

Test Firm: Environmental Technology & Eng., Mil, WI
Crew Chief & Phone#: Mr Bill Dick (414) 784-2434

Pollutant Tested: Particulate Test Method: Method 5
Pollutant Tested: Formaldehyde Test Method: NIOSH 3500
Pollutant Tested: _____ Test Method: _____

~~Test Date: _____~~
Rated Production Level: 300 T/Hr

Discussion of Results:

Poll. Test Ave. - <u>0.041 Gr Part/DSCF</u>	Limit - <u>0.040 Gr Part/DSCF</u>	In Compliance? Y <input checked="" type="radio"/> N
Poll. Test Ave. - <u>0.42 Lb HCOH/Hr</u>	Limit - _____	In Compliance? Y <input type="radio"/> N
Poll. Test Ave. - <u>3,679 Lb HCOH/Yr</u>	Limit - <u>250 Lb/Yr</u>	In Compliance? Y <input type="radio"/> N
Poll. Test Ave. - _____	Limit - _____	In Compliance? Y <input checked="" type="radio"/> N
.....		In Compliance? Y <input type="radio"/> N

Is This a Valid Test? N If answer is no see page 2.

* Test may be reviewed in depth later, if necessary.

CC Joe Perez-AM/10
US EPA Region V
Tom Roushar-SD

PARTICULATE CHECKLIST

Name of Source: Kennedy & Sons Test Date: NOV 13, 1991

1. Are the isokinetics per run between 90 and 110%?
If the XI for a run is outside the range, void the run. See 5. YES NO
 2. Is the sample volume per run ≥ 30 DSCF?
If the sample volume for a run is < 30 DSCF, void the run. See 5. YES NO
 3. Is the sample time per run ≥ 60 min.?
If the sample time for a run is < 60 min., void the run. See 5. YES NO
 4. Is the sample time per sample point \geq two min.?
If the sample time per point for a run is $<$ two min., void the run. See 5. YES NO
 5. A stack test shall consist of three valid runs or, at a minimum, two valid runs if one run is voided. Is this a valid test?
If no, inform the District or the source that the test is unacceptable and should be redone. Your review is over. YES NO
 6. Is the total particulate per run added correctly?
If an incorrect total is found, correct the total and the results or call the consultant and ask for a correction. YES NO
 7. Was the backhalf included in the total particulate? *NSPS source* YES NO
NSPS sources are exempt from including the backhalf. All other sources must include the backhalf. If they don't, the test is invalid. See 5.
-
- Eq. 1 $Gr/DSCF = 15.43 * g \text{ of part./sample volume of run in DSCF}$
- Eq. 2 $Gr/DSCF @ 12\% CO_2 = (Gr/DSCF) * 12 / \text{Stack } CO_2$
- Eq. 3 $Gr/DSCF @ 7\% O_2 = (Gr/DSCF) * (20.9 - 7) / (20.9 - \text{Stack } O_2)$
- Eq. 4 $Lb/DSCF = (Gr/DSCF) / 7000$ Eq. 5 $Lb/MLb_{DRY} = 385.6 * 10^3 * (Lb/DSCF) / MW_{DRY}$
- Eq. 6 $Lb/MLb_{WET} = 385.6 * 10^3 * (Lb/DSCF) * (1 - (\% \text{ Moisture} / 100)) / MW_{WET}$
- Eq. 7 $Lb/Hr = 60 * DSCFM * (Lb/DSCF)$ Eq. 8 $Lb/10^6 \text{ BTU} = (Lb/Hr) / (10^6 \text{ BTU/Hr})$
- Eq. 9 $Lb/10^6 \text{ BTU} = (Lb/DSCF) * F \text{ Factor} * 20.9 / (20.9 - \text{Stack } O_2)$
-
8. If the emission limit is in Gr/DSCF, Lb/DSCF, Lb/MLb, Lb/Hr or Lb/10⁶ BTU, solve Eq. 1-9. Do your results match the consultant's?
If no, fix the problem or call the consultant for a correction. YES NO
 9. Is the three run(or two run) average correct?
If no, write in the correct average. YES NO
 10. Is the average result in compliance?
If no, the District should issue an NOV. YES NO
 11. Was the source operating at a level representative of full capacity? 59.0%
If no, the permit release may need to provide conditions to cap the source at the test level until a stack test at a higher production level(showing compliance) is performed. If the test was not for permit release, other actions may be warranted. YES NO

SUMMARY

On November 13, 1991, Environmental Technology & Engineering Corporation personnel performed a stack emission test on the Wm. J. Kennedy & Son, Inc. ^{8:15 AM} ~~Boeing~~ 300 drum mix asphalt plant located in Janesville, Wisconsin. The average of the three particulate tests show the emissions to be slightly above the limit of 0.04 grains of particulate matter per dry standard cubic foot (gr/dscf) as specified by the State of Wisconsin Department of Natural Resources (DNR) by permit. The numerical test results are summarized below:

Test	Emissions	% of Allowable
1	0.033 gr/dscf	82 %
2	0.046	115
3	0.044	110
	-----	---
AVG	0.041 gr/dscf	102 %

In addition, the permit also required testing for formaldehyde emissions. The following table presents the numerical results:

Test	LB/HR	LB/TON
1	0.48 lb/hr	0.0018 lb/ton
2	0.35	0.0013
3	0.44	0.0016
	-----	-----
AVG	0.42 lb/hr	0.0016 lb/ton

The permit also required that opacity observations be performed concurrently with the particulate test. All individual readings were either 0 % or 5 % and thus the six minute average opacities were all well below the permit limit of 20 %.

1.0 GENERAL

On Wednesday, November 13, 1991, Environmental Technology and Engineering Corporation personnel performed a stack emission test on the Wm.J. Kennedy & Son, Inc. asphalt plant located in Janesville, Wisconsin. The test was a provision of an Air Pollution Control Permit. The State of Wisconsin Department of Natural Resources (DNR) has established a particulate emission limit of 0.04 grains per dry standard cubic foot (gr/dscf). The purpose of this test was to demonstrate the compliance status of this plant with the particulate limits set by the DNR. In addition, the permit also required a test to determine the formaldehyde emissions and that opacity observations be performed by a certified reader.

The plant tested was a ^{B: FUM2} ~~Seeing~~ 300 drum mix plant equipped with a wet scrubber for particulate control. During the test period, the plant production rate was approximately 270 tons per hour and the mix was composed of approximately 70 % virgin material and 30 % recycled material. The plant was fired with natural gas. Dave Barkley of Wm.J. Kennedy was responsible for plant operation during the tests. A copy of the plant production log is included in the APPENDIX to this report. The field tests, corresponding laboratory analysis and report preparation were coordinated by Bill Dick of ETE. The test procedures, plant operating conditions, and stack opacity were witnessed by Tom Roushar of the Wisconsin DNR Southern District Office.

The following sections of this report document the activities and results of the test program. The report presents all of the relevant data collected and discussions on the interpretation of the data are provided where appropriate. The report, therefore, includes much necessary detail. The results, however, have been summarized in the SUMMARY section at the beginning of this report for those readers not wishing to be burdened by the details.

Bitumz
KENNEDY ~~BOEING~~ 300 PLANT

TEST 1

TABLE 2-1

11-13-91

BAROMETRIC PRESSURE, in Hg = 29.150
 TIP DIAMETER, in .2500
 STACK AREA, sq ft = 8.727
 SAMPLING TIME PER POINT, min = 3.00
 NUMBER OF POINTS = 20
 GAS METER VOLUME, acf = 38.71
 WATER COLLECTED, ml = 344.00
 PARTICULATE COLLECTED, grams = 0.0804
 CO₂ = 6.20 O₂ = 11.80 CO = 0.00 N₂ = 82.00

SAMPLING POINT	STACK TEMP deg F	PITOT DEL P inches	ORIFICE METER inches	GAS METER OUTLET T deg F	GAS VELOCITY fps
1	150	0.680	1.45	42	53.62
2	150	0.620	1.32	43	51.20
3	155	0.620	1.32	44	51.41
4	155	0.660	1.42	45	53.05
5	150	0.660	1.42	46	52.83
6	155	0.660	1.42	48	53.05
7	155	0.650	1.30	50	52.64
8	160	0.600	1.20	51	50.78
9	160	0.580	1.16	51	49.93
10	155	0.500	1.00	51	46.17
11	155	0.600	1.20	53	50.58
12	155	0.640	1.28	54	52.24
13	155	0.660	1.32	54	53.05
14	155	0.680	1.36	55	53.84
15	155	0.680	1.36	56	53.84
16	155	0.650	1.30	56	52.64
17	160	0.620	1.24	57	51.62
18	160	0.600	1.20	58	50.78
19	160	0.550	1.10	59	48.62
20	155	0.500	1.00	60	46.17
AVG VALUES	156		1.269	52	51.40

TOTAL GAS WITHDRAWN, scf = 54.32
 DRY GAS WITHDRAWN, scf = 38.13
 WATER VAPOR WITHDRAWN, scf = 16.19
 PERCENT WATER VAPOR = 29.81
 ACTUAL WET FLOW RATE, acfm = 26,915.66
 STANDARD DRY FLOW RATE, scfm = 15,771.08
 , m³/hr = 26,798.21
 PARTICULATE CONCENTRATION, grains/dscf = 0.033
 PARTICULATE EMISSIONS, lb/1000 lb wet gas = 0.049
 PARTICULATE EMISSION RATE, lb/hr = 4.47
 PERCENT OF ISOKINETIC SAMPLING = 103.17

BAROMETRIC PRESSURE, in Hg = 29.150
 TIP DIAMETER, in .2500
 STACK AREA, sq ft = 8.727
 SAMPLING TIME PER POINT, min = 3.00
 NUMBER OF POINTS = 20
 GAS METER VOLUME, acf = 38.45
 WATER COLLECTED, ml = 367.00
 PARTICULATE COLLECTED, grams = 0.1141
 CO₂ = 6.40 O₂ = 11.60 CO = 0.00 N₂ = 82.00

SAMPLING POINT	STACK TEMP deg F	PITOT DEL P inches	ORIFICE METER inches	GAS METER OUTLET T deg F	GAS VELOCITY fps
1	160	0.700	1.40	61	55.01
2	155	0.660	1.32	62	53.20
3	160	0.660	1.32	63	53.42
4	155	0.640	1.28	64	52.39
5	155	0.640	1.28	66	52.39
6	160	0.700	1.40	67	55.01
7	160	0.650	1.30	68	53.01
8	155	0.600	1.20	69	50.73
9	155	0.560	1.12	70	49.01
10	155	0.500	1.00	71	46.31
11	160	0.640	1.28	75	52.60
12	160	0.640	1.28	76	52.60
13	160	0.640	1.28	77	52.60
14	160	0.640	1.28	77	52.60
15	155	0.600	1.20	77	50.73
16	160	0.660	1.32	78	53.42
17	160	0.660	1.32	79	53.42
18	155	0.650	1.30	80	52.80
19	155	0.580	1.16	81	49.87
20	155	0.560	1.12	81	49.01
	155	0.500	1.00	81	46.31
AVG VALUES	157		1.244	72	51.69

TOTAL GAS WITHDRAWN, scf = 55.24
 DRY GAS WITHDRAWN, scf = 37.96
 WATER VAPOR WITHDRAWN, scf = 17.27
 PERCENT WATER VAPOR = 31.27
 ACTUAL WET FLOW RATE, acfm = 27,066.61
 STANDARD DRY FLOW RATE, scfm = 15,484.52
 , m3/hr = 26,311.29
 PARTICULATE CONCENTRATION, grains/dscf = 0.046
 PARTICULATE EMISSIONS, lb/1000 lb wet gas = 0.069
 PARTICULATE EMISSION RATE, lb/hr = 6.30
 PERCENT OF ISOKINETIC SAMPLING = 104.63

BAROMETRIC PRESSURE, in Hg = 29.150
 TIP DIAMETER, in .2500
 STACK AREA, sq ft = 8.727
 SAMPLING TIME PER POINT, min = 3.00
 NUMBER OF POINTS = 20
 GAS METER VOLUME, acf = 37.03
 WATER COLLECTED, ml = 359.00
 PARTICULATE COLLECTED, grams = 0.1051
 CO₂ = 6.20 O₂ = 11.60 CO = 0.00 N₂ = 82.20

SAMPLING POINT	STACK TEMP deg F	PITOT DEL P inches	ORIFICE METER inches	GAS METER OUTLET T deg F	GAS VELOCITY fps
1	160	0.660	1.32	80	53.48
2	160	0.680	1.36	80	54.28
3	155	0.680	1.36	80	54.06
4	160	0.680	1.36	80	54.28
5	160	0.650	1.30	81	53.07
6	155	0.650	1.30	81	52.86
7	155	0.620	1.24	82	51.62
8	160	0.600	1.20	82	50.99
9	155	0.560	1.12	83	49.06
10	155	0.500	1.00	84	46.36
11	160	0.650	1.30	86	53.07
12	160	0.650	1.30	87	53.07
13	160	0.660	1.32	87	53.48
14	155	0.660	1.32	87	53.26
15	155	0.650	1.30	88	52.86
16	155	0.620	1.24	88	51.62
17	155	0.620	1.24	89	51.62
18	160	0.600	1.20	89	50.99
19	160	0.560	1.12	90	49.26
20	155	0.500	1.00	90	46.36
AVG VALUES	158		1.245	85	51.78

TOTAL GAS WITHDRAWN, scf = 53.51
 DRY GAS WITHDRAWN, scf = 36.62
 WATER VAPOR WITHDRAWN, scf = 16.90
 PERCENT WATER VAPOR = 31.58
 ACTUAL WET FLOW RATE, acfm = 27,113.82
 STANDARD DRY FLOW RATE, scfm = 15,436.61
 , m³/hr = 26,229.90
 PARTICULATE CONCENTRATION, grains/dscf = 0.044
 PARTICULATE EMISSIONS, lb/1000 lb wet gas = 0.065
 PARTICULATE EMISSION RATE, lb/hr = 5.90
 PERCENT OF ISOKINETIC SAMPLING = 101.23

KENNEDY & SONS BITUM 300

FORMALDEHYDE CALCULATIONS

$P_0 = 29.15$

$\gamma = 1.023$

TEST 1

270 TPI

$$V_M = 2.00 \quad T_M = 50$$

$$V_{Mstd} = V_M \times \gamma \times \frac{528}{T_M} \times \frac{P_0}{29.92}$$

$$= 2.07 \text{ scf} = .059 \text{ m}^3$$

$$C = \frac{0.475 \text{ mg}}{.059 \text{ m}^3} = 8.05 \text{ mg/m}^3$$

$$ER = 0.48 \text{ \#/hr.} = .0018 \text{ \#/tm}$$

TEST 2

$$V_M = 2.50 \quad T_M = 53$$

$$V_{Mstd} = 2.58 \text{ scf} = .073 \text{ m}^3$$

$$C = \frac{0.440}{.073} = 6.03 \text{ mg/m}^3$$

$$ER = 0.35 \text{ \#/hr.} = .0013 \text{ \#/tm}$$

TEST 3

$$V_M = 1.25 \quad T_M = 54$$

$$V_{Mstd} = 1.29 \text{ scf} = .036 \text{ m}^3$$

$$C = \frac{0.273}{.036} = 7.58 \text{ mg/m}^3$$

$$ER = 0.44 \text{ \#/hr.} = .0016 \text{ \#/tm}$$

SUMMARY

On November 13, 1991, Environmental Technology & Engineering Corporation personnel performed a stack emission test on the Wm. J. Kennedy & Son, Inc. ~~6000~~ 300 drum mix asphalt plant located in Janesville, Wisconsin. The average of the three particulate tests show the emissions to be slightly above the limit of 0.04 grains of particulate matter per dry standard cubic foot (gr/dscf) as specified by the State of Wisconsin Department of Natural Resources (DNR) by permit. The numerical test results are summarized below:

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1	0.033 gr/dscf	82 %
2	0.046	115
3	0.044	110
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AVG	0.041 gr/dscf	102 %

In addition, the permit also required testing for formaldehyde emissions. The following table presents the numerical results:

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The plant tested was a ^{Bitum2} ~~Boeing~~ 300 drum mix plant equipped with a wet scrubber for particulate control. During the test period, the plant production rate was approximately 270 tons per hour and the mix was composed of approximately 70 % virgin material and 30 % recycled material. The plant was fired with natural gas. Dave Barkley of Wm.J. Kennedy was responsible for plant operation during the tests. A copy of the plant production log is included in the APPENDIX to this report. The field tests, corresponding laboratory analysis and report preparation were coordinated by Bill Dick of ETE. The test procedures, plant operating conditions, and stack opacity were witnessed by Tom Roushar of the Wisconsin DNR Southern District Office.

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2.0 RESULTS

2.1 Particulate Emissions

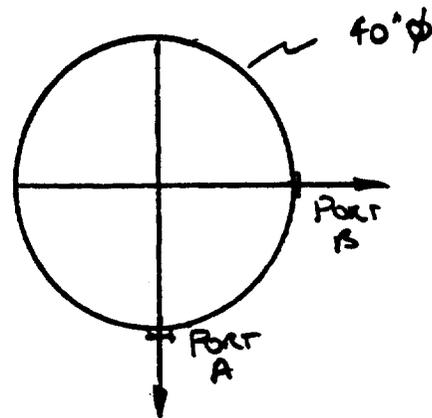
Isokinetic sampling for particulate matter was performed in accordance with the procedures outlined in EPA Method 5 - "Determination of Particulate Emissions from Stationary Sources" - as published in the Federal Register. A brief summary of this method is included in section 3.0 of this report. The tests were performed in the final discharge stack at the location shown in Figure 2-1. This same figure also depicts the location of the exact test points relative to the stack wall. The stack flow parameters recorded during testing and the weights of particulate collected were used to compute the emissions for each test of the three-test sequence. These data were then entered into a computer and printouts showing detailed results are included as Tables 2-1, 2-2, and 2-3.

The results of each of the three individual tests show the emissions to be slightly above the limit of 0.04 grains of particulate matter per dry standard cubic foot (gr/dscf) as specified by the State of Wisconsin Department of Natural Resources (DNR). The numerical test results are summarized below:

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FIGURE 2-1

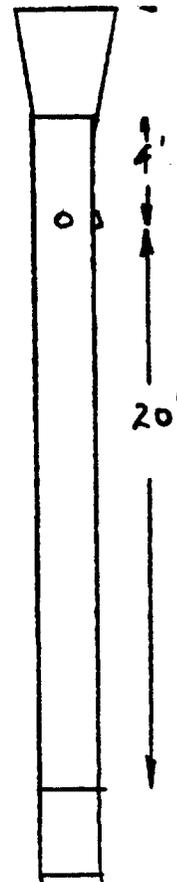
PLANT W^M J KENNEDY
 LOCATION JANESVILLE
 PROCESS BOILING 300 TPH
PLANT
 DIMENSIONS 40" ϕ
 COMMENTS _____



TEST SECTION

POINT	DISTANCE FROM STACK WALL
1	1.0
2	3.3
3	5.8
4	9.0
5	13.7
6	26.3
7	31.0
8	34.2
9	36.7
10	39.0

SAMPLING LOCATION



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4	160	0.680	1.36	80	54.28
5	160	0.650	1.30	81	53.07
6	155	0.650	1.30	81	52.86
7	155	0.620	1.24	82	51.62
8	160	0.680	1.20	82	50.99
9	155	0.560	1.12	83	49.06
10	155	0.500	1.00	84	46.36
11	160	0.650	1.30	86	53.07
12	160	0.650	1.30	87	53.07
13	160	0.660	1.32	87	53.48
14	155	0.660	1.32	87	53.26
15	155	0.650	1.30	88	52.86
16	155	0.620	1.24	88	51.62
17	155	0.620	1.24	89	51.62
18	160	0.600	1.20	89	50.99
19	160	0.560	1.12	90	49.26
20	155	0.500	1.00	90	46.36
AVG VALUES	158		1.245	85	51.78

TOTAL GAS WITHDRAWN, scf = 53.51
 DRY GAS WITHDRAWN, scf = 36.62
 WATER VAPOR WITHDRAWN, scf = 16.90
 PERCENT WATER VAPOR = 31.58
 ACTUAL WET FLOW RATE, acfm = 27,113.82
 STANDARD DRY FLOW RATE, scfm = 15,436.61
 , m³/hr = 26,229.90
 PARTICULATE CONCENTRATION, grains/dscf = 0.044
 PARTICULATE EMISSIONS, lb/1000 lb wet gas = 0.065
 PARTICULATE EMISSION RATE, lb/hr = XXXXXXXXXX
 PERCENT OF ISOKINETIC SAMPLING = 101.23

2.2 Formaldehyde Emissions

The formaldehyde emissions were determined concurrently with the particulate and opacity observations using NIOSH Method 3500. A brief description of the method is included in section 3.0 of this report. The numerical results are presented below:

Test	LB/HR	LB/TON
1	0.48 lb/hr	0.0018 lb/ton
2	0.35	0.0013
3	0.44	0.0016
	-----	-----
AVG	0.42 lb/hr	0.0016 lb/ton

2.3 Visible Emissions (Opacity)

The visible emissions (opacity) was observed for three sixty minute periods which coincided with the particulate emission tests. The opacity was observed in accordance with the procedures outlined in EPA Method 9 -Visible Determination of the Opacity of Emissions from Stationary Sources. All individual opacity readings were either 0 % or 5 % and thus the six minute average opacities were well below the permit limit of 20 %. Copies of the field data observation sheets are included in the APPENDIX to this report.

3.0 METHOD OF TEST

3.1 Particulate Matter

The equipment used to sample was the Western Precipitation Division of the Joy Manufacturing Company Emission Parameter Analyzer. Samples were collected and analyzed in accordance with procedures outlined in 40 CFR 60 Appendix A, Method 5 - Determination of Particulate Emissions from Stationary Sources.

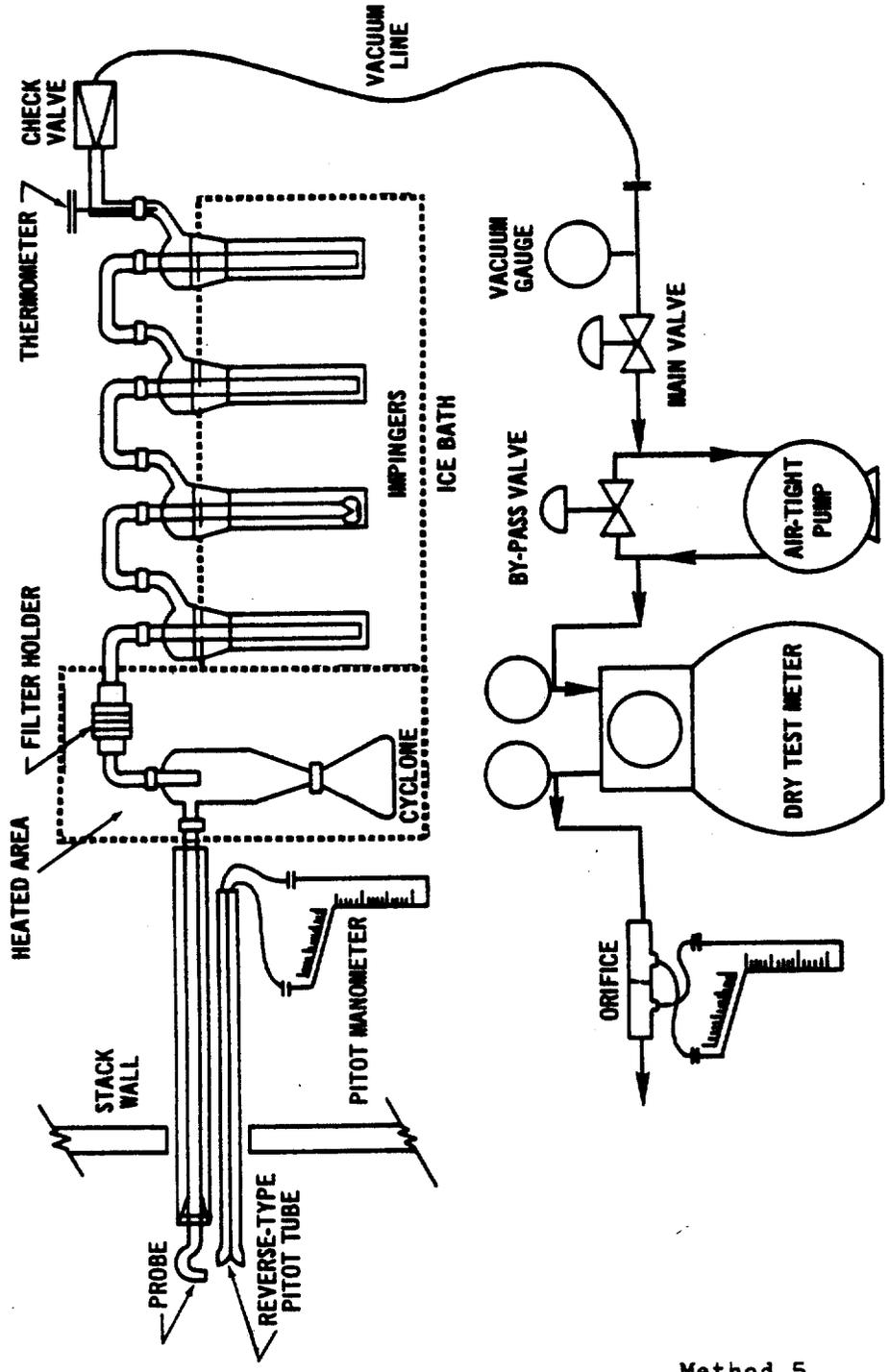
The sampling train consisted of a stainless steel probe tip, a heated stainless steel lined probe, a glass cyclone and flask, and a heated 125 millimeter Whatman 934-AH fiberglass filter. A series of four impingers followed in an ice bath. The first was a modified Greenburg-Smith impinger with 100 ml of distilled water; the second was a Greenburg-Smith impinger with 100 ml water; the third was a modified Greenburg-Smith impinger dry; the fourth was also a modified Greenburg-Smith impinger containing a tared quantity of silica gel. The gas then passed through a vacuum pump, calibrated dry gas meter, and a calibrated orifice. A schematic drawing of the sampling train is included.

The temperatures at strategic locations within the sampling devices, were monitored by RTDs and read directly from a gauge on the control unit.

The initial gas stream velocity was obtained from a preliminary traverse using an "S" type pitot tube. The initial moisture was estimated from previous tests of similar processes. This data, along with the stack temperature, was used to set a nomograph so that rapid calculations of isokinetic sampling conditions could be made.

The principle of the method was to collect the sample representative of the exhaust by adjusting the sample collection velocity to match the exhaust gas stream velocity at the point of collection. The velocity at the point of collection was measured with an "S" type pitot tube attached to the probe and the collection velocity was matched to the stack gas velocity by adjusting the flow as indicated by the calibrated orifice.

To determine the molecular weight of the stack gas, integrated bag samples were collected and analyzed on-site with an Orsat analyzer for percentage CO₂, O₂, CO, and N₂.



Method 5

Particulate sampling train.

At the completion of the test, the probe and glassware preceding the filter were washed with acetone which was placed in a tared beaker and evaporated to dryness at room temperature. The filter and beaker were then desiccated to the tared humidity conditions and weighed. The impinger contents were measured and weighed for determination of the actual moisture content of the exhaust gas stream.

The combined weight of the filter catch and the probe washing residue was used to determine the particulate emission rates. A computer was used to calculate the stack velocities, emission concentrations, emission rates and volumetric flow rates using the field and laboratory data.

3.2 Formaldehyde

The sampling and analysis were performed using procedures outlined in NIOSH Method 3500, the method accepted by the Wisconsin Department of Natural Resources for determining formaldehyde emissions.

Sampling was performed by drawing a known quantity of stack exhaust through appropriate sampling media by means of a battery operated pump. The media consisted of a train of three midget impingers; the first two each contained 15 milliliters of a one percent sodium bisulfite solution and the third was dry to serve as a water trap. The impingers were set in an ice water bath to accommodate the temperature of the gas stream sampled. The sampling volumes were determined through the use of a calibrated dry gas meter.

Following the sampling, the samples were sealed and brought back to the lab for analysis. The samples were analyzed via colorimetric methods as described in the NIOSH procedures. Each impinger was analyzed separately to insure the complete absorption of all formaldehyde in the solution.

4.0 CALIBRATIONS

The probe tip, pitot tube, dry gas meter, and orifice were calibrated prior to the test according to procedures outlined in the Maintenance, Calibration, and Operation of Isokinetic Source-Sampling Equipment as published by the EPA. The values obtained were:

Probe tip diameter	d = 0.250"
Pitot tube coeff.	Cp = 0.85
Orifice coeff.	dHo = 1.779

The dry gas meter presently installed in the control box is a temperature compensating meter. The correction factor for this dry gas meter is represented by:

$$\text{Gama} = 1.010 + (T_d - 70) \times .00012$$

where: Td = Dry Gas Meter Temperature

The most recent calibration was performed October 9, 1991.

APPENDIX A

FIELD & LABORATORY DATA SHEETS

155
* AUGUST 27, 1973, U → 78

cp = 0.85
R 1.010 } 10-9-91
METER AN, 1.779

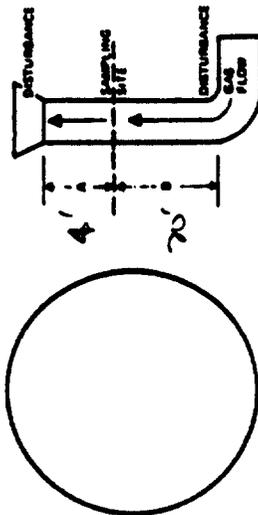
PARTICULATE FIELD DATA

PLANT KENNEDY
 DATE 11-13-91
 LOCATION JANESVILLE
 OPERATOR WJD
 STACK NO. 1
 RUN NO. 1
 SAMPLE BOX NO. 1
 METER BOX NO. 1

AMBIENT TEMPERATURE 40
 BAROMETRIC PRESSURE 29.15
 ASSUMED MOISTURE, % SAI (-25%)
 PROBE LENGTH, in. 52"
 NOZZLE DIAMETER, in. 1/4
 STACK DIAMETER, in. 48
 PROBE HEATER SETTING 250
 HEATER BOX SETTING 250

PROCESS WEIGHT RATE 2600 270 TPA
 ORSAT RESULTS
 CO2 6.2
 CO 11.8
 N2 82.0
 FACE LK ON
 PITOT LK ON
 POST LK ON

SCHEMATIC OF STACK

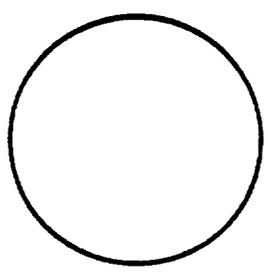
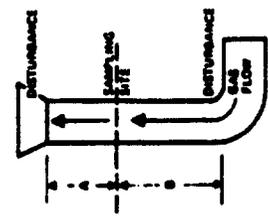


CROSS SECTION

TRAVERSE POINT NUMBER	SAMPLING TIME (hr), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (V _p) (ft/s)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔP) (in. H ₂ O)	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F	HClO ₄ SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING OR CONDENSER OR LAST IMPINGER °F	PUMP VACUUA in. Hg gauge	VELOCITY f/s
A 1	05:00		150	.68	1.45	9408.00		42	746.26/48			
2	05		150	.62	1.32	10.1		43	743.26/52			
3	05	-.40	155	.62	1.32	12.1		44				
4	05		155	.66	1.42	14.1		45	2.04/50			
5	05		150	.66	1.42	16.2		46				
6	05	-.50	155	.66	1.42	18.3		48				
7	05		155	.65	1.30	20.3		50				
8	05		160	.60	1.20	22.3		51				
9	05	-.50	160	.58	1.16	24.2		51				
10	05		155	.50	1.00	26.0 (0.50)		51				
B 11	05:15		155	.60	1.20	27.1/28.21		53				
12	05		155	.64	1.28	30.1		54				
13	05	-.50	158	.66	1.32	32.0		54				
14	05		155	.68	1.36	34.0		55				
15	05		155	.68	1.36	36.0		56				
16	05	-.50	155	.65	1.30	38.0		56				
17	05		160	.62	1.24	39.1		57				
18	05		160	.69	1.20	41.8		58				
19	05	-.40	160	.55	1.10	43.7		59				
20	12		155	.50	1.00	45.5		60				
	05:55					9497.21						
						38.71						

PARTICULATE FIELD DATA

PLANT KENNEDY AMBIENT TEMPERATURE 95 METER A.M. _____
 DATE 11-13-91 BAROMETRIC PRESSURE _____ C FACTOR _____
 LOCATION JACKSONVILLE ASSUMED MOISTURE, % 5% PROCESS WEIGHT RATE _____
 OPERATOR WJD PROBE LENGTH, in. 80" ORSAT RESULTS
 STACK NO. 1 NOZZLE DIAMETER, in. 1/4 CO2 6.4
 RUN NO. 2 STACK DIAMETER, in. 40 CO 11.6
 SAMPLE BOX NO. 2 PROBE HEATER SETTING 250 N2 820
 METER BOX NO. 1 HEATER BOX SETTING 250 *see below*

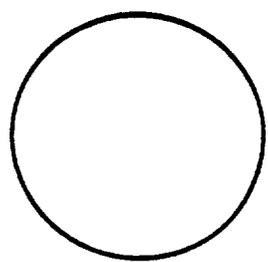
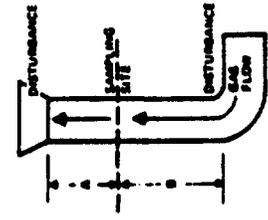


CROSS SECTION

TRAVERSE POINT NUMBER	SAMPLING TIME (n), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (V _s) (ft/s)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (in. H ₂ O)	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		HCON	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER (°F)	PUMP VACUUM in. Hg gauge	VELOCITY fps
							INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F				
A1	101500		160	.70	1.40	9451.00			740.24/53			
2	11	-.50	155	.66	1.32	53.0			750.76/51			
3	11		160	.66	1.32	55.0						
4	24		155	.64	1.28	56.9						
5	30		155	.64	1.28	58.8						
6	30		160	.70	1.40	60.8						
7	35		160	.65	1.30	62.8						
8	35		155	.60	1.20	64.7						
9	35		155	.56	1.12	66.5						
10	35		155	.50	1.00	68.3 (0.31)						
B11	55/51		160	.64	1.28	70.60/70.50						
12	50		160	.64	1.28	72.4						
13	51		160	.64	1.28	74.3						
14	50	-.50	155	.60	1.20	76.2						
15	52		160	.66	1.32	78.0						
16	50		160	.66	1.32	79.9						
17	51		155	.65	1.30	81.8						
18	12		155	.58	1.16	83.7						
19	15		155	.50	1.12	85.5						
20	18		155	.50	1.00	87.2						
	1121					9488.95						
						(38.43)						

PARTICULATE FIELD DATA

PLANT KEENEY AMBIENT TEMPERATURE 50 METER Δ H. _____
 DATE 11-13-91 BAROMETRIC PRESSURE _____ C FACTOR _____
 LOCATION JANESVILLE ASSUMED MOISTURE, % SAT. PROCESS WEIGHT RATE _____
 OPERATOR WJD PROBE LENGTH, in. 52 ORSAT RESULTS
 STACK NO. 1 NOZZLE DIAMETER, in. 1/4 CO 02.6
 RUN NO. 3 STACK DIAMETER, in. 40 CO 02.11.6
 SAMPLE BOX NO. 3 PROBE HEATER SETTING 750 N₂ 02.2
 METER BOX NO. 1 HEATER BOX SETTING 750 PRE LK ON
 P.T. ST LK ON
 POST LK ON



CROSS SECTION

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (V _p), (ft/s)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (in. H ₂ O)	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUA in. Hg gauge	VELOCITY fps
							INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F				
A 1	114400		160	.60	1.32	990.00		80				
2	47		160	.68	1.36	919		80				
3	53	-0.5	155	.68	1.34	93.9		80				
4	55		160	.68	1.36	95.8		80				
5	56		160	.65	1.30	97.7		81				
6	59		155	.65	1.30	99.6		81				
7	02		155	.62	1.24	01.5		82	753.42	51		
8	05		160	.62	1.20	03.2		82	754.62	51		
9	07		155	.59	1.12	05.1		83	1.75			
10	08		155	.60	1.00	05.9	(-0.50)	84				
B 11	14/19		160	.65	1.30	08.58	09.08	86				
12	27		160	.65	1.30	10.9		87				
13	25	-0.50	160	.66	1.32	12.8		87				
14	28		155	.66	1.52	14.7		87				
15	31		155	.65	1.30	16.7		88				
16	30		155	.62	1.24	18.6		88				
17	31		155	.62	1.24	20.5		89				
18	06		160	.60	1.20	22.3		89				
19	05		160	.56	1.12	28.2		90				
20	06		155	.50	1.00	25.9		90				
	124600					237.53						
						(37.03)						

← (1) B320 H₂O TEMPE 152 °F

LABORATORY DATA SHEET
PARTICULATE & WATER COLLECTED

JOB NAME Kennedy Asphalt - Jonesville
JOB NO. _____

DATE OF TEST 11-13-91
TEST ENGINEER WJD

RUN NO. 1 STACK Scrubber

Sample Box 1 Filter 1492 Wash Bottle —
Beaker No. 7

WATER COLLECTED

<u>Impinger No.</u>	<u>Final Wt. g</u>	<u>Initial Wt. g</u>	<u>Collected grams</u>
<u>1</u>	<u>233</u>	<u>100</u>	<u>133</u>
<u>2</u>	<u>192</u>	<u>100</u>	<u>92</u>
<u>3</u>	<u>89</u>	<u>0</u>	<u>89</u>
<u>SILGEL</u>	<u>731</u>	<u>701</u>	<u>30</u>
		TOTAL	<u><u>344</u></u>

PARTICULATE COLLECTED

	<u>Final Wt. g</u>	<u>Tare Wt. g</u>	<u>Collected grams</u>
Filter	<u>0.8226</u>	<u>0.7910</u>	<u>0.0316</u>
Washings (.000g)	<u>93.9404</u>	<u>93.8907</u>	<u>0.0488</u>
		TOTAL	<u><u>0.0804</u></u>

WATER COLLECTED 344 GRAMS

PARTICULATE COLLECTED 0.0804 GRAMS

NOTES:

Technology & Engineering Corp.

Name of Company: **KENNEDY**
 Date: **11-13-91**
 Location: **PEB Number**
 City, State, Zip Code: **BELoit, WISC**
 Observer Certification Date: **OCT 1991**
 Discharge Location: **SCRUBBER - FINAL EXHAUST**
 Control Device: **WET SCRUBBER**
 Height of Discharge Above Ground: **~ 35 FT**
 Steam Plume? Attached Detached
 Time of Observation: Initial **8:40:00** Final **9:40**
 Observer Location: Distance to Discharge **500'** Direction from Discharge **NE**
 Height of Observation Point in Relation to Discharge: **-30 FT**
 Plume Description (Color, Length, etc.): **WHITE, 500'**
 Plume Background Description: **BLUE SKY**
 Weather Conditions: Wind Direction **SOUTH** Wind Speed **0-5** Ambient Temperature **40 F**
 Sky Conditions (clear, overcast, % clouds, etc.): **CLEAR, 10% WISPY CLOUDS**

SEC MIN	0	15	30	45	SEC MIN	0	15	30	45
0	-	-	-	S	36	-	S	S	-
1	-	S	-	S	31	S	-	-	-
2	-	-	S	-	32	-	S	-	-
3	S	S	-	-	33	S	-	-	-
4	-	S	S	-	34	-	-	S	-
5	-	-	S	S	35	-	S	S	S
6	-	S	S	-	36	-	-	S	S
7	S	-	-	S	37	S	-	-	S
8	-	S	-	S	38	-	S	-	-
9	S	-	S	-	39	S	-	-	S
10	S	S	S	-	40	S	-	S	-
11	-	S	-	S	41	-	-	-	S
12	S	-	S	-	42	-	S	-	-
13	-	S	-	S	43	S	-	S	-
14	S	S	-	-	44	-	S	-	S
15	S	-	S	-	45	-	S	S	-
16	-	S	S	-	46	S	-	S	S
17	-	S	-	S	47	10	S	-	S
18	S	-	S	S	48	-	S	-	-
19	-	S	-	S	49	S	-	S	-
20	-	-	-	S	50	-	S	-	-
21	S	-	S	-	51	S	-	S	-
22	-	S	-	S	52	-	-	S	-
23	S	-	S	-	53	S	S	-	S
24	-	S	-	-	54	-	-	-	-
25	S	-	-	S	55	S	S	-	S
26	-	S	S	S	56	-	-	S	-
27	S	-	-	S	57	S	S	-	-
28	-	-	-	-	58	-	S	S	-
29	S	-	S	-	59	S	S	-	-

Describe Point in Plume at Which Opacity was Determined: **END OF STEAM DISSIPATION**

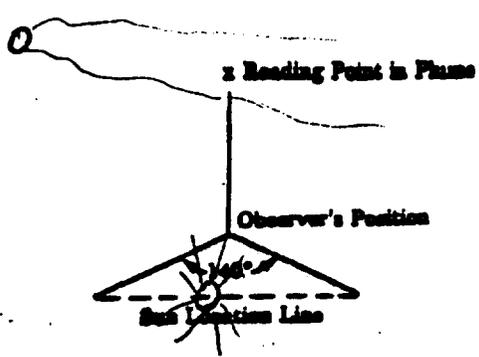
Remarks:

Summary of Average Opacity (From Computer Program)

Set Number	Time	Opacity	
	Start - End	Sum	Average
1		50	
2		65	
3		60	
4		60	
5		50	
6		45	
7		50	
8		70	
9		50	
10		50	

Signature of Observer: *[Signature]* Name of Observer (Please print): **MICHAEL HUENINK**

Sketch of Observer, Discharge, and Sun Location.



Allowable Source Opacity

Technology & Engineering Corp.

Name of Company: **KENNEDY** Date: **11-13-91**

Location: **BELOIT** FID. Number: _____

City, State, Zip Code: **BELOIT** Observer Certification Date: **OCT 1991**

Discharge Location: **ASPHALT PLANT - FINAL DISCHARGE** Control Device: **NET SCRUBBER**

Height of Discharge Above Ground: **~ 35 FT** Steam Plume? Attached Detached

Time of Observation: Initial **10:15:00** Final **11:15:00**

Observer Location: Distance to Discharge: **~ 450'** Direction from Discharge: **ENE**

Height of Observation Point in Relation to Discharge: **-30 FT**

Plume Description (Color, Length, etc.): **WHITE, 450 FT**

Plume Background Description: **SKY (BLUE)**

Weather Conditions: Wind Direction: **S** Wind Speed: **0-5** Ambient Temperature: **45**

Sky Conditions (clear, overcast, % clouds, etc.): **CLEAR, 10% CLOUDS**

SEC MIN	0	15	30	45	SEC MIN	0	15	30	45
0	-	5	5	-	30	5	-	5	-
1	-	-	5	-	31	-	5	-	5
2	5	-	-	5	32	-	-	5	5
3	-	-	-	-	33	-	5	-	5
4	-	5	-	-	34	5	-	5	-
5	-	-	5	-	35	-	5	5	-
6	5	-	-	-	36	5	-	-	-
7	-	-	-	5	37	-	5	-	-
8	-	-	5	-	38	-	-	5	-
9	-	5	-	5	39	-	5	-	-
10	5	-	-	-	40	5	-	-	5
11	-	-	5	-	41	-	-	5	-
12	-	5	-	-	42	-	5	-	-
13	-	-	5	-	43	-	-	5	-
14	5	5	-	-	44	-	-	-	-
15	-	-	-	5	45	5	-	-	-
16	-	5	-	-	46	-	5	-	-
17	5	-	5	-	47	5	-	-	5
18	-	5	-	-	48	-	5	-	-
19	5	-	-	-	49	5	-	-	-
20	-	5	-	-	50	-	-	-	-
21	-	5	-	-	51	-	-	5	5
22	5	-	5	5	52	-	5	-	-
23	5	-	-	5	53	-	-	-	5
24	5	-	5	5	54	-	-	-	5
25	-	5	5	-	55	-	5	-	-
26	5	-	5	5	56	5	-	-	5
27	-	5	-	-	57	-	-	-	-
28	5	-	5	5	58	5	-	5	-
29	-	5	-	5	59	-	-	-	-

Describe Point in Plume at Which Opacity was Determined: **END OF STEAM DISSIPATION!**

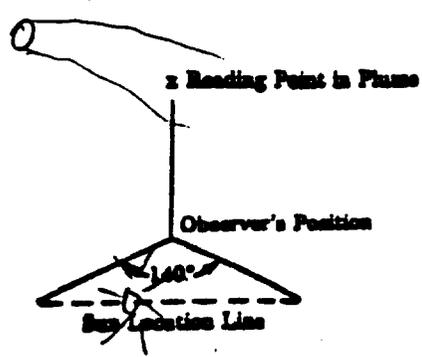
Remarks: _____

Summary of Average Opacity (From Computer Program)

Set Number	Time	Opacity	
	Start - End	Sum	Average
1		35	
2		35	
3		40	
4		45	
5		70	
6		60	
7		35	
8		30	
9		30	
10		30	

Signature of Observer: *[Signature]* Name of Observer (Please print): **MICHAEL HUENINK**

Sketch of Observer, Discharge, and Sun Location.



Allowable Source Opacity

Technology & Engineering Corp.

Name of Company: **KENNEDY + SON** Date: **11-13-91**

Located: [] PID Number: []

City, State, Zip Code: **BLOOM, WISC** Observer Certification Date: **OCT 1991**

Discharge Location: **ASPHALT PLANT SCRUBBER STACK** Control Device: **WET SCRUBBER**

Height of Discharge Above Ground: **~ 35 FT** Steam Plume? Attached Detached

Time of Observation: Initial **11:45:00** Final **12:45**

Observer Location: Distance to Discharge: **250 FT** Direction from Discharge: **EAST** Height of Observation Point in Relation to Discharge: **-30 FT**

Plume Description (Color, Length, etc.): **WHITE, 300 FT**

Plume Background Description: **BLUE SKY**

Weather Conditions: Wind Direction: **SOUTH** Wind Speed: **0-5 MPH** Ambient Temperature: **45**

Sky Conditions (clear, overcast, % clouds, etc.): **CLEAR, 10% CLOUDS**

SEC MIN	0	15	30	45	SEC MIN	0	15	30	45
0	-	-	-	-	30	-	-	-	5
1	-	5	-	5	31	-	-	-	-
2	-	-	5	-	32	-	-	5	-
3	5	-	-	-	33	5	-	-	-
4	-	-	-	-	34	-	-	-	-
5	-	5	-	-	35	-	-	-	5
6	-	-	-	5	36	-	-	-	-
7	-	-	-	-	37	-	5	-	-
8	5	-	-	-	38	-	-	-	-
9	-	-	5	-	39	5	-	-	-
10	-	5	-	-	40	-	-	5	-
11	5	-	-	5	41	-	-	-	-
12	-	-	-	-	42	-	-	-	5
13	-	-	-	5	43	5	-	-	-
14	-	-	5	-	44	-	-	-	-
15	-	-	-	5	45	-	5	-	-
16	-	-	5	-	46	-	-	-	-
17	-	-	-	-	47	5	-	-	-
18	5	-	5	-	48	-	-	-	-
19	-	-	5	-	49	-	-	5	-
20	-	-	-	-	50	-	-	-	-
21	-	-	-	-	51	-	-	-	-
22	-	5	-	-	52	-	-	-	-
23	-	-	-	-	53	5	-	-	-
24	-	-	-	5	54	-	-	-	-
25	-	-	-	-	55	-	-	-	-
26	5	-	-	-	56	5	-	-	-
27	-	5	-	-	57	-	-	5	-
28	-	-	-	-	58	-	-	-	-
29	5	-	-	-	59	-	-	5	-

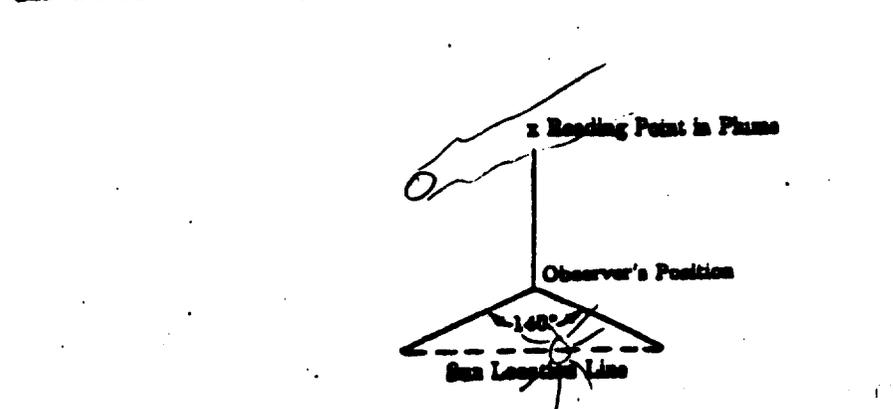
Describe Point in Plume at Which Opacity was Determined: **END OF STEAM DISSIPATION**

Remarks: []

Summary of Average Opacity (From Computer Program)

Sec Number	Time		Opacity	
	Start	End	Sum	Average
1			25	
2			30	
3			20	
4			20	
5			20	
6			20	
7			15	
8			20	
9			10	
10			15	

Signature of Observer: *Michael J. Huenink* Name of Observer (Please print): **MICHAEL HUENINK**



Allowable Source Opacity

Wm J. KENNEDY and SON, Inc.

P.O. Box 813
Janesville, Wisconsin 53547
(608) 752-8944
FAX (608) 365-8146

November 15, 1991

Mr. Bill Dick
Environmental Technology &
Engineering Corp.
13020 West Bluemound Rd.
Elm Grove, WI 53122

Dear Bill:

Enclosed is a copy of the production log taken during the stack test performed on Wednesday, November 13th. If you have any questions or need additional information, please contact me.

Sincerely,

WM. J. KENNEDY AND SON, INC.

Dave Barkley
cmh

Dave Barkley
Plant Superintendent

DB:cmh



RATE dTPH	180	80	10.7	65	0	13	105	75
TOTAL TON	703.5	321.0	43.4	262	+	53	418	312
BLEND %	69.3	30.7	4.0	24.9	0.0	5.1	40.0	30.0
No of ERRs	0	0	0	0	0	0	0	0
MIX # 19	225 TPH	268 F	5.3 %mAC	[298 F	8.58 lb/gal	4.0 %rAC]	11/13/91	11:30
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	106	47	6.6	38	0	8	61	45
TOTAL TON	739.4	337.4	45.7	275	+	56	439	328
BLEND %	69.0	31.0	4.2	24.9	0.0	5.1	40.2	29.8
No of ERRs	10	7	3	0	0	0	0	0
MIX # 19	198 TPH	296 F	5.3 %mAC	[299 F	8.58 lb/gal	4.0 %rAC]	11/13/91	11:45
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	180	79	11.2	66	0	14	106	78
TOTAL TON	773.7	352.2	47.8	288	+	58	460	343
BLEND %	69.5	30.5	4.2	24.9	0.0	5.2	40.3	29.7
No of ERRs	8	15	3	0	0	0	0	0
MIX # 19	267 TPH	276 F	5.3 %mAC	[300 F	8.58 lb/gal	4.0 %rAC]	11/13/91	12:00
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	174	77	10.9	66	0	13	105	78
TOTAL TON	818.0	371.8	50.5	305	+	62	486	363
BLEND %	69.3	30.7	4.1	25.1	0.0	5.0	40.0	29.9
No of ERRs	0	0	0	0	0	0	0	0
MIX # 19	267 TPH	245 F	5.3 %mAC	[300 F	8.58 lb/gal	4.0 %rAC]	11/13/91	12:15
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	176	75	11.3	65	0	13	103	77
TOTAL TON	862.3	391.5	53.3	321	+	65	512	382
BLEND %	70.0	30.0	4.3	25.1	0.0	5.0	39.9	30.0
No of ERRs	0	0	0	0	0	0	0	0
MIX # 19	264 TPH	241 F	5.3 %mAC	[300 F	8.58 lb/gal	4.0 %rAC]	11/13/91	12:30
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	178	78	11.1	64	0	13	103	77
TOTAL TON	906.3	410.9	56.0	337	+	68	538	402
BLEND %	69.4	30.6	4.2	24.9	0.0	5.0	40.1	29.9
No of ERRs	0	0	0	0	0	0	0	0
MIX # 19	265 TPH	248 F	5.3 %mAC	[300 F	8.58 lb/gal	4.0 %rAC]	11/13/91	12:45
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	177	77	10.9	64	0	13	103	77
TOTAL TON	950.3	430.5	56.7	353	+	71	564	421
BLEND %	69.6	30.4	4.2	25.0	0.0	5.1	40.0	29.9
No of ERRs	0	0	0	0	0	0	0	0
MIX # 19	225 TPH	266 F	5.3 %mAC	[300 F	8.58 lb/gal	4.0 %rAC]	11/13/91	13:00
	VScale	RScale	+AC	1 Vir	2 Vir	3 Vir	4 Vir	5 Rap
MOISTURE %	3.8	3.5		3.5	4.0	3.0	4.0	3.5
RATE dTPH	116	49	6.6	43	0	9	68	51
TOTAL TON	986.6	446.7	61.0	366	+	74	585	437
BLEND %	70.4	29.6	4.0	25.0	0.0	5.1	39.8	30.0
No of ERRs	7	8	3	0	0	0	0	0

APPENDIX B

SAMPLE CALCULATIONS

SAMPLE CALCULATION

BAROMETRIC PRESSURE, in Hg (Pb) = 29.200
 STACK PRESSURE, in Hg (Pb + Pg/13.6) = 29.178
 TIP DIAMETER, in (An = PI*D^2/576) = .2450
 STACK AREA, sq ft (A) = 10.560
 SAMPLING TIME PER POINT, min = 2.50
 NUMBER OF POINTS = 24
 GAS METER VOLUME, acf (Vm) = 66.06
 WATER COLLECTED, ml (Vf - Vi) = 86.00
 PARTICULATE COLLECTED, grams (Mn) = 0.0755
 CO2 = 0.60 O2 = 21.00 CO = 0.00 N2 = 78.40
 WET MOLECULAR WEIGHT, lb/mole (Ms) = 28.45

SAMPLING POINT	STACK TEMP deg F	PITOT DEL P inches	ORIFICE DEL H inches	GAS METER OUTLET T deg F	GAS VELOCITY fps
1	110	1.450	4.05	32	72.51
2	110	1.350	3.75	32	69.97
3	110	1.350	3.75	32	69.97
4	110	1.300	3.70	32	68.66
5	110	1.250	3.60	32	67.33
6	110	1.250	3.60	32	67.33
7	110	1.050	2.95	32	61.71
8	110	1.000	2.85	32	60.22
9	110	1.000	2.85	34	60.22
10	110	1.050	2.95	34	61.71
11	110	0.950	2.75	38	58.69
12	115	0.950	2.75	38	58.95
13	115	1.300	3.70	42	68.96
14	115	1.250	3.60	42	67.62
15	115	1.200	3.40	42	66.26
16	115	1.200	3.40	42	66.26
17	115	1.150	3.30	44	64.86
18	115	1.150	3.30	46	64.86
19	115	1.050	2.95	48	61.98
20	115	1.150	3.30	48	64.86
21	115	1.000	2.85	50	60.48
22	115	1.100	3.15	50	63.43
23	115	1.050	2.95	50	61.98
24	115	0.900	2.55	50	57.38
AVG VALUES	113		3.250	40	64.42

TOTAL GAS WITHDRAWN, scf = 69.39
 DRY GAS WITHDRAWN, scf (Vmstd) = 65.35
 WATER VAPOR WITHDRAWN, scf (Vwstd) = 4.05
 PERCENT WATER VAPOR (%H2O) = 5.83
 ACTUAL WET FLOW RATE, acfm = 40,819.39
 STANDARD DRY FLOW RATE, scfm (Qs) = 34,558.69
 PARTICULATE CONCENTRATION, grains/dscf (Cs) = 0.018
 PARTICULATE EMISSION RATE, lb/hr (ER) = 5.325
 PARTICULATE EMISSIONS, lb/1000 lb (EC) = 0.033
 PERCENT OF ISOKINETIC SAMPLING (I) = 101.67

SAMPLE CALCULATIONS

1. DRY MOLECULAR WEIGHT (Md) lb/lb-mole

$$Md = .44*\% \text{ CO}_2 + .32*\% \text{ O}_2 + .282*\% \text{ N}_2 + .28*\% \text{ CO}$$

2. WATER VAPOR PERCENT (%H₂O)

$$V_w \text{ std} = 0.04707*(V_f - V_i)$$

where: $V_w \text{ std}$ = standard cubic feet of water vapor
 V_f = Final volume of impingers, ml
 V_i = Initial volume of impingers, ml

$$\% \text{ H}_2\text{O} = V_w \text{ std} * 100 / (V_m \text{ std} + V_w \text{ std})$$

where $V_m \text{ std}$ = standard cubic feet of gas sampled

3. WET MOLECULAR WEIGHT (Ms) lb/lb-mole

$$Ms = Md*(1 - \% \text{ H}_2\text{O}/100) + 18*\% \text{ H}_2\text{O}/100$$

4. STACK PRESSURE (Ps) in. Hg

$$Ps = Pb + Pg/13.6$$

where: Pb = barometric pressure (uncorrected), in. Hg
 Pg = stack gauge pressure, in. H₂O
13.6 = specific gravity of mercury (Hg)

5. AVERAGE STACK VELOCITY (Vs) feet per second

$$Vs = Kp * Cp * (\text{DELP}) \quad Ts_{\text{avg}} / (Ps * Ms)$$

where: Kp = 85.49 unit conversion
 Cp = 0.85, pitot tube calibration factor
 DELP = square root of velocity head, in. H₂O
 Ts_{avg} = average stack temperature, deg R (460+F)
 Ps = stack pressure
 Ms = wet molecular weight

6. STACK GAS FLOW RATE (Qs) std cubic feet per minute

$$Qs = 60*(1 - \% \text{ H}_2\text{O}/100)*Vs*A*(528*Ps/Ts_{\text{avg}}/29.92)$$

where: A = stack area, ft²
528 = std temperature, deg R
29.92 = std pressure, in. Hg

7. DRY GAS VOLUME (V_m std) std cubic feet

$$V_m \text{ std} = GAMA * (V_m - (AL - .02)t) * (P_b + DELH/13.6) / 29.92$$

where: GAMA = dry gas meter calibration factor
 V_m = volume of dry gas metered, cubic feet
AL = post test leak rate, cubic feet per minute
t = total time of test, minutes
DELH = average orifice pressure drop, in.H₂O

8. PARTICULATE CONCENTRATION (C_s) grains/dry std cubic foot

$$C_s = M_n * 15.43 / V_m \text{ std}$$

where: M_n = particulate captured, grams
15.43 = grains per gram

9. EMISSION RATE (ER) pounds per hour

$$PMRA = M_n * A * 60 / (t * A_n * 453.6) \quad \text{AREA METHOD lb/hr}$$

$$PMRC = C_s * Q_s * 60 / (15.43 * 453.6) \quad \text{CONC. METHOD lb/hr}$$

$$ER = (PMRA + PMRC) / 2$$

where: A_n = area of sampling nozzle, square feet

10. EMISSION CONCENTRATION (EC) lb/1000 lb exhaust gas

$$EC = ER * 386700 * (1 - \%H_2O/100) / (Q_s * 60 * M_s)$$

where: 386700 = cubic feet per lb mole * 1000

11. ISOKINETIC SAMPLING PERCENTAGE (I) %

$$I = PMRA / PMRC$$

KENNEDY & SONS

FORMALDEHYDE CALCULATIONS

$P_0 = 29.15$

$\gamma = 1.023$

TEST 1

270 TPI

$$V_M = 2.00 \quad T_M = 50$$

$$V_{Mstd} = V_M \times \gamma \times \frac{503}{T_M} \times \frac{P_0}{29.92}$$

$$= 2.07 \text{ scf} = .059 \text{ m}^3$$

$$C = \frac{0.475 \text{ mg}}{.059 \text{ m}^3} = 8.05 \text{ mg/m}^3$$

$$ER = 0.48 \text{ \#/hr.} = .0018 \text{ \#/tm}$$

TEST 2

$$V_M = 2.50 \quad T_M = 53$$

$$V_{Mstd} = 2.58 \text{ scf} = .073 \text{ m}^3$$

$$C = \frac{0.440}{.073} = 6.03 \text{ mg/m}^3$$

$$ER = 0.35 \text{ \#/hr} = .0013 \text{ \#/tm}$$

TEST 3

$$V_M = 1.25 \quad T_M = 54$$

$$V_{Mstd} = 1.29 \text{ scf} = .036 \text{ m}^3$$

$$C = \frac{0.273}{.036} = 7.58 \text{ mg/m}^3$$

$$ER = 0.44 \text{ \#/hr} = .0016 \text{ \#/tm}$$