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UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

SYNTHETIC FIBERS

AP-42 Section 5.19

Reference Number

31

DATE: 9/20/81 1981

SUBJECT: Trip Report - Plant Visit to Globe Manufacturing Company

FROM: Dennis Crumpler *Dennis W. Crumpler*  
Chemical Applications Section, CPB (MD-13)

TO: James Berry, Chief  
Chemical Applications Section, CPB (MD-13)

I. Purpose

To observe the VOC emission control system for reaction-spun urethane fiber and to discuss the technical and economic problems of operating such a system.

II. Place and Date

Globe Manufacturing Company  
Gastonia, N.C.  
September 16-17, 1981

III. Attendees

Dennis Crumpler, EPA  
Gene Smith, EPA  
Fred Keener, Globe Manufacturing Company  
Richard Legendre, Globe Manufacturing Company

IV. Discussion

Globe Manufacturing Company (henceforth referred to as "Globe") invited EPA to their plant at Gastonia, N.C. to discuss the technical problems and exorbitant costs of controlling VOC emissions from the reaction spinning of spandex fibers. Mr. Keener and Mr. Legendre also led us on a very informative plant tour.

Globe is one of two U.S. producers of spandex fiber. Spandex is a generic name for polyurethane fiber. Urethane is the product of reacting a polyester prepolymer with a diamine crosslinking agent. Globe manufactures their own prepolymer at the plant.

Globe forms their fiber by pumping a polyester prepolymer through spinnerets at a constant rate into a 2-4 percent solution of ethylenediamine in toluene. A chemical reaction precipitates the polymer which is withdrawn from the bath and laid on a heated conveyor belt. The crosslinking reaction continues for the duration of the process. Fiber sizes range from 10-7000 denier.

From the heated conveyor the fiber is drawn through a two-stage oven. The first stage is heated with steam coils to about 300°F. The second stage is heated with infrared heaters to over 400°F. After drying the fiber is wound on packages.

Potential VOC emissions originate at the spin bath, the heated conveyor belt and in the oven. Essentially all air that enters the spinning room is sucked into the hooding that surrounds the spin bath and conveyor belt. This stream is ducted to a carbon adsorption (CA) system. The first stage of the oven is also vented to the carbon adsorber. The second stage exhaust has been shown to have a maximum of 30 ppm solvent so it is not vented to the CA system. The gas streams from the spinning room and oven are combined and cooled in a heat wheel-type exchanger to less than 100°F prior to entering the bed. (Globe uses six carbon beds at Gasonia and is planning to add two more. Their plant in Fall River, Massachusetts, uses 16.)

The carbon is regenerated with steam. Steam consumption is about 2,000 pounds per hour. Regeneration is on a time cycle because severe carbon-fouling reduces the bed efficiency in a few weeks to the point that a breakthrough cycle would be steaming the bed much too frequently. Condensed steam and solvent is sent to solvent recovery. There is some diamine and prepolymer in the aqueous phase of the condensate. After decantation of the toluene, gentle agitation causes the remaining organics to globulate which make them easy to separate from the aqueous phase. The toluene is purified in a flash distillation column.

The concentration of the exhaust stream to the CA unit is always less than 25 percent LEL. The spinning room toluene concentration is maintained around 50-60 ppm. The oven exhausts are designed to never exceed 25 percent LEL.

Globe's overall solvent recovery is not as high as they would like it to be. They make daily readings of recovered solvent and total solvent feed. The problem is centered around the performance of the CA system. Apparently unreacted prepolymer and diamine cause severe carbon fouling. The nature of the fouling is such that the carbon pellets are cemented into a hardened asphalt-like solid. The carbon has to be removed from the beds at least every 18 months. The operation is manual (picks and axes) and requires two weeks to complete. The carbon must then be shipped to Union Carbide or another supplier to be reactivated in a furnace. The calcining process is not effective.

Globe has had several bed fires but these were attributed to inadequate sensing instrumentation. They have recently solved this problem, however, by installing CO monitors in the beds and exhaust ducts.

Globe loses a large percentage of the carbon during each reactivation. The actual amount was discussed in our conversation concerning the cost of emission control. Globe's average losses of carbon are 44 percent. Their attempts to control emissions is costing them an estimated \$247,000 per year for two plants. This data is attached. Globe is considering an on-site reactivation process which should result in a considerable savings if successful. Globe considers incineration to be too expensive and a waste of energy. They also think there could be severe corrosion problems.

V. Summary

In most industrial processes the key to reducing VOC emissions is improving the capture of would-be fugitive vapors. Subsequent control device efficiencies routinely operate at 95 percent efficiency and higher. Globe's situation is the opposite. Over 99 percent of the organic vapors evolved in their reaction spun process are captured and sent to solvent recovery. A rather complex fouling phenomenon in the carbon bed, however, decreases the emission control efficiency to less than 90 percent rather quickly. The consequential removing, shipping, and reactivating of the carbon is a large expense to the company. There are not any short-term solutions although Globe is investigating sacrificial beds and on-site carbon reactivation.

Attachment

OAQPS:ESED:CPB:CAS:DCrumpler:tec:MU:1033:x5605:MD-13:11/30/81:File NO \_\_\_\_\_

## ESTIMATED ANNUALIZED COSTS SUMMARY

	SENT IN FOR B.I.D. ADJUSTMENTS	ADJUSTED LEFOR PER B.I.D.	ADJUSTED MAINT MATL TO ACTUAL	ADJUSTED LABOR TO ACTUAL
<b>Direct Operating Cost</b>				
OPERATORS (3)	324000	109000	108000	⑤ 102368
SUPERVISION	42600	16200	16200	15355
OPERATING MATERIALS ①	156378	53378	156378	156378
MAINTENANCE LABOR	324000	82200	102000	⑦ 122657
MAINT. MATERIAL	46450	46450	⑥ 117399	117399
ELECTRICITY ②	198332	198332	198332	198332
STEAM ③	414292	414292	414292	414292
WASTE DISPOSAL	15423	15423	15423	5423
	1522135	1263235	135124	1141364
<b>Indirect Operating Cost</b>				
OVERHEAD	522250	212250	290699	276319
PROPERTY TAX	15423	15423	15423	15423
INSURANCE	15423	15423	15423	15423
ADMINISTRATION	30966	30966	30966	30966
CAPITAL RECOVERY COST	185201	185201	125201	125201
	812583	466923	539432	544252
<b>TOTAL COST</b>	2334718	1530158	1673616	1625416
<b>CREDITS</b>				
RECOVERED SOLVENT ④	1438323	1438323	1438323	1438323
<b>NET ANNUAL LOSS</b>	902395	92305	235293	247093

- ① COST OF CARBON REPLACEMENT & REACTIVATION
- ② BASED ON ACTUAL USAGE & \$0.0635 IN MA, & \$0.0263 IN N.C.
- ③ BASED ON USAGE & ACTUAL COST OF \$7.00/1000 LB
- ④ BASED ON PROJECTED COST OF \$ 1.77/GAL
- ⑤ ACTUAL MATERIAL COST
- ⑥ BASED ON WAGES OF \$13.39/HR
- ⑦ BASED ON ACTUAL MAINTENANCE LABOR CHARGES

## DIRECT OPERATING COSTS

### DIRECTORS

WAGES OF \$11.16 PER HOUR, 52 HRS/WK, 49 WKS/YR FOR 3 MEN.  
 $(\$11.16 \times 52 \times 49 \times 3) = \$85,307$   
ADD 10% PER YEAR FOR INCREASES  $(85307)(1.1) = \$102,368$

### SUPERVISION

AT 15% OF DIRECT LABOR  $(\$102,368)(0.15) = \$15,355$

### OPERATING MATERIALS

WILL LIMIT THIS ITEM TO CARBON REPLACEMENT COSTS PLUS CARBON REACTIVATION COSTS.

#### HISTORICAL LOSSES:

1977 = 78,000 LB REACTIVATED W/ LOSSES OF	23,400 LB
1978 = 73,000 " " "	52,260 LB
1980 = <u>84,000 " " "</u>	<u>29,400 LB</u>
240,000	105,060

AVG. LOSSES =  $(105060) \div (240,000) = 43.78\%$

#### PROJECTED LOSSES:

STARTING IN JULY 1983 WE WILL BE REACTIVATING 144,000 LB OF CARBON EVERY 18 MONTHS, OR AN AVERAGE OF 96,000 LB/YR. AT THE PRESENT RATE OF LOSSES, WE EXPECT TO REPLACE  $(96,000)(0.4378) = 42,029$  LB/YR OR 21 TONS.

#### REPLACEMENT COSTS:

CARBON COST HAS RISEN FROM \$0.30/LB IN 1976 TO \$1.30/LB IN 1981 OR APPROXIMATELY 12.5% PER YEAR. IF WE CONSERVATIVELY ASSUME THE RATE DROPS TO 10% PER YEAR, CARBON WILL COST \$1.56/LB IN 1983. REPLACEMENT COST IS THEN  
 $(42,000)(\$1.56) = \$65,520$  PER YEAR

### REACTIVATION COSTS:

UNION CARBIDE'S CHARGES FOR REACTIVATION IN 1981 WERE \$ 91 PER 55 GAL DRUM. IF WE ASSUME A 10% ANNUAL INCREASE CHARGES WOULD BE \$ 109.20/DRUM IN 1983.

SINCE 96,000 LBS IS EQUIVALENT TO 540 DRUMS, THE CHARGES WOULD BE (540)(\$109.20) = \$53,968 PER YEAR.

TRANSPORTATION IS ESTIMATED AT \$10,965 PER YEAR

REPLACEMENT DRUM COST = (540)(\$15)(0.45) = \$3,645

LABOUR TO UNLOAD & LOAD TANKS REQUIRES 8 MEN FOR 16 DAYS WORKING 10 HR/DAY

COST IS (8)(16)(10)(\$13.39) = \$17,139 PER YEAR

TOTAL OPERATING MATERIALS COST IS

REPLACEMENT CARBON = \$65,520

REACTIVATION CHARGES = 53,968

TRANSPORTATION CHG. = 10,965

REPLACEMENT DRUMS = 3,645

LABOUR = 17,139

\$156,378

### MAINTENANCE LABOUR

DIRECT WAGES PAID FROM 1977 TO 1981 WERE \$109,130 OR \$21,826 PER YEAR IN FALL RIVER

DIRECT WAGES PAID FROM 1976 TO 1981 WERE \$126,753 OR \$21,126 PER YEAR IN GASTONIA.

FALL RIVER SYSTEM SIZE DOUBLED IN JULY 1980 SO COSTS SHOULD DOUBLE BY 1983 TO \$43,652 PER YEAR

GASTONIA SYSTEM EXPANSION IN DEC 1981 WILL INCREASE COST TO (21,126)(\$/6) = \$28,168 PER YEAR

DIRECT WAGES ARE THEN \$71,820/YR

WITH FRINGES & INCREASES IN 1983 THIS WILL AMOUNT TO (71,820)(1.14)(1.2) = \$120,657 PER YEAR

Material Claimed Confidential  
By Company and Therefore  
Deleted From Inclusion  
In The Public Record

As requested in Docket Item Number IV-D-9  
and consistent with 40 CFR Part 2, page 4  
of the 4 page attachment to this trip report  
has been withdrawn from the docket and placed  
in the Emission Standards and Engineering  
Division confidential files.