

**Bell Jr. High**

LFG EFD

BELL JR. HIGH SCHOOL LANDFILL  
SURELITE FLARE

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02\_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Data Qual. = D  
making some calls  
flares not operated  
under normal conditions

No exhaust flow  
NO<sub>x</sub> & CO emissions;

November 25, 1992

TO: Michael R. Lake, Chief  
Engineering Division

FROM: Dave Byrnes, Associate Toxics Engineer  
Archi dela Cruz, Junior Toxics Engineer

### EMISSION FACTORS FOR LANDFILL GAS FLARES

The San Diego Air Pollution Control District (District) contracted the South Coast Environmental Company (SCEC) to source test the Arizona Street and Bell Junior High School landfill gas flares. The sites were source tested for SO<sub>x</sub>, NO<sub>x</sub>, CO, TOG/ROG, particulates, and speciated toxic organic gases between March 30 and April 7, 1992.

The source test results of SCEC have been reviewed and approved by the District Monitoring and Technical Services Section (M&TS). District Toxics Engineering Section has generated the following emission factors for landfill gas flares using the M&TS approved source test reports. The emission factors are presented below in units of lbs of contaminant per million BTU.

Emission Factors for Landfill Gas Flares (lbs contaminant/mm BTU).

Contaminant	Arizona	Bell	Average	Recommended*	SCAQMD
SO <sub>x</sub>	0.0077	0.0105	0.0091	0.01	0.001
NO <sub>x</sub>	0.0825	0.0562	0.0694	0.10	0.05
CO	<0.0170	<0.0181	<0.0176	0.02	0.19
Particulates	0.0106	0.0207	0.0157	0.02	0.07
ROG**				0.06	0.42

\* Recommended for permit processing.

\*\* Inlet concentrations of 0.2 and a conservative destruction efficiency of 70% will be used for the purposes of permit processing.

## ENGINEERING'S METHODOLOGY.

Both energy and mass balance were performed to verify the source test report information approved by M&TS. A carbon balance was used to determine the landfill gas flow at the inlet. A hydrogen balance was used to verify the methane content of the inlet landfill gas. Data from Arizona Run #3 and Bell Run #1 were determined to be acceptable after adjustment of the outlet stack temperatures, landfill gas inlet flow rates, and inlet methane concentrations.

An Excel spreadsheet was developed to calculate the energy at the inlet and at the outlet of the flare, the heat of combustion of the landfill gas, and the heat loss by the flare. Test results were adjusted to develop more accurate operating parameters. These operating parameters were verified by inspecting the heat loss as a percent of the total heat output.

Table 1 lists the key operating parameters that were used to produce reasonable energy balances and to determine the landfill emission factors.

Table 1. Flare Operating Parameters.

PARAMETERS	ARIZONA	BELL
Stack Temperature	2110°R	2010°R
Inlet Flow of Landfill Gas	242 cfm	316 cfm
Methane Content at Inlet	60%	55%

## STACK TEMPERATURE CORRECTIONS.

It was discovered that SCEC's temperature readings may have been taken improperly and the temperature probe may have been calibrated incorrectly. At Arizona Street, M&TS noticed the SCEC did not allow the temperature probe to reach equilibrium after reinserting the probe into the next port or sampling location. M&TS corrected for this incorrect measurement technique and approved a temperature value of 1903°R. No correction was made by M&TS for the possible calibration error. The thermocouple installed in the site flare displayed an average temperature of 2110°R. A difference of 207° is observed between the two temperature probes.

Temperature readings were apparently performed properly at Bell. SCEC measured an average temperature of 1776°R. The thermocouple installed in the site flare displayed an average temperature of 2010°R. A difference of 234° is observed between the two temperature probes.

It is believed that the temperature readings from the installed thermocouples in both site flares represent the actual stack temperature. The differences between SCEC's temperature measurements and the temperature displayed by the installed thermocouples at both sites are very similar. SCEC's temperature measurements are ~200° lower than both of the thermocouples installed in each

site flare. It is believed that SCEC's temperature probe is reading ~200° less than the actual stack temperature due to a calibration error.

Engineering used the temperature readings measured by the installed thermocouples at each site in an energy balance of each system and for emission factor calculations.

#### **LANDFILL GAS INLET FLOW RATE CORRECTIONS.**

The landfill gas inlet flow meters at both sites were inaccurate. Correct landfill gas inlet flow rates were determined by performing a carbon balance using a temperature corrected exhaust flow rate and the %CO<sub>2</sub> outlet value approved by M&TS. Arizona's flow meter read 345 cfm during the source test. The calculated flow rate was 242 cfm (the site's flow meter reads 43% higher). Bell's flow meter read 195 cfm while the calculated flow rate was 316 cfm (the site's flow meter reads 38% lower).

Engineering used the corrected inlet flow rates in an energy balance of each systems and for emission factors calculations.

#### **LANDFILL GAS METHANE CONCENTRATION CORRECTIONS.**

##### **Arizona Street Landfill Gas Flare Source Test Report.**

Run #3 of the particulates testing was the only run that was used for energy balance and emission factors calculations. Runs #1 and #2 were eliminated from the average by M&TS.

An average inlet methane content of 390,000 ppm was approved by M&TS for Arizona. This average included an unrealistic methane content of 120,000 ppm. This approved methane concentration is incorrect as demonstrated by an energy balance of the system. See spreadsheet #1. An inlet methane content of 600,000 ppm is more accurate based on both a hydrogen and energy balance of the system. See spreadsheet #2. Past inlet sampling conducted by the site supports this value. Therefore, a methane content of 600,000 ppm was used by Engineering to calculate the emission factors for Arizona Street.

##### **Bell Junior High School Landfill Flare Source Test Report.**

Run #1 of the particulates testing is believed to be the best data obtained for the energy balance and emission factor calculations. Run #2 was eliminated from the average by M&TS. Run #3 is ignored by Engineering because the percent H<sub>2</sub>O at the outlet is too high relative to the percent CO<sub>2</sub> at the outlet. The percent of H<sub>2</sub>O at the outlet should equal the percent of CO<sub>2</sub> at the outlet for an inlet methane content of 50%.

An average inlet methane content of 253,333 ppm was approved by M&TS for Bell. The average included an unrealistic methane content of 160,000 ppm. This approved methane concentration is incorrect as demonstrated by an energy balance on the system. See spreadsheet #3. An inlet methane content of 550,000 ppm is more accurate based on both a hydrogen and energy balance of the system. See spreadsheet #4. Therefore, a methane content of 550,000 ppm was used by Engineering to calculate the emission factors for Bell.

### TOXIC AIR CONTAMINANTS.

The GC analyses of toxic air contaminants (TAC's) as approved by M&TS shows that both sites have similar compositions of TAC's. Table 2 and 3 presents the TAC's destruction efficiencies for both sites. Inlet and outlet detection limits were used when non-detectable concentrations were reported.

Table 2. Destruction Efficiency of TAC's at Arizona Street Flare.

Contaminant	Inflow Conc., lbm/hr	Outflow Conc., lbm/hr	Destruction Efficiency, %
Vinyl Chloride	0.0024	<0.00044 (ND)	>81.7
Methylene Chloride	0.0010	0.00008	91.8
Chloroform	<0.0005 (ND)	<0.00044 (ND)	>12
1,2-Dichloroethane	<0.0005 (ND)	<0.00044 (ND)	>12
1,1,1-Trichloroethane	0.0025	<0.00044 (ND)	>82.4
Benzene	0.00056	0.0003	38.2
Carbon Tetrachloride	<0.0005 (ND)	<0.00044 (ND)	>12
Trichloroethene	0.0038	<0.00044 (ND)	>88.4
1,2-Dibromoethane	<0.0005 (ND)	<0.00044 (ND)	>12
Tetrachloroethene	0.0079	<0.00044 (ND)	>94.4

Table 3. Destruction Efficiency of TAC's at Bell Jr. High Flare.

Contaminant	Inflow Conc., lbm/hr	Outflow Conc., lbm/hr	Destruction Efficiency, %
Vinyl Chloride	0.0012	<0.00028 (ND)	>76.7
Methylene Chloride	0.0029	<0.00028 (ND)	>90.5
Chloroform	<0.0004 (ND)	<0.00029 (ND)	>29.3
1,2-Dichloroethane	<0.0004 (ND)	<0.00028 (ND)	>30.0
1,1,1-Trichloroethane	0.0014	<0.00028 (ND)	> 79.7
Benzene	0.0027	0.00038	85.9
Carbon Tetrachloride	<0.0004 (ND)	<0.00027 (ND)	>32.5
Trichloroethene	0.011	<0.00027 (ND)	>97.5
1,2-Dibromoethane	<0.0004 (ND)	<0.00028 (ND)	>30.0
Tetrachloroethene	0.017	<0.00027 (ND)	>98.4

### **LANDFILL GAS FLARE EMISSION FACTORS.**

Emission factors for SO<sub>x</sub>, NO<sub>x</sub>, CO, and particulates were calculated using M&TS approved emissions, the corrected flow rate out the stack (using installed thermocouple readings), the corrected landfill gas flow rate at the inlet (using carbon balance), and the adjusted methane content at the inlet (using energy and hydrogen balance).

M&TS reported undetectable CO in the exhaust of both stacks but did not specify a detection limit. A detection limit of 10 ppm was assumed by Engineering and was used to calculate the CO emission factors.

The approved M&TS source test report showed that all non-methane hydrocarbons (ROG) were non-detectable (ppm range) at both the inlet and the outlet sampling locations for each site. It is recommended that an inlet concentration of 0.2 lbs ROG/mm BTU based on detection limits be used to estimate the landfill ROG generation rate. Using a conservative destruction efficiency of 70%, a 0.06 lbs ROG/mm BTU emission factor is recommended for permit processing.

### **SUMMARY AND DISCUSSION OF RESULTS.**

The recommended emission factor of NO<sub>x</sub> is relatively similar to the SCAQMD emission factor. SCAQMD emission factor for SO<sub>x</sub> is one order of magnitude less than the recommended emission factor. This is probably due to differing of sulfur content in the landfill gas or differing sampling methodology. The recommended emission factors for CO and particulates indicate more efficient combustion than the SCAQMD emission factors.

SCAQMD's emission factor for ROG is too high. With SCAQMD's ROG emission factor, the outlet concentration of ROG would equal ~69 ppm. This value is higher than the measured ROG concentration in any of the sampled landfill gas inlets in San Diego. SCAQMD's emission factor for ROG is questionable. The recommended value based on non-detectable concentrations will be used by Engineering.

## RECOMMENDATIONS.

It is recommended that these emission factors be used to calculate emissions for landfill gas flares and be used to determine a cut-off point for source testing landfill gas flares. With the recommended emission factors, landfill gas flare emissions can be estimated. Table 4 presents these estimated emissions.

Table 4. Estimated Emissions from Landfill Gas Flares.

Landfill Size, tons	Gas Gen. Rate, mm cu ft/yr	Estimated Emissions, tons/yr*				
		NOx	ROG	CO	Particulates	SOx
1,000,000	85.6	2.0	1.2	0.4	0.4	0.2
2,000,000	171.4	4.0	2.4	0.8	0.8	0.4
4,000,000	343	8.0	4.8	1.6	1.6	0.8
6,000,000	514	12.0	7.2	2.4	2.4	1.2
10,000,000	857	20.0	12.0	4.0	4.0	2.0

\* Assumes an inlet methane content of 50%.

A landfill with a size of 9,000,000 tons and a continuous operating flare triggers Rule 20.2. A landfill with a size of 5,000,000 tons would require offsets per the proposed New Source Review. It is recommended that the presented emission factors be used to estimate emissions from landfills with a size of <5,000,000 tons. Source testing is recommended for landfills with a size of ≥5,000,000 tons.

TEST SUMMARY OF LANDFILL GAS THERMAL OXIDIZER  
AT BELL JUNIOR HIGH SCHOOL IN SAN DIEGO

1. Narrative Summary
2. Test Summary
3. Engineering Report
4. SO<sub>x</sub> Average
  - Run #1
  - Run #2
  - Run #3
5. NO<sub>x</sub> and CO Analysis
6. Runs #1 - #4 GC Analysis
7. Particulates
8. Test Witness
  - Run #1
  - Run #2
  - Run #3

**Purpose:** The SDAPCD engineering division requested testing of emissions from a landfill gas thermal oxidizer located at Bell Junior High School. Data regarding emissions from this type of operation were needed for regulatory decision making. The objective of these tests was to quantify emissions of speciated organic gases, oxides of nitrogen, carbon monoxide, oxides of sulfur and particulates. An additional objective was to assess the efficiency of the thermal oxidizer in destroying incoming toxic organic compounds.

**Methods:** Organic gases were collected in summa polished stainless steel canisters and analyzed using gas chromatography as detailed in the attached appendix. Particulate matter and oxides of sulfur were collected and determined according to modified EPA Methods 5 and 8. Oxides of nitrogen and carbon monoxide were determined using SDAPCD Method 20. A copy of the protocol and referenced methods are contained in an appendix to this report. In general, testing was accomplished in accordance with agreed upon methodology. Individual sample runs which were determined to be substantively in error were deleted from data used in the attached summary table.

**Process Description:** Gases are generated from the decomposition or volatilization of previously deposited waste at the landfill. A gas collection system has been installed at this site to gather these gases for processing. The collected landfill gases are oxidized in an enclosed flare. Emissions associated with this incineration are quantified in the test program discussed in this report.

**Conclusions:** As indicated in the attached table of summarized results, emissions of oxides of sulfur, carbon monoxide and particulate matter are quite low. Emissions of oxides of nitrogen are also fairly low as would be expected from a low heating value fuel. Emissions of hydrocarbons, including various halogenated toxic species, are also quite low.

## Test Summary of Lar

:R

Site: Bell Junior High School  
620 South Briarwood Road  
San Diego, CA

Test #: 74070  
P.O. #: 880614  
Test Date: April 7, 1992

Equipment: Landfill gas thermal oxidizer  
Tested by: Russ Logan and Ted Jackman of SCEC  
Site personnel: Ray Purtee  
APCD engineer: Archi de la Cruz  
Lab analysis by: SCEC and Performance Analytical on April 21, 1992  
Report by: SCEC (Russ Logan) on May 14, 1992  
Reviewed by: David N. Shina on August 4, 1992  
Approved by: Judith Lake, chief of monitoring *Judith A. Lake 10/12/92*  
(This report has been reviewed and found to be representative of the testing that was performed.)

### SOx Test Results Summary

Item	I	SO <sub>3</sub>			SO <sub>2</sub>			Total SOx		
		O <sub>s</sub>	Cs(12%)	E	O <sub>s</sub>	Cs(12%)	E	O <sub>s</sub>	Cs(12%)	E
Units	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
Value	107	0.001733	0.002787	0.0643	0.001237	0.001998	0.0459	0.002970	0.004782	0.1102

### NOx and CO Test Results Summary

Gas	Test (ppm)	Limits (ppm)	Performance Exceedance/Non-exceedance
NOx	18.98	N/A	N/A
CO	ND	N/A	N/A

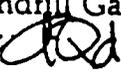
### Particulate Test Results Summary

Item	ts	Bws	%O <sub>2</sub>	%CO <sub>2</sub>	vs	Qstd	Cs(total)	Cs (12%, total)	E (total)	%I
Units	°F	%	%	%	ft/sec	dscfm	gr/hr	gr/dscf	lbs/hr	%
Value	1316	9.34	11.88	7.47	21.952	4337	0.0069	0.0095	0.22	105

### G.C. Test Results Summary

	Avg. Inlet		Avg. Outlet			Avg. Inlet		Avg. Outlet	
	Result ppm	Det. limit ppm	Result ppm	Det. limit ppm		Result ppb	Det. limit ppb	Result ppb	Det. limit ppb
C1 as methane	253333	54	1	1.8	Vinyl chloride	357	133	ND	7.3
C2 as ethane	ND	54	ND	1.8	Methylene chloride	703	98	ND	5.4
C3 as n-propane	ND	43	ND	1.5	Chloroform	ND	69	ND	3.8
C4 as n-butane	ND	33	ND	1.1	1,2-Dichloroethane	ND	83	ND	4.5
C5 as pentane	ND	22	ND	0.7	1,1,1-Trichloroethane	210	62	ND	3.4
C6 as n-hexane	ND	22	ND	0.7	Benzene	700	106	8	5.7
C7 as n-heptane	ND	22	ND	0.7	Carbon tetrachloride	ND	53	ND	2.9
C8 as n-octane	ND	22	ND	0.7	Trichloroethene	1633	62	ND	3.4
C9 as n-nonane	ND	22	ND	0.7	1,2-Dibromoethane	ND	43	ND	2.4
>C9 as n-nonane	ND	22	ND	0.7	Tetrachloroethene	2100	50	ND	2.7

**ENGINEERING SOURCE TEST REPORT  
BELL JR. HIGH LANDFILL GAS FLARE**

DATE: April 10, 1992  
SOURCE: Bell Jr. High Landfill  
EQUIPMENT: Bell Jr. High Landfill Gas Flare  
ENGINEER: Archi dela Cruz 

**TEST PURPOSE**

The purpose of this source test is to more accurately assess PM, CO, NO<sub>x</sub>, SO<sub>2</sub>, and TOG/ROG emissions which are generated at this type of source. Also, there will be an analysis of toxic emissions generated at the inlet and outlet of the landfill gas flare system. The results of this source test will be used to generate emission factors for this type of source.

**BACKGROUND INFORMATION**

SDAPCD M&TS personnel: Dave Shina and Janet Cawyer  
Contracted source testing company: Russ Logan  
South Coast Environmental Company  
Operator of flare: Bob Hanley and Bob Hobbs  
County of San Diego

The source test was conducted through the course of three separate source test dates. In the initial source test (March 30, 1992), the boom that was present to lift the source technician up to the stack was not adequate enough to accommodate all of the testing equipment. There was only enough room to accommodate the equipment that would sample NO<sub>x</sub>, CO, and TOG/ROG. Testing proceeded for these contaminants on this date. Only two TOG/ROG samples were obtained since one sampling canister broke.

A second date (April 1, 1992) was scheduled to sample for PM. A scissor lift was provided by the operators of the flare to accommodate both the source test technician and the PM sampling equipment. After approximately one hour of testing, the sampling nozzle broke. The contractor was unable to put a replacement nozzle on. Testing was discontinued.

On the third date of sampling (April 7, 1992), the contractor returned to sample for PM. I was unable to attend this source test. Lynn Shallenberger was my replacement for this source test.

**OPERATING PARAMETERS DURING TESTING**

**March 30, 1992 Source Testing**

The flare was not in operation upon arrival. The flare was shut down for a day prior to the source test in order to generate enough landfill gas for testing.

The auxiliary gas line was manually shut. A boom was provided to lift the source test technician up to the stack. The following parameters were observed during the NO<sub>x</sub>, CO, and TOG/ROG source test.

Starting time of sampling:	12:00 pm
Ending time of sampling:	2:55 pm
Average landfill gas flowrate:	195 cfm
Natural gas usage:	0 cfm
Average flare temperature:	1547 F
Flare operating set temperature	1550 F
Average landfill gas O <sub>2</sub> content:	0.4%

#### April 7, 1992 Source Testing

Only PM was tested on this source test. Lynn Shallenberger was the engineer present for this source test. The following parameters were obtained from her source test data.

Starting time of sampling:	10:29 am
Ending time of sampling:	3:59 pm
Average landfill gas flowrate:	195 cfm
Natural gas usage:	0 cfm
Average flare temperature:	1549 F
Flare operating set temperature	1550 F
Average landfill gas O <sub>2</sub> content:	0.47%

#### DISCUSSION AND CONCLUSION

The flare was not operated under typical conditions during testing. The flare usually operates for two hours per day (as reported by Bob Hanley). To conduct the source test, the flare had to operate 40 minutes to one hour for each sampling. Though operating times were extended for the source test, it is believed that the gas that was burned is representative of the typical landfill gas extracted for combustion in the flare because of the relatively minor increase in the landfill gas O<sub>2</sub> content.

The landfill gas flare system appeared to be in good operating condition. There were no visible emissions during the source test. There were no noticeable operational testing changes observed throughout the testing. The flare operated under permit conditions.

# Landfill Flare Source Test Data

## Bell Jr. High Landfill (NO<sub>x</sub>, CO, TOG/ROG)

### BACKGROUND DATA:

existing cumulative flow = 17311.74 (1000ft<sup>3</sup>)

ending cum. flow 17349.45 (1000ft<sup>3</sup>)

operating set temperature = 1550°F

warm up time 11:39 to 11:45

O<sub>2</sub> % content = 0.045%

no visible emissions on start-up

flame rate = 185 scfm

Time	low cutoff (175) LANDFILL GAS BURNED, cfm	low cutoff (1500) TEMPERATURE °F	O <sub>2</sub> CONTENT	meter read as percent
2:00	200	1514	0.35%	
2:10	200	1529	0.35%	
2:20	199	1549	"	
2:30	197	1572	"	
2:40	198	1550	"	
2:50	197	1549	"	
3:00	196	1557	0.35%	
3:10	195	1544	0.38%	
3:20	195	1542	0.4%	
3:30	193	1545	0.4	
3:40	192	1546	0.4	
3:50	192	1547	0.4	
4:00	191	1559	0.4	
4:10	191	1552	0.4	
4:20	191	1552	0.4	

AE	LANDFILL GAS BURNED, cfm	TEMPERATURE	O <sub>2</sub> CONTENT, %
2:30	192	1544	0.45%
2:40	193	1550	0.45
2:50	193	1554	0.45
2:55	193	1559	0.45

# Landfill Source Test Data (PM Tests) Bell Jr. High Flare

initial flow meter reading = 17349.45 x 1000 scf (standard ft<sup>3</sup>)

initial O<sub>2</sub> content = 0.55%

start-up time = 2:50

ending time = 2:57 to reach 1550°F

↳ to reach 1550°F

0 visible emissions on start-up

temp. fluctuates from ~1500 to ~1590°F for first minutes

TIME	LAND FILL GAS BURNED, cfm	TEMP., °F	O <sub>2</sub> CONTENT
:05	201	1516	0.55%
-	201	1569	0.55
2	201	1554	0.55
:30	199	1539	0.55
40	198	1563	0.55
:10	195	1553	0.5

~~3:00~~ broke nozzle (3:45)

↳ shut down flare. Having difficulty putting on new nozzle.

Test bombed.



Shallenberger  
1-2-92  
Bell Jr. High Flare PM Tests

Bob  
Russ  
TED  
Dave  
Lynn

initial flowmeter reading: 18603.94  
initial O<sub>2</sub> Content: .41  
startup time: 12:10  
1550° F at: 12:20  
problems? no VE's  
specific gravity gauge broke. Didn't affect test

18605.77

TIME	CFM	TEMP, °F	O <sub>2</sub> content
12:22	200	1542	.41
12:27	201	1543	.41
12:32	202	1544	.41
12:38	200	1548	.41
12:47	200	1544	.45
12:52	200	1541	.46
12:57	200	1552	.45
1:06	200	1546	.48
1:11	199	1549	.48

~~inlet & outlet TOG & ROG sample taken at:~~  
1:11 probe broke during part change. Can't continue test.

2  
12/20

in Shallenberger

7-92

# Bell Jr. High Flare PM Tests

initial flowmeter reading: 18617.55 x 1000 cf

initial O<sub>2</sub> content: .5

startup time: 2:08

550° F at: 2:18

problems? none. lag after at startup no VE's  
water shut off. test delayed.

Final of 1 out flowmeter reading: 18624.99 x 1000 cf

	CFM	TEMP °F	O <sub>2</sub> content
2:49	197	1551	.5
2:50	194	1550	.5
2:51	194	1546	.5
2:52	194	1546	.54
2:53	193	1547	.55
2:54	193	1553	.55
2:55	194	1544	.58
2:56	194	1553	.58
2:57	194	1547	.59

inlet & outlet TOG & ROG sample taken at: 2:55. Strong methane smell during draw 356 °F

ending flowmeter reading: 18638.54 x 1000 cf

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #3  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @		lbs/hr
				12% CO2		
Probe & Nozzle:	0.33	0.000171	0.000154	0.000298		0.01
Filter:	0.1	0.000052	0.000046	0.000090		0
Condensables:	13.804	0.007184	0.006448	0.012494		0.28
Total:	14.234	0.007408	0.006649	0.012883		0.29

N BaCl = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @		lbs/hr
					12% CO2		
Probe & Nozzle:	16.5	0.1	0.000404	0.000362	0.000703		0.02
Filter:	10	0	0	0	0		0
Condensables:	20.3	0.24	0.001194	0.001071	0.002076		0.05
Total:			0.001598	0.001434	0.002780		0.07

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1445	1555	12.33	6.9	10.24	29.59	4497

$$\text{Concentration(SO}_2\text{)} = [K \cdot \text{Normality} \cdot V\text{-titrant} \cdot (V\text{-solution}/V\text{-aliquot})] / Vm\text{-}(std)$$

### CALCULATIONS:

#### SCCELLANEEOUS DATA

N = Normality =

Vmstd =

Qstd =

%CO2 =

15.43 grains = 1 gram

7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

**SO2:**

MW =

# equiv/mole vs. BaCl2 =

K =

#### FRONT HALF

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(SO2,front) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std) =$

Cs(SO2,front) = 15.43 \* Conc(SO2,front) =

Cs(SO2,12%,front) = Cs(SO2,front) \* (12/%CO2) =

E (SO2,front) = 0.00857 \* Qstd \* Cs(SO2,front) =

#### FILTER

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(SO2,filter) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std) =$

Cs(SO2,filter) = 15.43 \* Conc(SO2,filter) =

Cs(SO2,12%,filter) = Cs(SO2,filter) \* (12/%CO2) =

E (SO2,filter) = 0.00857 \* Qstd \* Cs(SO2,filter) =

#### BACK HALF

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(SO2,back) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std) =$

Cs(SO2,back) = 15.43 \* Conc(SO2,back) =

Cs(SO2,12%,back) = Cs(SO2,back) \* (12/%CO2) =

E (SO2,back) = 0.00857 \* Qstd \* Cs(SO2,back) =

#### TOTAL SO2

Conc(SO2,total) =  $\sum \text{Conc(SO2,location)}$

Cs(SO2,total) =  $\sum \text{Cs(SO2,location)}$  =

Cs(SO2,12%,total) =  $\sum \text{Cs(SO2,12%,location)}$  =

E (SO2,total) =  $\sum \text{E(SO2,location)}$  =

SDAPCD
--------

SCEC
------

0.00971
29.59
4478
6.9

0.00971	equiv/liter
29.59	dscf
4497	dscfm
6.9	%

15.43  
0.00857

15.4 grains/gram  
0.00857 lbs-min/grs-hr

64.06

not done g/mole

2

not done equiv/mole

32.03

not done grams/equiv

0.2
250
10

not done	ml
not done	ml
not done	ml

0.0000526

not done grams/dscf

0.0008109

not done grains/dscf

0.0014103

not done grains/dscf

0.0311

not done lbs/hr

0
250
10

not done	ml
not done	ml
not done	ml

0.0000000

not done grams/dscf

0.0000000

not done grains/dscf

0.0000000

not done grains/dscf

0.0000

not done lbs/hr

0.1
250
10

not done	ml
not done	ml
not done	ml

0.0000263

not done grams/dscf

0.0004054

not done grains/dscf

0.0007051

not done grains/dscf

0.0156

not done lbs/hr

not done grams/dscf

not done grains/dscf

not done grains/dscf

not done lbs/hr

### COMMENTS:

SCEC did not calculate the contribution due to SO2; so, the District will use the values generated by the District's spreadsheet.

$$\text{Concentration}(\text{H}_2\text{SO}_4) = [K * \text{Normality} * V_{\text{titrant}} * (V_{\text{solution}} / V_{\text{aliquot}})] / V_{\text{m}}(\text{std})$$

### CALCULATIONS:

#### SCCELLANEUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 %CO2 =  
 15.43 grains = 1 gram  
 7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

SDAPCD	SCEC	
0.00971	0.00971	equiv/liter
29.59	29.59	dscf
4478	4497	dscfm
6.9	6.9	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

#### SO3 as H2SO4:

MW = 98.08      \*\* 97 g/mole  
 # equiv/mole vs. BaCl2 = 2      2 equiv/mole  
 K = 49.04      48.5 grams/equiv

#### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,front) =  $[K * N * V_t * (V_{\text{soln}} / V_{\text{aliquot}})] / V_{\text{m}}(\text{std}) =$   
 Cs(H2SO4,front) = 15.43 \* Conc(H2SO4,front) =  
 Cs(H2SO4,12%,front) = Cs(front) \* (12 / %CO2) =  
 E (H2SO4,front) = 0.00857 \* Qstd \* Cs(H2SO4,front) =

0.1	0.1	ml
165	165	ml
10	10	ml
0.0000266	0.0000263	grams/dscf
0.0004097	0.0004044	grains/dscf
0.0007125	0.0007033	grains/dscf
0.0157	0.0156	lbs/hr

#### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,filter) =  $[K * N * V_t * (V_{\text{soln}} / V_{\text{aliquot}})] / V_{\text{m}}(\text{std}) =$   
 Cs(H2SO4,filter) = 15.43 \* Conc(H2SO4,filter) =  
 Cs(H2SO4,12%,filter) = Cs(filter) \* (12 / %CO2) =  
 E (H2SO4,filter) = 0.00857 \* Qstd \* Cs(H2SO4,filter) =

0	0	ml
100	100	ml
10	10	ml
0.0000000	0.0000000	grams/dscf
0.0000000	0.0000000	grains/dscf
0.0000000	0.0000000	grains/dscf
0.0000	0.0000	lbs/hr

#### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,back) =  $[K * N * V_t * (V_{\text{soln}} / V_{\text{aliquot}})] / V_{\text{m}}(\text{std}) =$   
 Cs(H2SO4,back) = 15.43 \* Conc(H2SO4,back) =  
 Cs(H2SO4,12%,back) = Cs(H2SO4,back) \* (12 / %CO2) =  
 E (H2SO4,back) = 0.00857 \* Qstd \* Cs(H2SO4,back) =

0.24	0.24	ml
203	203	ml
10	10	ml
0.0000784	0.0000775	grams/dscf
0.0012098	0.0011941	grains/dscf
0.0021039	0.0020767	grains/dscf
0.0464	0.0460	lbs/hr

#### TOTAL SO3

Conc(H2SO4,total) =  $\sum \text{Conc}(\text{H}_2\text{SO}_4, \text{location}) =$   
 Cs(H2SO4,total) =  $\sum \text{Cs}(\text{H}_2\text{SO}_4, \text{location}) =$   
 Cs(H2SO4,12%,total) =  $\sum \text{Cs}(\text{H}_2\text{SO}_4, 12\%, \text{location}) =$   
 E (H2SO4,total) =  $\sum \text{E}(\text{H}_2\text{SO}_4, \text{location}) =$

0.0001050	0.0001038	grams/dscf
0.0016195	0.0015985	grains/dscf
0.0028165	0.0027800	grains/dscf
0.0621	0.0616	lbs/hr

#### COMMENTS:

\*\* SCEC used an incorrect molecular weight for H2SO4, and this gave incorrect values for all the subsequent numbers that SCEC generated in their final report.

The District will use the numbers generated by the District's spreadsheet, because these values are correct.

**Test Witness - Run #3 (SOx)**

**TEST RESULTS SUMMARY:**

ITEM	I	SO3			SO2			Total SOx		
		Cs	Cs(12%)	E	Cs	Cs(12%)	E	Cs	Cs(12%)	E
UNITS	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
VALUE	104	0.001619	0.002816	0.062	0.001216	0.002115	0.047	0.002836	0.004932	0.109

**TEST PARAMETERS:**

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA NSPS guidelines and from the EPA CFR 40, Standards Method 8. The sampling utilized a front-end filter (fig. 1).

**CALCULATIONS:**

All calculations are based on the EPA CFR 40, July 1, 1991, Parts 53-60, Appendix A, Method 8.

**SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data, SCEC's as well as the District's, were transferred to the computer printout. All calculations were done by computer.

**ANALYSES:**

*Gas:* A CEM analysis was performed by SCEC.

*SOx:* All procedures follow EPA guidelines, except where noted in this report.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.

**OVERVIEW OF THE TEST**

**SAMPLING:** Passed

**LABORATORY:** Passed

The data from this test is acceptable and will be used in the overall test average.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #2  
 @ 68°F  
 EPA METHOD 5/8

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PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @		lbs/hr
				12% CO2		
Probe & Nozzle:	0	0	0	0		0
Filter:	1.2	0.000975	0.000868	0.001567		0.03
Condensables:	14.52	0.011806	0.010510	0.018965		0.39
Total:	15.72	0.012781	0.011379	0.020533		0.42

N BaCl = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @		lbs/hr
					12% CO2		
Probe & Nozzle:	13	0.05	0.000248	0.000221	0.000399		0.01
Filter:	10	0	0	0	0		0
Condensables:	22	0.1	0.000842	0.000749	0.001353		0.03
Total:			0.001091	0.000971	0.001753		0.04

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1220	1302	12.11	7.47	10.97	18.94	3834

---

$$\text{Concentration(SO}_2\text{)} = [K \cdot \text{Normality} \cdot V\text{-titrant} \cdot (V\text{-solution}/V\text{-aliquot})] / Vm\text{-}(std)$$

# CALCULATIONS:

## SCCELLANEOUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 %CO2 =  
 15.43 grains = 1 gram  
 7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

**SO2:**

MW =  
 # equiv/mole vs. BaCl2 =  
 K =

### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,front) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std)$  =  
 Cs(SO2,front) = 15.43 \* Conc(SO2,front) =  
 Cs(SO2,12%,front) = Cs(SO2,front) \* (12%/CO2) =  
 E (SO2,front) = 0.00857 \* Qstd \* Cs(SO2,front) =

### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,filter) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std)$  =  
 Cs(SO2,filter) = 15.43 \* Conc(SO2,filter) =  
 Cs(SO2,12%,filter) = Cs(SO2,filter) \* (12%/CO2) =  
 E (SO2,filter) = 0.00857 \* Qstd \* Cs(SO2,filter) =

### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,back) =  $[K \cdot N \cdot Vt \cdot (Vsoln/Valiquot)] / Vm(std)$  =  
 Cs(SO2,back) = 15.43 \* Conc(SO2,back) =  
 Cs(SO2,12%,back) = Cs(SO2,back) \* (12%/CO2) =  
 E (SO2,back) = 0.00857 \* Qstd \* Cs(SO2,back) =

SDAPCD	SCEC	
0.00971	0.00971	equiv/liter
18.94	18.94	dscf
3831	3834	dscfm
7.47	7.47	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

64.06 not done g/mole  
 2 not done equiv/mole  
 32.03 not done grams/equiv

0.05	not done	ml
130	not done	ml
10	not done	ml
0.0000107	not done	grams/dscf
0.0001647	not done	grains/dscf
0.0002646	not done	grains/dscf
0.0054	not done	lbs/hr

0	not done	ml
100	not done	ml
10	not done	ml
0.0000000	not done	grams/dscf
0.0000000	not done	grains/dscf
0.0000000	not done	grains/dscf
0.0000	not done	lbs/hr

0.1	not done	ml
22	not done	ml
10	not done	ml
0.0000036	not done	grams/dscf
0.0000557	not done	grains/dscf
0.0000895	not done	grains/dscf
0.0018	not done	lbs/hr

### TOTAL SO2

Conc(SO2,total) = $\sum \text{Conc(SO2,location)}$	0.0000143	not done	grams/dscf
<i>Correction for non-isokinetic conditions</i>			
Conc(SO2,total) = $\sum \text{Conc(SO2,location)} \cdot (1/100)$	0.0000169	not done	grams/dscf
Cs(SO2,total) = $\sum \text{Cs(SO2,location)}$	0.0002204	not done	grains/dscf
<i>Correction for non-isokinetic conditions</i>			
Cs(SO2,total) = $\sum \text{Cs(SO2,location)} \cdot (1/100)$	0.0002601	not done	grains/dscf
Cs(SO2,12%,total) = $\sum \text{Cs(SO2,12%,location)}$	0.0003541	not done	grains/dscf
<i>Correction for non-isokinetic conditions</i>			
Cs(SO2,12%,total) = $\sum \text{Cs(SO2,12%,location)} \cdot (1/100)$	0.0004179	not done	grains/dscf
E (SO2,total) = $\sum \text{E(SO2,location)}$	0.0085	not done	lbs/hr
<i>Correction for non-isokinetic conditions</i>			
E (SO2,total) = $\sum \text{E(SO2,location)} \cdot (1/100)$	0.0101	not done	lbs/hr

### COMMENTS:

SCEC did not calculate the contribution due to SO2; so, the District will use the values generated by the District's spreadsheet.

$$\text{Concentration(H}_2\text{SO}_4) = [K \cdot \text{Normality} \cdot V_{\text{titrant}} \cdot (V_{\text{solution}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$$

### CALCULATIONS:

#### SCCELLANEOUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 %CO2 =  
 15.43 grains = 1 gram  
 7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

SDAPCD	SCEC	
0.00971	0.00971	equiv/liter
18.94	18.94	dscf
3831	3834	dscfm
7.47	7.47	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

#### SB3 as H2SO4:

MW =  
 # equiv/mole vs. BaCl2 = 98.08      \*\* 97 g/mole  
 K = 2      2 equiv/mole  
 49.04      48.5 grams/equiv

#### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,front) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  = 0.0000163      0.0000162 grams/dscf  
 Cs(H2SO4,front) = 15.43 \* Conc(H2SO4,front) = 0.0002522      0.0002489 grains/dscf  
 Cs(H2SO4,12%,front) = Cs(front) \* (12/%CO2) = 0.0004051      0.0003998 grains/dscf  
 E (H2SO4,front) = 0.00857 \* Qstd \* Cs(H2SO4,front) = 0.0083      0.0082 lbs/hr

0.05	0.05	ml
130	130	ml
10	10	ml

#### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,filter) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  = 0.0000000      0.0000000 grams/dscf  
 Cs(H2SO4,filter) = 15.43 \* Conc(H2SO4,filter) = 0.0000000      0.0000000 grains/dscf  
 Cs(H2SO4,12%,filter) = Cs(filter) \* (12/%CO2) = 0.0000000      0.0000000 grains/dscf  
 E (H2SO4,filter) = 0.00857 \* Qstd \* Cs(H2SO4,filter) = 0.0000      0.0000 lbs/hr

0	0	ml
100	100	ml
10	10	ml

#### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,back) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  = 0.0000553      0.0000547 grams/dscf  
 Cs(H2SO4,back) = 15.43 \* Conc(H2SO4,back) = 0.0008535      0.0008424 grains/dscf  
 Cs(H2SO4,12%,back) = Cs(H2SO4,back) \* (12/%CO2) = 0.0013710      0.0013533 grains/dscf  
 E (H2SO4,back) = 0.00857 \* Qstd \* Cs(H2SO4,back) = 0.0280      0.0277 lbs/hr

0.1	0.1	ml
220	220	ml
10	10	ml

#### TOTAL SO3

Conc(H2SO4,total) =  $\sum \text{Conc(H}_2\text{SO}_4, \text{location)}$  = 0.0000717      0.0000709 grams/dscf  
*Correction for non-isokinetic conditions*  
 Conc(H2SO4,total) =  $\sum \text{Conc(H}_2\text{SO}_4, \text{location}) \cdot (1/100)$  = 0.0000846      0.0000836 grams/dscf  
 Cs(H2SO4,total) =  $\sum \text{Cs(H}_2\text{SO}_4, \text{location})$  = 0.0011056      0.0010913 grains/dscf  
*Correction for non-isokinetic conditions*  
 Cs(H2SO4,total) =  $\sum \text{Cs(H}_2\text{SO}_4, \text{location}) \cdot (1/100)$  = 0.0013046      0.0012877 grains/dscf  
 Cs(H2SO4,12%,total) =  $\sum \text{Cs(H}_2\text{SO}_4, 12\%, \text{location})$  = 0.0017761      0.0017531 grains/dscf  
*Correction for non-isokinetic conditions*  
 Cs(H2SO4,12%,total) =  $\sum \text{Cs(H}_2\text{SO}_4, 12\%, \text{location}) \cdot (1/100)$  = 0.0020958      0.0020687 grains/dscf  
 E (H2SO4,total) =  $\sum \text{E(H}_2\text{SO}_4, \text{location})$  = 0.0363      0.0358 lbs/hr  
*Correction for non-isokinetic conditions*  
 E (H2SO4,total) =  $\sum \text{E(H}_2\text{SO}_4, \text{location}) \cdot (1/100)$  = 0.0428      0.0423 lbs/hr

#### MENTS:

\*\* SCEC used an incorrect molecular weight for H2SO4, and this gave incorrect values for all the subsequent numbers that SCEC generated in their final report.

The District will use the numbers generated by the District's spreadsheet, because these values are correct.

**Test Witness - Run #2 (SOx)**

**TEST RESULTS SUMMARY:**

ITEM	I	SO3			SO2			Total SOx		
		Cs	Cs(12%)	E	Cs	Cs(12%)	E	Cs	Cs(12%)	E
UNITS	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
VALUE	118	0.001106	0.001776	0.0363	0.000220	0.000354	0.0085	0.001326	0.002130	0.0448

**TEST PARAMETERS:**

**OVERVIEW OF THE TEST**

**SAMPLING:** Failed

**LABORATORY:** Passed

The sampling data from this test is unacceptable and will not be used in the overall test average.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #1  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @	
				12% CO2	lbs/hr
Probe & Nozzle:	10.38	0.005581	0.005114	0.008330	0.2
Filter:	0.6	0.000322	0.000295	0.000481	0.01
Condensables:	1.173333	0.000630	0.000578	0.000941	0.02
Total:	12.15333	0.006534	0.005988	0.009753	0.23

N BaCl<sub>2</sub> = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @	
					12% CO2	lbs/hr
Probe & Nozzle:	25	0.2	0.001266	0.001160	0.001889	0.05
Filter:	10	0	0	0	0	0
Condensables:	22	0.1	0.000557	0.000510	0.000831	0.02
Total:			0.001823	0.001670	0.002721	0.07

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1030	1130	11.43	8.04	8.36	28.64	4174

Avg. of 3 runs: *exhaust flow rate* =  $\frac{4174 + 3874 + 4497}{3} = 4168$

$$\text{Concentration}(\text{SO}_2) = [\text{K} * \text{Normality} * \text{V-titrant} * (\text{V-solution} / \text{V-aliquot})] / \text{Vm}(\text{std})$$

### Calculations:

#### MISCELLANEOUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 % CO2 =  
 15.43 grains = 1 gram  
 7000 grains = 1 lb, 60 min = 1 hr; 60 min/hr / 7000 grains/lb =

SDAPCD	SCEC
--------	------

0.00971	0.00971	equiv/liter
28.64	28.64	dscf
4192	4174	dscfm
8.04	8.04	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

#### SO2:

MW =  
 # equiv/mole vs. BaCl2 =  
 K =

64.06 not done g/mole  
 2 not done equiv/mole  
 32.03 not done grams/equiv

#### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,front) =  $[K * N * Vt * (Vsoln / Valiquot)] / Vm(\text{std}) =$   
 Cs(SO2,front) = 15.43 \* Conc(SO2,front) =  
 Cs(SO2,12%,front) = Cs(SO2,front) \* (12/%CO2) =  
 E (SO2,front) = 0.00857 \* Qstd \* Cs(SO2,front) =

0.2	not done	ml
250	not done	ml
10	not done	ml
0.0000543	not done	grams/dscf
0.0008378	not done	grains/dscf
0.0012504	not done	grains/dscf
0.0301	not done	lbs/hr

#### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,filter) =  $[K * N * Vt * (Vsoln / Valiquot)] / Vm(\text{std}) =$   
 Cs(SO2,filter) = 15.43 \* Conc(SO2,filter) =  
 Cs(SO2,12%,filter) = Cs(SO2,filter) \* (12/%CO2) =  
 E (SO2,filter) = 0.00857 \* Qstd \* Cs(SO2,filter) =

0	not done	ml
250	not done	ml
10	not done	ml
0.0000000	not done	grams/dscf
0.0000000	not done	grains/dscf
0.0000000	not done	grains/dscf
0.0000	not done	lbs/hr

#### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,back) =  $[K * N * Vt * (Vsoln / Valiquot)] / Vm(\text{std}) =$   
 Cs(SO2,back) = 15.43 \* Conc(SO2,back) =  
 Cs(SO2,12%,back) = Cs(SO2,back) \* (12/%CO2) =  
 E (SO2,back) = 0.00857 \* Qstd \* Cs(SO2,back) =

0.1	not done	ml
250	not done	ml
10	not done	ml
0.0000271	not done	grams/dscf
0.0004189	not done	grains/dscf
0.0006252	not done	grains/dscf
0.0150	not done	lbs/hr

#### TOTAL SO2

Conc(SO2,total) =  $\sum \text{Conc}(\text{SO}_2, \text{location})$  = 0.0000814  
 Cs(SO2,total) =  $\sum \text{Cs}(\text{SO}_2, \text{location})$  = 0.0012567  
 Cs(SO2,12%,total) =  $\sum \text{Cs}(\text{SO}_2, 12\%, \text{location})$  = 0.0018757  
 E (SO2,total) =  $\sum \text{E}(\text{SO}_2, \text{location})$  = 0.0451

not done grams/dscf  
 not done grains/dscf  
 not done grains/dscf  
 not done lbs/hr

#### COMMENTS:

SCEC did not calculate the contribution due to SO2; so, the District will use the values generated by the District's spreadsheet.

$$\text{Concentration}(\text{H}_2\text{SO}_4) = [\text{K} \cdot \text{Normality} \cdot \text{V-titrant} \cdot (\text{V-solution} / \text{V-aliquot})] / \text{Vm} - (\text{std})$$

## CALCULATIONS:

### SCCELLANEOUS DATA

N = Normality =

Vmstd =

Qstd =

%CO2 =

15.43 grains = 1 gram

7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

### SO3 as H2SO4:

MW =

# equiv/mole vs. BaCl2 =

K =

### FRONT HALF

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(H2SO4,front) =  $[\text{K} \cdot \text{N} \cdot \text{Vt} \cdot (\text{Vsoln} / \text{Valiquot})] / \text{Vm}(\text{std}) =$

Cs(H2SO4,front) = 15.43 \* Conc(H2SO4,front) =

Cs(H2SO4,12%,front) = Cs(front) \* (12/%CO2) =

E (H2SO4,front) = 0.00857 \* Qstd \* Cs(H2SO4,front) =

### FILTER

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(H2SO4,filter) =  $[\text{K} \cdot \text{N} \cdot \text{Vt} \cdot (\text{Vsoln} / \text{Valiquot})] / \text{Vm}(\text{std}) =$

Cs(H2SO4,filter) = 15.43 \* Conc(H2SO4,filter) =

Cs(H2SO4,12%,filter) = Cs(filter) \* (12/%CO2) =

E (H2SO4,filter) = 0.00857 \* Qstd \* Cs(H2SO4,filter) =

### BACK HALF

Volume of the titrant = Vt

Volume of the solution = Vsoln =

Volume of the aliquot = Valiquot =

Conc(H2SO4,back) =  $[\text{K} \cdot \text{N} \cdot \text{Vt} \cdot (\text{Vsoln} / \text{Valiquot})] / \text{Vm}(\text{std}) =$

Cs(H2SO4,back) = 15.43 \* Conc(H2SO4,back) =

Cs(H2SO4,12%,back) = Cs(H2SO4,back) \* (12/%CO2) =

E (H2SO4,back) = 0.00857 \* Qstd \* Cs(H2SO4,back) =

### TOTAL SO3

Conc(H2SO4,total) =  $\sum \text{Conc}(\text{H}_2\text{SO}_4, \text{location})$

Cs(H2SO4,total) =  $\sum \text{Cs}(\text{H}_2\text{SO}_4, \text{location}) =$

Cs(H2SO4,12%,total) =  $\sum \text{Cs}(\text{H}_2\text{SO}_4, 12\%, \text{location}) =$

E (H2SO4,total) =  $\sum \text{E}(\text{H}_2\text{SO}_4, \text{location}) =$

SDAPCD	SCEC	
0.00971	0.00971	equiv/liter
28.64	28.64	dscf
4192	4174	dscfm
8.04	8.04	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

98.08

\*\* 97 g/mole

2

2 equiv/mole

49.04

48.5 grams/equiv

0.2	0.2	ml
250	250	ml
10	10	ml

0.0000831 0.0000822 grams/dscf

0.0012827 0.0012661 grains/dscf

0.0019145 0.0018897 grains/dscf

0.0461 0.0455 lbs/hr

0	0	ml
100	100	ml
10	10	ml

0.0000000 0.0000000 grams/dscf

0.0000000 0.0000000 grains/dscf

0.0000000 0.0000000 grains/dscf

0.0000 0.0000 lbs/hr

0.1	0.1	ml
220	220	ml
10	10	ml

0.0000366 0.0000362 grams/dscf

0.0005644 0.0005571 grains/dscf

0.0008424 0.0008315 grains/dscf

0.0203 0.0200 lbs/hr

0.0001184 grams/dscf

0.0018232 grains/dscf

0.0027212 grains/dscf

0.0655 lbs/hr

### COMMENTS:

\*\* SCEC used an incorrect molecular weight for H2SO4, and this gave incorrect values for all the subsequent numbers that SCEC generated in their final report.

The District will use the numbers generated by the District's spreadsheet, because these values are correct.

**Test Witness - Run #1 (SOx)**

**TEST RESULTS SUMMARY:**

ITEM	I	SO3			SO2			Total SOx		
		Cs	Cs(12%)	E	Cs	Cs(12%)	E	Cs	Cs(12%)	E
UNITS	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
VALUE	109	0.001847	0.002757	0.0664	0.001257	0.001876	0.0451	0.003104	0.004633	0.1115

**TEST PARAMETERS:**

**OVERVIEW OF THE TEST**

**SAMPLING:** Passed

**LABORATORY:** Passed

The data from this test is acceptable and will be used in the overall test average.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #1  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	10.38	0.005581	0.005114	0.008330	0.2
Filter:	0.6	0.000322	0.000295	0.000481	0.01
Condensables:	1.173333	0.000630	0.000578	0.000941	0.02
Total:	12.15333	0.006534	0.005988	0.009753	0.23

N BaCl<sub>2</sub> = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	25	0.2	0.001266	0.001160	0.001889	0.05
Filter:	10	0	0	0	0	0
Condensables:	22	0.1	0.000557	0.000510	0.000831	0.02
Total:			0.001823	0.001670	0.002721	0.07

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1030	1130	11.43	8.04	8.36	28.64	4174

$$\text{Concentration(SO}_2\text{)} = [K \cdot \text{Normality} \cdot V\text{-titrant} \cdot (V\text{-solution}/V\text{-aliquot})] / V_m\text{-std}$$

### Calculations:

#### MISCELLANEOUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 %CO2 =  
 15.43 grains = 1 gram  
 7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

#### SO2:

MW =  
 # equiv/mole vs. BaCl2 =  
 K =

#### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,front) =  $[K \cdot N \cdot V_t \cdot (V_{soln}/V_{aliquot})] / V_m(std) =$   
 Cs(SO2,front) = 15.43 \* Conc(SO2,front) =  
 Cs(SO2,12%,front) = Cs(SO2,front) \* (12/%CO2) =  
 E (SO2,front) = 0.00857 \* Qstd \* Cs(SO2,front) =

#### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,filter) =  $[K \cdot N \cdot V_t \cdot (V_{soln}/V_{aliquot})] / V_m(std) =$   
 Cs(SO2,filter) = 15.43 \* Conc(SO2,filter) =  
 Cs(SO2,12%,filter) = Cs(SO2,filter) \* (12/%CO2) =  
 E (SO2,filter) = 0.00857 \* Qstd \* Cs(SO2,filter) =

#### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(SO2,back) =  $[K \cdot N \cdot V_t \cdot (V_{soln}/V_{aliquot})] / V_m(std) =$   
 Cs(SO2,back) = 15.43 \* Conc(SO2,back) =  
 Cs(SO2,12%,back) = Cs(SO2,back) \* (12/%CO2) =  
 E (SO2,back) = 0.00857 \* Qstd \* Cs(SO2,back) =

#### TOTAL SO2

Conc(SO2,total) =  $\sum \text{Conc(SO2,location)}$  = 0.0000814  
 Cs(SO2,total) =  $\sum \text{Cs(SO2,location)}$  = 0.0012567  
 Cs(SO2,12%,total) =  $\sum \text{Cs(SO2,12%,location)}$  = 0.0018757  
 E (SO2,total) =  $\sum \text{E(SO2,location)}$  = 0.0451

SDAPCD	SCEC	
0.00971	0.00971	equiv/liter
28.64	28.64	dscf
4192	4174	dscfm
8.04	8.04	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr
64.06		not done g/mole
2		not done equiv/mole
32.03		not done grams/equiv

0.2	not done	ml
250	not done	ml
10	not done	ml
0.0000543		not done grams/dscf
0.0008378		not done grains/dscf
0.0012504		not done grains/dscf
0.0301		not done lbs/hr

0	not done	ml
250	not done	ml
10	not done	ml
0.0000000		not done grams/dscf
0.0000000		not done grains/dscf
0.0000000		not done grains/dscf
0.0000		not done lbs/hr

0.1	not done	ml
250	not done	ml
10	not done	ml
0.0000271		not done grams/dscf
0.0004189		not done grains/dscf
0.0006252		not done grains/dscf
0.0150		not done lbs/hr

not done grams/dscf  
 not done grains/dscf  
 not done grains/dscf  
 not done lbs/hr

#### COMMENTS:

SCEC did not calculate the contribution due to SO2; so, the District will use the values generated by the District's spreadsheet.

$$\text{Concentration(H}_2\text{SO}_4) = [K \cdot \text{Normality} \cdot V_{\text{-titrant}} \cdot (V_{\text{-solution}}/V_{\text{-aliquot}})]/V_{\text{m-(std)}}$$

### CALCULATIONS:

#### SCCELLANEOUS DATA

N = Normality =  
 Vmstd =  
 Qstd =  
 %CO2 =  
 15.43 grains = 1 gram  
 7000grains=1lb, 60min=1hr; 60min/hr/7000grains/lb=

#### S03 as H2SO4:

MW =  
 # equiv/mole vs. BaCl2 =  
 K =

#### FRONT HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,front) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  =  
 Cs(H2SO4,front) = 15.43 \* Conc(H2SO4,front) =  
 Cs(H2SO4,12%,front) = Cs(front) \* (12/%CO2) =  
 E (H2SO4,front) = 0.00857 \* Qstd \* Cs(H2SO4,front) =

#### FILTER

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,filter) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  =  
 Cs(H2SO4,filter) = 15.43 \* Conc(H2SO4,filter) =  
 Cs(H2SO4,12%,filter) = Cs(filter) \* (12/%CO2) =  
 E (H2SO4,filter) = 0.00857 \* Qstd \* Cs(H2SO4,filter) =

#### BACK HALF

Volume of the titrant = Vt  
 Volume of the solution = Vsoln =  
 Volume of the aliquot = Valiquot =  
 Conc(H2SO4,back) =  $[K \cdot N \cdot V_t \cdot (V_{\text{soln}}/V_{\text{aliquot}})]/V_{\text{m(std)}}$  =  
 Cs(H2SO4,back) = 15.43 \* Conc(H2SO4,back) =  
 Cs(H2SO4,12%,back) = Cs(H2SO4,back) \* (12/%CO2) =  
 E (H2SO4,back) = 0.00857 \* Qstd \* Cs(H2SO4,back) =

#### TOTAL S03

Conc(H2SO4,total) =  $\sum \text{Conc(H}_2\text{SO}_4, \text{location})$  =  
 Cs(H2SO4,total) =  $\sum \text{Cs(H}_2\text{SO}_4, \text{location})$  =  
 Cs(H2SO4,12%,total) =  $\sum \text{Cs(H}_2\text{SO}_4, 12\%, \text{location})$  =  
 E (H2SO4,total) =  $\sum \text{E(H}_2\text{SO}_4, \text{location})$  =

SDAPCD	SCEC
--------	------

0.00971	0.00971	equiv/liter
28.64	28.64	dscf
4192	4174	dscfm
8.04	8.04	%
15.43	15.4	grains/gram
0.00857	0.00857	lbs-min/grs-hr

98.08      \*\* 97 g/mole  
 2            2 equiv/mole  
 49.04      48.5 grams/equiv

0.2	0.2	ml
250	250	ml
10	10	ml
0.0000831	0.0000822	grams/dscf
0.0012827	0.0012661	grains/dscf
0.0019145	0.0018897	grains/dscf
0.0461	0.0455	lbs/hr

0	0	ml
100	100	ml
10	10	ml
0.0000000	0.0000000	grams/dscf
0.0000000	0.0000000	grains/dscf
0.0000000	0.0000000	grains/dscf
0.0000	0.0000	lbs/hr

0.1	0.1	ml
220	220	ml
10	10	ml
0.0000366	0.0000362	grams/dscf
0.0005644	0.0005571	grains/dscf
0.0008424	0.0008315	grains/dscf
0.0203	0.0200	lbs/hr

0.0001184 grams/dscf  
 0.0018232 grains/dscf  
 0.0027212 grains/dscf  
 0.0655 lbs/hr

#### COMMENTS:

\*\* SCEC used an incorrect molecular weight for H2SO4, and this gave incorrect values for all the subsequent numbers that SCEC generated in their final report.

The District will use the numbers generated by the District's spreadsheet, because these values are correct.

**Test Witness - Run #1 (SOx)**

**TEST RESULTS SUMMARY:**

ITEM	I	SO3			SO2			Total SOx		
		Cs	Cs(12%)	E	Cs	Cs(12%)	E	Cs	Cs(12%)	E
UNITS	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
VALUE	109	0.001847	0.002757	0.0664	0.001257	0.001876	0.0451	0.003164	0.004633	0.1115

**TEST PARAMETERS:**

**OVERVIEW OF THE TEST**

**SAMPLING:** Passed

**LABORATORY:** Passed

The data from this test is acceptable and will be used in the overall test average.

**SOURCE TEST OF OXIDES OF SULFUR EMISSIONS TO THE ATMOSPHERE**

**Test Witness - Average (SOx)**

**TEST RESULTS SUMMARY:**

ITEM	I	SO3			SO2			Total SOx		
		Cs	Cs(12%)	E	Cs	Cs(12%)	E	Cs	Cs(12%)	E
UNITS	%	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr	gr/dscf	gr/dscf	lbs/hr
VALUE	107	0.001733	0.002787	0.0643	0.001237	0.001996	0.0459	<b>0.002970</b>	<b>0.004782</b>	<b>0.1102</b>

**TEST PARAMETERS:**

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA NSPS guidelines and from the EPA CFR 40, Standards Method 8. The sampling utilized a front-end filter (fig. 1).

**CALCULATIONS:**

All calculations are based on the EPA CFR 40, July 1, 1991, Parts 53-60, Appendix A, Method 8.

**SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way, because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data, SCEC's as well as the District's, were transferred to the computer printout. All calculations were done by computer.

**ANALYSES:**

**Gas:** A CEM analysis was performed by SCEC.

**SOx:** All procedures follow EPA guidelines, except where noted in this report.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.

**OVERVIEW OF THE TEST:**

	RUN #1	RUN #2	RUN #3
<b>SAMPLING:</b>	Passed	Failed	Passed
<b>LABORATORY:</b>	Passed	Passed	Passed

Run #2 was eliminated from the overall test average because QA criteria were not met. (See the laboratory sheet of the particulate report for an in depth explanation.)

$$\text{Concentration(H}_2\text{SO}_4) = [K \cdot \text{Normality} \cdot V\text{-titrant} \cdot (V\text{-solution}/V\text{-aliquot})] / V_m\text{-(std)}$$

$$\text{Concentration(SO}_2) = [K \cdot \text{Normality} \cdot V\text{-titrant} \cdot (V\text{-solution}/V\text{-aliquot})] / V_m\text{-(std)}$$

$$K = \text{MW} / \# \text{equiv/mole}$$

**CALCULATIONS:**

**TOTAL SO3**

	SDAPCD RUN1	SDAPCD RUN 2	SDAPCD RUN 3	SDAPCD **AVG	
Conc(H <sub>2</sub> SO <sub>4</sub> ,total) = ΣConc(H <sub>2</sub> SO <sub>4</sub> ,location) =	0.0001197	0.0000846	0.0001050	0.0001124	grams/dscf
Cs(H <sub>2</sub> SO <sub>4</sub> ,total) = ΣCs(H <sub>2</sub> SO <sub>4</sub> ,location) =	0.0018471	0.0013046	0.0016195	0.0017333	grains/dscf
Cs(H <sub>2</sub> SO <sub>4</sub> ,12%,total) = ΣCs(H <sub>2</sub> SO <sub>4</sub> ,12%,location) =	0.0027569	0.0020958	0.0028165	0.0027867	grains/dscf
E (H <sub>2</sub> SO <sub>4</sub> ,total) = ΣE(H <sub>2</sub> SO <sub>4</sub> ,location) =	0.0664	0.0428	0.0621	0.0643	lbs/hr

**TOTAL SO2**

Conc(SO <sub>2</sub> ,total) = ΣConc(SO <sub>2</sub> ,location) =	0.0000814	0.0000169	0.0000788	0.0000801	grams/dscf
Cs(SO <sub>2</sub> ,total) = ΣCs(SO <sub>2</sub> ,location) =	0.0012567	0.0002601	0.0012163	0.0012365	grains/dscf
Cs(SO <sub>2</sub> ,12%,total) = ΣCs(SO <sub>2</sub> ,12%,location) =	0.0018757	0.0004179	0.0021154	0.0019956	grains/dscf
E (SO <sub>2</sub> ,total) = ΣE(SO <sub>2</sub> ,location) =	0.0451	0.0101	0.0467	0.0459	lbs/hr

**TOTAL SOx**

Conc(SOx,total) = Conc(H <sub>2</sub> SO <sub>4</sub> ,total)+Conc(SO <sub>2</sub> ,total) =	0.0002011	0.0001015	0.0001838	0.00019245	grams/dscf
Cs(SOx,total) = Cs(H <sub>2</sub> SO <sub>4</sub> ,total)+Cs(SO <sub>2</sub> ,total) =	0.0031038	0.0015647	0.00283583	0.00296982	grains/dscf
Cs(SO <sub>2</sub> ,12%,total) = Cs(H <sub>2</sub> SO <sub>4</sub> ,12%,total)+Cs(SO <sub>2</sub> ,12%,total) =	0.0046326	0.0025137	0.0049319	0.00478225	grains/dscf
E(SOx,total) = E(H <sub>2</sub> SO <sub>4</sub> ,total)+E(SO <sub>2</sub> ,total) =	0.1115	0.0529	0.1088	0.11015	lbs/hr

\*\* Run #2 is eliminated from the overall test average





Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: N/A

PAI Sample ID: PAI Method Blank

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Today

Matrix: Summa Canister  
Date Received: N/A  
Date Analyzed: 04/14/92  
Volume Analyzed: 1.00 Liter

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	ND	5.0	ND	2.0
75-09-2	METHYLENE CHLORIDE	ND	5.0	ND	1.5
67-66-3	CHLOROFORM	ND	5.0	ND	1.0
107-06-2	1,2-DICHLOROETHANE	ND	5.0	ND	1.2
71-55-6	1,1,1-TRICHLOROETHANE	ND	5.0	ND	0.93
71-43-2	BENZENE	ND	5.0	ND	1.6
56-23-5	CARBON TETRACHLORIDE	ND	5.0	ND	0.80
79-01-6	TRICHLOROETHENE	ND	5.0	ND	0.94
106-93-4	1,2-DIBROMOETHANE	ND	5.0	ND	0.65
127-18-4	TETRACHLOROETHENE	ND	5.0	ND	0.75

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



**Performance Analytical Inc.**  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #1 (04/07/92) (2:50)

PAI Sample ID: 9201624

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tудay

Matrix: Summa Canister  
Date Received: 04/09/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.050 ml  
P<sub>i</sub> = -0.4 P<sub>f</sub> = +2.1 DF = 1.17

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	190000	25
C2 as Ethane	ND	25
C3 as n-Propane	ND	20
C4 as n-Butane	ND	15
C5 as Pentane	ND	10
C6 as n-Hexane	ND	10
C7 as n-Heptane	ND	10
C8 as n-Octane	ND	10
C9 as n-Nonane	ND	10
> C9 as n-Nonane	ND	10

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: N/A

PAI Sample ID: PAI Method Blank

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: N/A  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	ND	0.50
C2 as Ethane	ND	0.50
C3 as n-Propane	ND	0.40
C4 as n-Butane	ND	0.30
C5 as Pentane	ND	0.20
C6 as n-Hexane	ND	0.20
C7 as n-Heptane	ND	0.20
C8 as n-Octane	ND	0.20
C9 as n-Nonane	ND	0.20
> C9 as n-Nonane	ND	0.20

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

Bell

LABORATORY REPORT

Client:	SAN DIEGO AIR POLLUTION CONTROL DISTRICT	Date of Report:	04/27/92
Address:	9150 Chesapeake Drive San Diego, CA 92123	Date Received:	04/09/92
Contact:	Ms. Judy Lake	PAI Project No:	4081
Client Project:	Bell Jr. High School #T-1483	Purchase Order:	Verbal

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Two (2) Stainless Steel "SUMMA" Polished Canisters labeled: "Inlet #1" and "Outlet #1"

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The samples were received at the laboratory under chain of custody on April 9, 1992. The samples were received intact. The dates of analysis are indicated on the data sheets.

C1 through >C9 Hydrocarbon Analysis

The samples were analyzed for C<sub>1</sub> through >C<sub>9</sub> Hydrocarbons by direct injection GC/FID. The analytical system consisted of a Hewlett-Packard model 5890A gas chromatograph equipped with a flame ionization detector. Separation was achieved using a Restek Rt<sub>x</sub>-1 megabore column, 60 meters long by 0.53 mm I.D., with a 5.0 um film thickness.

A four point standard calibration was performed using a certified gas standard mix (Scott Speciality Gases) prior to analysis of the field samples.

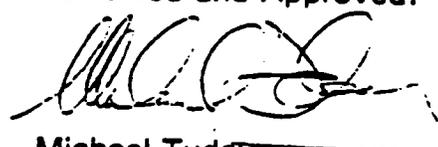
Volatile Organic Compound Analysis

The samples were also analyzed by combined gas chromatography/mass spectrometry (GC/MS) for ten Volatile Organic Compounds. The analyses were performed according to the methodology outlined in EPA Method TO-14 from the Compendium of Methods for the Determination of Toxic Organic Compounds in Ambient Air, EPA 600/4-84-041, U.S. Environmental Protection Agency, Research Triangle Park, NC, April, 1984 and May, 1988. The analyses were performed by gas chromatography/mass spectrometry, utilizing a direct cryogenic trapping technique. The analytical system used was comprised of a Finnigan Model 4500C GC/MS/DS interfaced to a Tekmar 5010 Automatic Desorber. A thick film (5 micron) crossbonded 100% Dimethyl polysiloxane megabore column (RT<sub>x</sub>-1, Restek Corporation, Bellefonte, PA) was used to achieve chromatographic separation.

Data Release Authorization:

Reviewed and Approved:

  
Ku-jih Chen  
Principal Chemist

  
Michael Tuday  
Laboratory Director



**Performance Analytical Inc.**  
Environmental Testing and Consulting

20954 Chhome Street  
Canoga Park, California 91304  
Phone 818 709-1139  
Fax 818 709-2915

**Chain of Custody Record**  
Analytical Services Request

Client/Project Name  
S.D.A.P.C.D. 96 S.C.E.C.

Address/Phone  
(714) 282-8240  
Client Project No.

ANALYSES:

PAI Project No.  
4060

Project Location  
Bell St. High School

Contact  
Russ Logan

Sample (Signature)  
*[Signature]*

P.O. No.

Sample Identification No.

Date

Time

Lab Sample No.

Type of Sample

CALDERON'S  
ROB'S

Expected Turnaround Time

Remarks

Taken #1

3-31-92

9201457

P.O.C.

X

00112

" #2

"

9201458

"

X

00080

" #5

"

9201459

n

X

00103

OSTAG #1

"

9201460

"

X

00029

" #2

"

9201461

"

X

00123

" #3 - Backup

"

9201462

"

X

00113

See Note Friday  
re: conversation  
w/ Judy Lake

labeled 00017

Relinquished by: (Signature)

Date

Time

Received by: (Signature)

Date

Time

Relinquished by: (Signature)

Date

Time

Received by: (Signature)

Date

Time

Relinquished by: (Signature)

Date

Time

Received by: (Signature)

Date

Time

Disposal Method

Disposed by: (Signature)

Date

Time

White Copy : Accompanies Samples

Yellow Copy : Sampler

*[Signature]*

*[Signature]*

4/2/92 10:30



Performance Analytical Inc.  
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RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #3 (03/31/92)

PAI Sample ID: 9201459 (Laboratory Duplicate)

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.050 ml  
 $P_i = -9.1$   $P_f = +4.0$   $DF = 3.34$

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	160000	75
C2 as Ethane	ND	75
C3 as n-Propane	ND	60
C4 as n-Butane	ND	45
C5 as Pentane	ND	30
C6 as n-Hexane	ND	30
C7 as n-Heptane	ND	30
C8 as n-Octane	ND	30
C9 as n-Nonane	ND	30
> C9 as n-Nonane	ND	30

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



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RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: N/A

PAI Sample ID: PAI Method Blank

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: N/A  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	ND	0.50
C2 as Ethane	ND	0.50
C3 as n-Propane	ND	0.40
C4 as n-Butane	ND	0.30
C5 as Pentane	ND	0.20
C6 as n-Hexane	ND	0.20
C7 as n-Heptane	ND	0.20
C8 as n-Octane	ND	0.20
C9 as n-Nonane	ND	0.20
> C9 as n-Nonane	ND	0.20

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



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### C1 through >C9 Hydrocarbon Analysis

The samples were analyzed for C<sub>1</sub> through >C<sub>9</sub> Hydrocarbons by direct injection GC/FID. The analytical system consisted of a Hewlett-Packard model 5890A gas chromatograph equipped with a flame ionization detector. Separation was achieved using a Restek Rt<sub>x</sub>-1 megabore column, 60 meters long by 0.53 mm I.D., with a 5.0 um film thickness.

A four point standard calibration was performed using a certified gas standard mix (Scott Speciality Gases) prior to analysis of the field samples.

### Volatile Organic Compound Analysis

The samples were also analyzed by combined gas chromatography/mass spectrometry (GC/MS) for ten Volatile Organic Compounds. The analyses were performed according to the methodology outlined in EPA Method TO-14 from the Compendium of Methods for the Determination of Toxic Organic Compounds in Ambient Air, EPA 600/4-84-041, U.S. Environmental Protection Agency, Research Triangle Park, NC, April, 1984 and May, 1988. The analyses were performed by gas chromatography/mass spectrometry, utilizing a direct cryogenic trapping technique. The analytical system used was comprised of a Finnigan Model 4500C GC/MS/DS interfaced to a Tekmar 5010 Automatic Desorber. A thick film (5 micron) crossbonded 100% Dimethyl polysiloxane megabore column (RT<sub>x</sub>-1, Restek Corporation, Bellefonte, PA) was used to achieve chromatographic separation.

The results of the analyses are included on the attached data sheets.



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 Environmental Testing and Consulting

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**LABORATORY REPORT**

Client: SAN DIEGO AIR POLLUTION CONTROL DISTRICT	Date of Report: 04/21/92
Address: 9150 Chesapeake Drive San Diego, CA 92123	Date Received: 04/02/92
Contact: Ms. Judy Lake	PAI Project No: 4060,4061
Client Project: Arizona Street & Bell Jr. High School	Purchase Order: Verbal

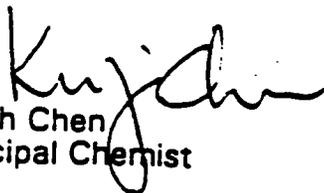
Twelve (12) Stainless Steel "SUMMA" Polished Canisters labeled:  
 "Inlet #1 (03/30/92)" "Inlet #2 (03/30/92)" "Inlet #3 (03/30/92)"  
 "Outlet #1 (03/30/92)" "Outlet #2 (03/30/92)" "Outlet #3 (03/30/92)"  
 "Inlet #1 (03/31/92)" "Inlet #2 (03/31/92)" "Inlet #3 (03/31/92)"  
 "Outlet #1 (03/31/92)" "Outlet #2 (03/31/92)" "Outlet #3 (03/31/92)"

The samples were received at the laboratory under chain of custody on April 2, 1992. The samples were received intact. The dates of analysis are indicated on the data sheets.

Twelve (12) six-liter passivated canisters were sent directly to the field sampler along with variable-constant differential low volume flow controllers. At the request of the sampler the flow controllers were calibrated to take one-hour time integrated samples. The majority of the canisters received by the laboratory were significantly undersampled. Ten of twelve canisters submitted to the laboratory were received under a unusually high vacuum. Canisters are evacuated to -14.0 psig at the laboratory prior to being sent out into the field. After time integrated sampling is completed, canisters returned to the laboratory generally have vacuum readings ranging from -2.5 psig to -0.5 psig. The ten canisters had vacuum readings of -12.5 psig to -8.9 psig, corresponding to sample volumes of 0.9 to 2.4 liters in a 6-liter container. In order to draw aliquots out of the canisters, the samples had to be pressurized with Nitrogen prior to laboratory analysis. The dilution factor due to the Nitrogen pressurization ranged from 3.22 to 8.50, thereby resulting in detection limits that are significantly higher than would otherwise be detected.

Data Release Authorization:

Reviewed and Approved:

  
 Ku-jih Chen  
 Principal Chemist

  
 Michael Tuday  
 Laboratory Director



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #1 (04/07/92) (2:55)

PAI Sample ID: 9201625

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/09/92  
Date Analyzed: 04/14/92  
Volume Analyzed: 0.0050 Liter  
P<sub>i</sub> = -5.3 P<sub>f</sub> = +1.9 DF= 1.77  
P<sub>i</sub> = -0.6 P<sub>f</sub> = +0.8 DF= 1.10

CAS #	COMPOUND	RESULT (MG/M <sup>3</sup> )	DETECTION LIMIT (MG/M <sup>3</sup> )	RESULT (PPM)	DETECTION LIMIT (PPM)
75-01-4	VINYL CHLORIDE	ND	2.0	ND	0.79
75-09-2	METHYLENE CHLORIDE	ND	2.0	ND	0.58
67-66-3	CHLOROFORM	ND	2.0	ND	0.41
107-06-2	1,2-DICHLOROETHANE	ND	2.0	ND	0.50
71-55-6	1,1,1-TRICHLOROETHANE	ND	2.0	ND	0.37
71-43-2	BENZENE	ND	2.0	ND	0.63
56-23-5	CARBON TETRACHLORIDE	ND	2.0	ND	0.32
79-01-6	TRICHLOROETHENE	ND	2.0	ND	0.38
106-93-4	1,2-DIBROMOETHANE	ND	2.0	ND	0.26
127-18-4	TETRACHLOROETHENE	ND	2.0	ND	0.30

ND = Not Detected .TR = Trace Level - Below Indicated Detection Limit



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Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #1 (04/07/92) (2:50)

PAI Sample ID: 9201624

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/09/92  
Date Analyzed: 04/14/92  
Volume Analyzed: 0.0050 Liter  
 $P_i = -0.4$   $P_f = +2.1$   $DF = 1.17$

CAS #	COMPOUND	RESULT (MG/M <sup>3</sup> )	DETECTION LIMIT (MG/M <sup>3</sup> )	RESULT (PPM)	DETECTION LIMIT (PPM)
75-01-4	VINYL CHLORIDE	ND	1.0	ND	0.39
75-09-2	METHYLENE CHLORIDE	1.8	1.0	0.54	0.29
67-66-3	CHLOROFORM	ND	1.0	ND	0.21
107-06-2	1,2-DICHLOROETHANE	ND	1.0	ND	0.25
71-55-6	1,1,1-TRICHLOROETHANE	ND	1.0	ND	0.19
71-43-2	BENZENE	2.2	1.0	0.68	0.31
56-23-5	CARBON TETRACHLORIDE	ND	1.0	ND	0.16
79-01-6	TRICHLOROETHENE	7.8	1.0	1.5	0.19
106-93-4	1,2-DIBROMOETHANE	ND	1.0	ND	0.13
127-18-4	TETRACHLOROETHENE	12	1.0	1.8	0.15

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



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PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #1 (04/07/92) (2:55)

PAI Sample ID: 9201625

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: 04/09/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml  
 $P_i = -5.3$   $P_f = +1.9$   $DF = 1.77$

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	43	1.0
C2 as Ethane	ND	1.0
C3 as n-Propane	ND	0.80
C4 as n-Butane	ND	0.60
C5 as Pentane	540	0.40
C6 as n-Hexane	ND	0.40
C7 as n-Heptane	ND	0.40
C8 as n-Octane	ND	0.40
C9 as n-Nonane	ND	0.40
> C9 as n-Nonane	ND	0.40

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



**Performance Analytical Inc.**  
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**PERFORMANCE ANALYTICAL INC.**

**RESULTS OF ANALYSIS**

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #1 (04/07/92) (2:50)

PAI Sample ID: 9201624 (Laboratory Duplicate)

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Today

Matrix: Summa Canister  
Date Received: 04/09/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.050 ml  
P<sub>i</sub> = -0.4 P<sub>f</sub> = +2.1 DF = 1.17

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	190000	25
C2 as Ethane	ND	25
C3 as n-Propane	ND	20
C4 as n-Butane	ND	15
C5 as Pentane	ND	10
C6 as n-Hexane	ND	10
C7 as n-Heptane	ND	10
C8 as n-Octane	ND	10
C9 as n-Nonane	ND	10
> C9 as n-Nonane	ND	10

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



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RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #3 (03/31/92)

PAI Sample ID: 9201462

Test Code: GC/MS EPA TO-14  
 Analyst: Kathleen Aguilera  
 Instrument ID: Finnigan 4500C/Tekmar 5010  
 Verified by: Michael Tuday

Matrix: Summa Canister  
 Date Received: 04/02/92  
 Date Analyzed: 04/07/92  
 Volume Analyzed: 1.00 Liter  
 P<sub>i</sub> = -11.1 P<sub>f</sub> = +4.0 DF = 5.19

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	ND	25	ND	9.9
75-09-2	METHYLENE CHLORIDE	ND	25	ND	7.3
67-66-3	CHLOROFORM	ND	25	ND	5.2
107-06-2	1,2-DICHLOROETHANE	ND	25	ND	6.2
71-55-6	1,1,1-TRICHLOROETHANE	ND	25	ND	4.6
71-43-2	BENZENE	54	25	17	7.8
56-23-5	CARBON TETRACHLORIDE	ND	25	ND	4.0
79-01-6	TRICHLOROETHENE	ND	25	ND	4.7
106-93-4	1,2-DIBROMOETHANE	ND	25	ND	3.3
127-18-4	TETRACHLOROETHENE	520	25	77	3.7

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



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Sample "Outlet #1" contained 1500 ppm of Acetone. Acetone is not a target compound. The presence of Acetone is most likely attributable to the cleaning or rinsing of sampling equipment by the field sampler. The presence of Acetone interferes with the analysis of speciated VOCs by GC/MS. Due to the high concentration of Acetone the sample had to be analyzed at a smaller volume resulting in an elevated detection limit. Also, the Acetone artifact gave a 540 ppm false positive for Pentane for the EPA Method 18 GC/FID analysis.

The results of the analyses are included on the attached data sheets.

Outlet #1 test 4/11/92 is Outlet #4



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PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #3 (03/31/92)

PAI Sample ID: 9201462

*Ex 10 et #3*

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml  
P<sub>i</sub> = -1.1 P<sub>f</sub> = +4.0 DF = 5.19

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	ND	2.5
C2 as Ethane	ND	2.5
C3 as n-Propane	ND	2.0
C4 as n-Butane	ND	1.5
C5 as Pentane	ND	1.0
C6 as n-Hexane	ND	1.0
C7 as n-Heptane	ND	1.0
C8 as n-Octane	ND	1.0
C9 as n-Nonane	ND	1.0
> C9 as n-Nonane	ND	1.0

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #3 (03/31/92)

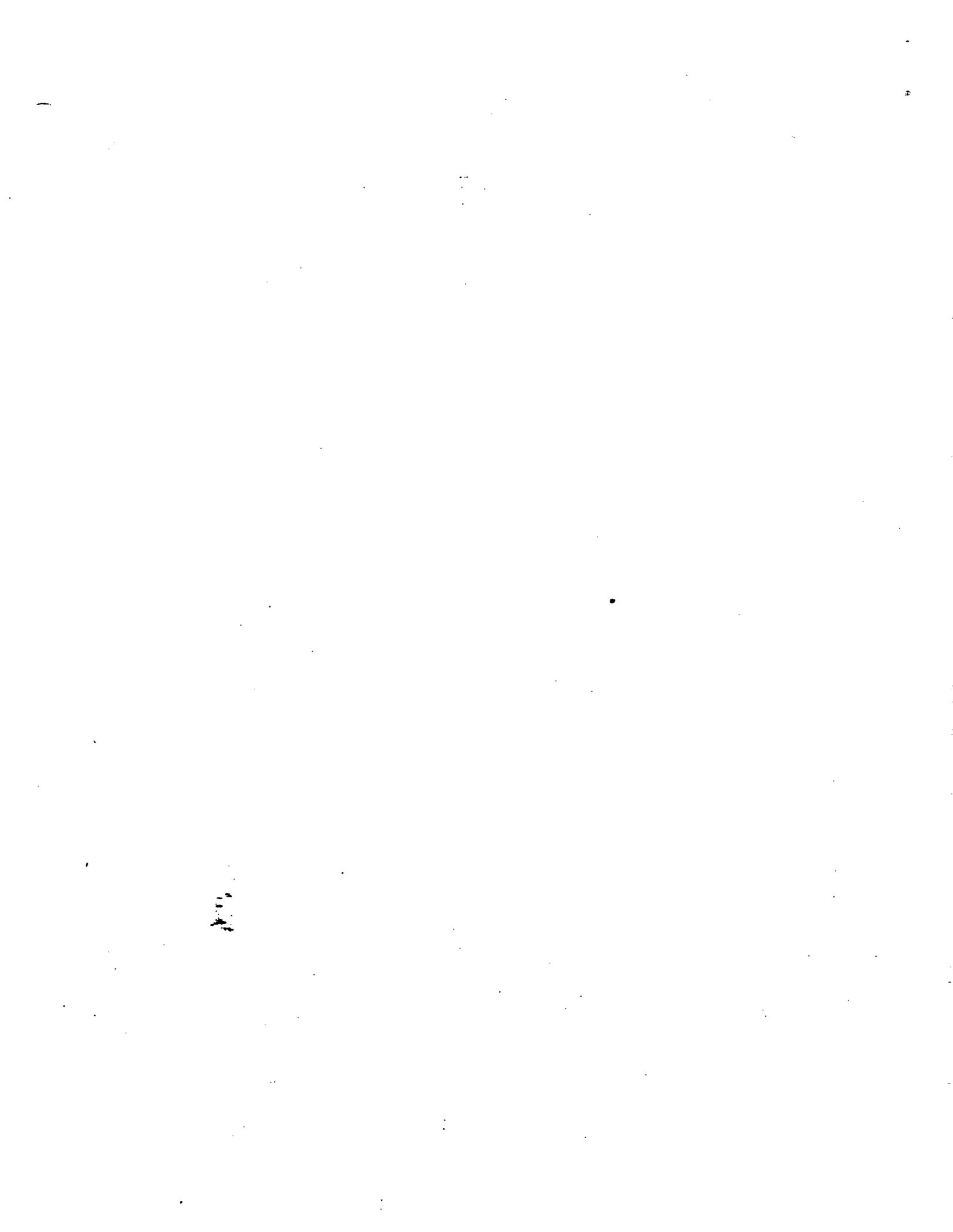
PAI Sample ID: 9201459

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/08/92  
Volume Analyzed: 0.050 Liter  
 $P_i = -9.1$   $P_f = +4.0$   $DF = 3.34$

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	750	300	300	120
75-09-2	METHYLENE CHLORIDE	2400	300	690	87
67-66-3	CHLOROFORM	ND	300	ND	62
107-06-2	1,2-DICHLOROETHANE	ND	300	ND	75
71-55-6	1,1,1-TRICHLOROETHANE	1200	300	230	56
71-43-2	BENZENE	2300	300	740	94
56-23-5	CARBON TETRACHLORIDE	ND	300	ND	48
79-01-6	TRICHLOROETHENE	9200	300	1700	56
106-93-4	1,2-DIBROMOETHANE	ND	300	ND	39
127-18-4	TETRACHLOROETHENE	15000	300	2300	45

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit





Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #3 (03/31/92)

PAI Sample ID: 9201459 Bell Inlet #3

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tудay

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.050 ml  
P<sub>i</sub> = -9.1 P<sub>f</sub> = +4.0 DF = 3.34

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	160000	75
C2 as Ethane	ND	75
C3 as n-Propane	ND	60
C4 as n-Butane	ND	45
C5 as Pentane	ND	30
C6 as n-Hexane	ND	30
C7 as n-Heptane	ND	30
C8 as n-Octane	ND	30
C9 as n-Nonane	ND	30
> C9 as n-Nonane	ND	30

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



**Performance Analytical Inc.**  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #2 (03/31/92)

PAI Sample ID: 9201458

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/08/92  
Volume Analyzed: 0.050 Liter  
P<sub>i</sub> = -8.9 P<sub>f</sub> = +4.0 DF = 3.22

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	1100	300	430	120
75-09-2	METHYLENE CHLORIDE	2500	300	740	87
67-66-3	CHLOROFORM	ND	300	ND	62
107-06-2	1,2-DICHLOROETHANE	ND	300	ND	75
71-55-6	1,1,1-TRICHLOROETHANE	780	300	140	56
71-43-2	BENZENE	2200	300	680	94
56-23-5	CARBON TETRACHLORIDE	ND	300	ND	48
79-01-6	TRICHLOROETHENE	8300	300	1600	56
106-93-4	1,2-DIBROMOETHANE	ND	300	ND	39
127-18-4	TETRACHLOROETHENE	12000	300	1900	45

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #2 (03/31/92)

PAI Sample ID: 9201461

Test Code: GC/MS EPA TO-14  
Analyst: Kathleen Aguilera  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Today

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/07/92  
Volume Analyzed: 1.00 Liter  
P<sub>i</sub> = -10.7 P<sub>f</sub> = +4.0 DF = 4.68

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	ND	25	ND	9.9
75-09-2	METHYLENE CHLORIDE	ND	25	ND	7.3
67-66-3	CHLOROFORM	ND	25	ND	5.2
107-06-2	1,2-DICHLOROETHANE	ND	25	ND	6.2
71-55-6	1,1,1-TRICHLOROETHANE	ND	25	ND	4.6
71-43-2	BENZENE	15 TR	25	4.7 TR	7.8
56-23-5	CARBON TETRACHLORIDE	ND	25	ND	4.0
79-01-6	TRICHLOROETHENE	ND	25	ND	4.7
106-93-4	1,2-DIBROMOETHANE	ND	25	ND	3.3
127-18-4	TETRACHLOROETHENE	150	25	22	3.7

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



**Performance Analytical Inc.**  
Environmental Testing and Consulting

**PERFORMANCE ANALYTICAL INC.**

**RESULTS OF ANALYSIS**

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #2 (03/31/92)

PAI Sample ID: 9201458 Inlet #2

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HPS890/FID #4  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.10 ml  
P<sub>i</sub> = -8.9 P<sub>f</sub> = +4.0 DF = 3.22

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	370000	38
C2 as Ethane	ND	38
C3 as n-Propane	ND	30
C4 as n-Butane	ND	23
C5 as Pentane	ND	15
C6 as n-Hexane	ND	15
C7 as n-Heptane	ND	15
C8 as n-Octane	ND	15
C9 as n-Nonane	ND	15
> C9 as n-Nonane	ND	15

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #2 (03/31/92)

PAI Sample ID: 9201461

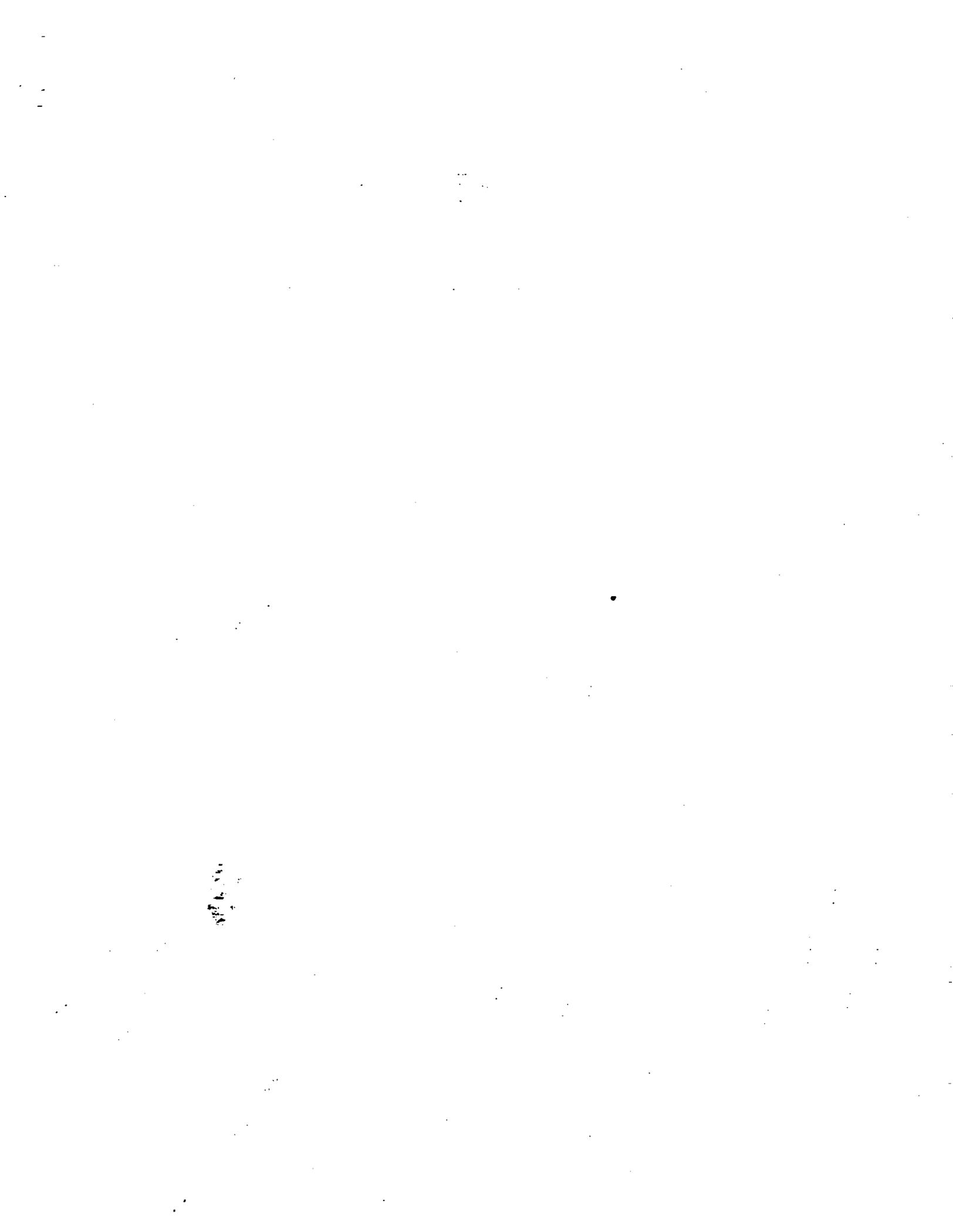
*PAI Outlet #2*

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml  
 $P_i = -10.7$   $P_f = +4.0$   $DF = 4.68$

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	ND	2.5
C2 as Ethane	ND	2.5
C3 as n-Propane	ND	2.0
C4 as n-Butane	ND	1.5
C5 as Pentane	ND	1.0
C6 as n-Hexane	ND	1.0
C7 as n-Heptane	ND	1.0
C8 as n-Octane	ND	1.0
C9 as n-Nonane	ND	1.0
> C9 as n-Nonane	ND	1.0

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit





**Performance Analytical Inc.**  
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**RESULTS OF ANALYSIS**

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #1 (03/31/92)

PAI Sample ID: 9201460

Test Code: GC/MS EPA TO-14  
Analyst: Kathleen Aguilera  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Taday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/07/92  
Volume Analyzed: 1.00 Liter  
P<sub>i</sub> = -0.5 P<sub>f</sub> = +4.0 DF = 1.32

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	ND	5.0	ND	2.0
75-09-2	METHYLENE CHLORIDE	ND	5.0	ND	1.5
67-66-3	CHLOROFORM	ND	5.0	ND	1.0
107-06-2	1,2-DICHLOROETHANE	ND	5.0	ND	1.2
71-55-6	1,1,1-TRICHLOROETHANE	ND	5.0	ND	0.93
71-43-2	BENZENE	5.2	5.0	1.6	1.6
56-23-5	CARBON TETRACHLORIDE	ND	5.0	ND	0.80
79-01-6	TRICHLOROETHENE	ND	5.0	ND	0.94
106-93-4	1,2-DIBROMOETHANE	ND	5.0	ND	0.65
127-18-4	TETRACHLOROETHENE	44	5.0	6.5	0.75

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Outlet #1 (03/31/92)

PAI Sample ID: 9201460

*Be: outlet #1*

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tудay

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 2.5 ml  
 $P_i = -0.5$   $P_f = +4.0$   $DF = 1.32$

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	4.0	0.50
C2 as Ethane	ND	0.50
C3 as n-Propane	ND	0.40
C4 as n-Butane	ND	0.30
C5 as Pentane	ND	0.20
C6 as n-Hexane	ND	0.20
C7 as n-Heptane	ND	0.20
C8 as n-Octane	ND	0.20
C9 as n-Nonane	ND	0.20
> C9 as n-Nonane	ND	0.20

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit



Performance Analytical Inc.  
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #1 (03/31/92)

PAI Sample ID: 9201457

Test Code: GC/MS EPA TO-14  
Analyst: Chris Parnell  
Instrument ID: Finnigan 4500C/Tekmar 5010  
Verified by: Michael Today

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/08/92  
Volume Analyzed: 0.050 Liter  
P<sub>i</sub> = -10.2 P<sub>f</sub> = +4.0 DF = 4.16

CAS #	COMPOUND	RESULT (UG/M <sup>3</sup> )	DETECTION LIMIT (UG/M <sup>3</sup> )	RESULT (PPB)	DETECTION LIMIT (PPB)
75-01-4	VINYL CHLORIDE	860	400	340	160
75-09-2	METHYLENE CHLORIDE	2300	400	680	120
67-66-3	CHLOROFORM	ND	400	ND	83
107-06-2	1,2-DICHLOROETHANE	ND	400	ND	100
71-55-6	1,1,1-TRICHLOROETHANE	1400	400	260	74
71-43-2	BENZENE	2200	400	680	130
56-23-5	CARBON TETRACHLORIDE	ND	400	ND	64
79-01-6	TRICHLOROETHENE	8500	400	1600	75
106-93-4	1,2-DIBROMOETHANE	ND	400	ND	52
127-18-4	TETRACHLOROETHENE	14000	400	2100	60

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit

# **GAS CHROMATOGRAPHY RESULTS**



**Performance Analytical Inc.**  
Environmental Testing and Consulting

**PERFORMANCE ANALYTICAL INC.**

**RESULTS OF ANALYSIS**

Client: San Diego Air Pollution Control District

Client Sample ID: Inlet #1 (03/31/92)

PAI Sample ID: 9201457 *Cell Inlet #1*

Test Code: EPA 18  
Analyst: Ku-Jih Chen  
Instrument ID: HP5890/FID #4  
Verified by: Michael Tuday

Matrix: Summa Canister  
Date Received: 04/02/92  
Date Analyzed: 04/10/92  
Volume Analyzed: 0.10 ml  
 $P_i = -10.2$   $P_f = +4.0$   $DF = 4.16$

COMPOUND	RESULT (PPM)	DETECTION LIMIT (PPM)
C1 as Methane	230000	50
C2 as Ethane	ND	50
C3 as n-Propane	ND	40
C4 as n-Butane	ND	30
C5 as Pentane	ND	20
C6 as n-Hexane	ND	20
C7 as n-Heptane	ND	20
C8 as n-Octane	ND	20
C9 as n-Nonane.	ND	20
> C9 as n-Nonane	ND	20

ND = Not Detected TR = Trace Level - Below Indicated Detection Limit

## Test Witness - Runs #1 - 4 GC Analysis

### TEST PARAMETERS:

#### PROCEDURES:

Procedures and equipment utilized in these tests are based on EPA NSPS guidelines and from the EPA 40 CFR PART 60, Method 18.

#### CALCULATIONS:

All calculations are based on the EPA 40 CFR, July 1, 1991, Part 60, Method 18.

#### GAS SAMPLING:

All samples were collected by SCEC. Their procedures are as follows:

A pressurized container was placed at the gas inlet BEFORE the flare. The container was opened after the flare reached a steady state. Once at a steady state, the container drew in the landfill gas for 25 minutes. After 25 minutes, the container was shut off, labeled, and shipped to Performance Analytical Inc. The outlet monitoring was run concurrently and parallel to the Method 20 sampling train. The pressurized container was opened and allowed to draw in the outlet gas for 25 minutes. The container was then shut off, labeled and shipped to Performance Analytical Inc.

#### ANALYSES:

All analyses were performed by Performance Analytical Inc.

#### EQUIPMENT:

All G.C. testing and analysis equipment was calibrated according to EPA guidelines and performed by Performance Analytical Inc.

#### OVERVIEW OF THE TEST:

**RUN #1:**        *INLET:* Accepted  
                  *OUTLET:* Accepted

**RUN #2:**        *INLET:* Accepted  
                  *OUTLET:* Accepted

**RUN #3:**        *INLET:* Accepted  
                  *OUTLET:* Accepted

**RUN #4:**        *INLET:* Not Accepted  
                  *OUTLET:* Not Accepted

	INLET #1		OUTLET #1		INLET #2		OUTLET #2		INLET #3		OUTLET #3	
	RESULT (PPM)	DET. LIMIT (PPM)										
C1 as Methane	230000	50	4.0	0.5	370000	38	ND	2.5	160000	75	ND	2.5
C2 as Ethane	ND	40	ND	0.5	ND	30	ND	2.5	ND	75	ND	2.5
C3 as n-Propane	ND	40	ND	0.4	ND	30	ND	2.0	ND	60	ND	2.0
C4 as n-Butane	ND	30	ND	0.5	ND	23	ND	1.5	ND	45	ND	1.5
C5 as Pentane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
C6 as n-Hexane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
C7 as n-Heptane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
C8 as n-Octane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
C9 as n-Nonane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
> C9 as n-Nonane	ND	20	ND	0.2	ND	15	ND	1.0	ND	30	ND	1.0
	RESULT (PPB)	DET. LIMIT (PPB)										
Vinyl Chloride	340	160	ND	2.0	430	120	ND	9.9	300	120	ND	9.9
Methylene Chloride	660	120	ND	1.5	740	87	ND	7.5	660	87	ND	7.3
Chloroform	ND	83	ND	1.0	ND	62	ND	5.2	ND	62	ND	5.2
1,2-Dichloroethane	ND	100	ND	1.2	ND	75	ND	6.2	ND	75	ND	6.2
1,1,1-Trichloroethane	260	74	ND	0.9	140	56	ND	4.6	230	56	ND	4.6
Benzene	660	150	1.6	1.6	660	94	4.7 TR	7.8	740	94	17	7.8
Carbon Tetrachloride	ND	64	ND	0.8	ND	48	ND	4.0	ND	48	ND	4.0
Trichloroethane	1800	75	ND	0.9	1600	56	ND	4.7	1700	56	ND	4.7
1,2-Dibromoethane	ND	52	ND	0.7	ND	39	ND	3.3	ND	39	ND	3.3
Tetrachloroethane	2100	60	ND	0.8	1900	45	22	3.7	2300	45	77	3.7

	AVERAGE INLET		AVERAGE OUTLET	
	RESULT (PPM)	DET. LIMIT (PPM)	RESULT (PPM)	DET. LIMIT (PPM)
C1 as Methane	253333	54	1	1.8
C2 as Ethane	ND	54	ND	1.5
C3 as n-Propane	ND	43	ND	1.5
C4 as n-Butane	ND	33	ND	1.1
C5 as Pentane	ND	22	ND	0.7
C6 as n-Hexane	ND	22	ND	0.7
C7 as n-Heptane	ND	22	ND	0.7
C8 as n-Octane	ND	22	ND	0.7
C9 as n-Nonane	ND	22	ND	0.7
> C9 as n-Nonane	ND	22	ND	0.7
	RESULT (PPB)	DET. LIMIT (PPB)	RESULT (PPB)	DET. LIMIT (PPB)
Vinyl Chloride	357	133	ND	7.3
Methylene Chloride	703	98	ND	4.4
Chloroform	ND	69	ND	3.8
1,2-Dichloroethane	ND	83	ND	3.5
1,1,1-Trichloroethane	210	62	ND	3.4
Benzene	700	100	6	7.7
Carbon Tetrachloride	ND	53	ND	2.9
Trichloroethane	1633	62	ND	3.4
1,2-Dibromoethane	ND	43	ND	2.4
Tetrachloroethane	2100	60	ND	2.7

### LEGEND

ND= Not Detected

TR= Trace Level (below the indicated detection limit)

### SAMPLE HISTORY

#### SAMPLES 1-3 INLET & OUTLET

Samples 1-3 INLET and OUTLET were taken on 3/31/92,

received on 4/2/92,

analyzed on 4/10/92.

#### SAMPLE 4 INLET & OUTLET

Sample 4 INLET and OUTLET was taken on 4/7/92,

received on 4/9/92,

analyzed 4/14/92

The G.C. detection limits for Run #4 were set too high; consequently, the values obtained were useless for our purposes. Because of this, it was decided to omit Run #4, INLET & OUTLET, from the average.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #1  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:

	net mg	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	10.38	0.005581	0.005114	0.008330	0.2
Filter:	0.6	0.000322	0.000295	0.000481	0.01
Condensables:	1.173333	0.000630	0.000578	0.000941	0.02
Total:	12.15333	0.006534	0.005988	0.009753	0.23

N-BaCl = 0.00971

SULFATE RESULTS:

	Vol aliq	vt	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	25	0.2	0.001266	0.001160	0.001829	0.05
Filter:	10	0	0	0	0	0
Condensables:	22	0.1	0.000557	0.000510	0.000831	0.02
Total:			0.001823	0.001670	0.002721	0.07

ADDITIONAL DATA:

TIME	start	finish	%O2	%CO2	%H2O	Vm(std)	SDCFM
	1030	1130	11.43	8.04	8.36	28.64	4174

③ 
$$\text{gr/DSCF} = \frac{\text{Norm. BaCl} \left( \frac{\text{Vol}}{\text{Aliq.}} \right) \left( \frac{\text{mls}}{\text{Time}} \right) \left( \frac{\text{Coefficient to grams}}{\text{grams}} \right) \left( \frac{\text{grams}}{\text{grams}} \right)}{\text{Vm(std)}}$$

$$= \frac{(0.00971) \left( \frac{25}{25} \right) (0.2) (485) (0.0154)}{28.64}$$

Equation:  
 CFR method 8

④ 
$$\text{Lbs/HR} = \frac{\text{gr/DSCF} \times \text{grains/Lbs} \times \text{DSCFM}}{\text{min/HR}}$$

$$= (0.001266) (0.00958) (4174)$$

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #:	1	2	3
<b>TIME</b>			
start .....	1030	1220	1445
finish ..	1130	1302	1555
%O2 .....	11.43	12.11	12.33
%CO2 .....	8.04	7.47	6.9
%H2O .....	8.36	10.97	10.24
Vm std .....	28.64	18.94	29.59
SDCFM .....	4174	3834	4497
DATA @62' Vm std..	28.64	35.25	32.36
PARTICULATE DATA %H2O.....	8.36	9.74	8.65
SDCFM ...	4174	3402	3267
<b>PROBE/NOZZLE WT</b>			
final # <i>574</i> <i>200 AL./200 Sample</i> .....	98.5025	96.8154	101.3358
init # <i>574</i> .....	98.4942	96.8154	101.3356
net <i>574</i> .....	0.01038	0	0.00033
<b>FILTER WT</b>			
final # <i>374</i> .....	0.5262	0.5279	0.4928
init. # .....	0.5256	0.5267	0.4927
net .....	0.0006	0.0012	0.0001
<b>CONDENSABLE WT</b>			
sample vol .....	220	220	203
alliq. vol .....	150	100	100
final # .....	95.4208	101.9367	95.4276
init # .....	95.42	101.9301	95.4206
net .....	0.001173	0.01452	0.013804

**TITRAMETRIC DATA**

<b>PROBE/NOZZLE</b>			
norm. BaCl .....	0.00971	0.00971	0.00971
sample vol .....	<i>250</i>	130	165
aliq. voi .....	<i>10</i>	10	10
dilution .....	1	1	1
mls titrant.....	<i>0.2</i>	0.05	0.1

<b>FILTER</b>			
norm. BaCl .....	0.00971	0.00971	0.00971
sample vol .....	100	100	100
aliq. vol .....	10	10	10
dilution .....	1	1	1
mls. titrant .....	0	0	0

<b>CONDENSABLES</b>			
norm. BaCl .....	<i>mls. Titrant 0.1</i>	<i>0.1</i>	<i>0.24</i>
sample vol .....	0.00971	0.00971	0.00971
sample vol .....	220	220	203
aliq. vol .....	10	10	10
dilution .....			

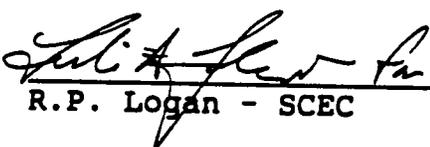
SAN DIEGO AIR POLLUTION CONTROL DISTRICT  
MONITORING AND TECHNICAL SERVICES  
9150 CHESAPEAKE DRIVE  
SAN DIEGO, CA 92123

NITROGEN OXIDES, CARBON MONOXIDE, PARTICULATE,  
AND SULFUR EMISSIONS SUMMARY REPORT

SITE: Bell Jr. High School

P/O NUMBER: 56896 and 59383 JOB NO: T1482-2  
TEST DATE: 4/7/92

EQUIPMENT: Bell Jr. High Landfill Gas Collection and  
Incineration System

REPORT BY:  DATE: 5/14/92  
R.P. Logan - SCEC

APCD PERSONNEL: Janet Cawyer/David Shina

SITE PERSONNEL: Bob Hanley/Bob Hobbs

APPROVED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

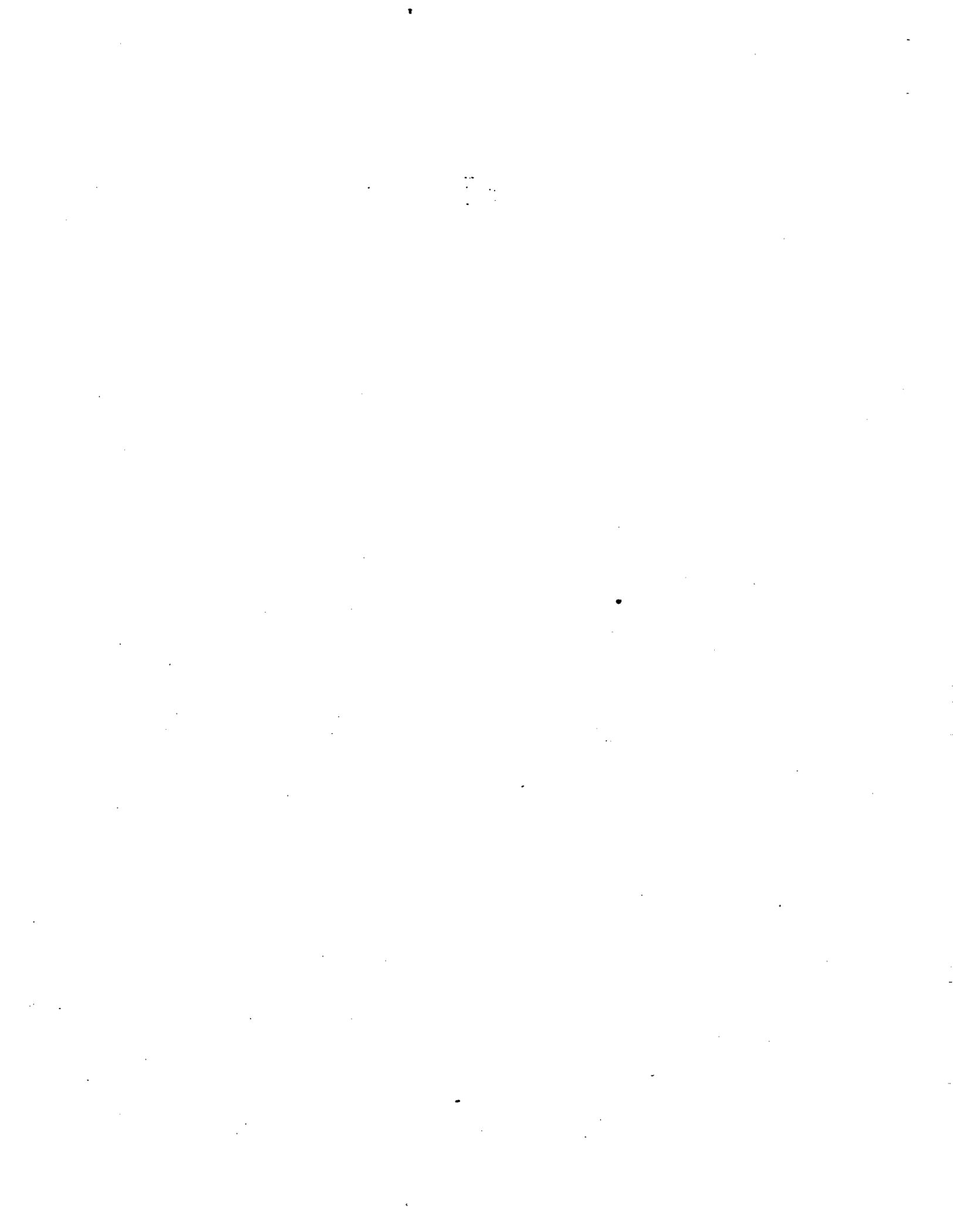
SCEC  
 1582-1 N. BATAVIA  
 ORANGE, CA 92667  
 (714)282-8240

COMPANY: S.D.A.P.C.D. @ BELL JR. HIGH SCHOOL  
 DATE: APRIL 7, 1992  
 UNIT: FLARE @ EXHAUST  
 REPORT #: T1482-2

FIELD DATA @ 68'

SITE:

	RUN #:	1	2	3
	TIME:	1030	1220	1445
<hr/>				
Vm (dry gas sampled).....		30.05	19.991	30.755
Y (meter calib. factor).....		0.976583	0.976583	0.976583
P bar (Barometric pressure).....		29.85	29.85	29.85
P static (stack pressure, " H2O).....		0	0	0
Delta H (differential meter press, " H2O)....		0.791	0.667	0.873
Tm (meter temperature, R').....		540.8	543.8	535.9
Vol H2O mls .....		55.5	49.6	71.7
<hr/>				
Vm(std),dscf .....		28.64	18.94	29.59
<hr/>				
Bws-H2O vapor .....		0.0836	0.1097	0.1024
MF-moisture factor .....		0.9164	0.8903	0.8976
<hr/>				
% CO2 .....		8.04	7.47	6.9
% O2 .....		11.43	12.11	12.33
% N2 .....		80.53	80.42	80.77
<hr/>				
Md-MW stk gas,dry .....		29.74	29.68	29.6
Ms-MW stk gas,wet .....		28.76	28.4	28.41
<hr/>				
Cp-pitot tube .....		0.84	0.84	0.84
Avg sq rt $\hat{p}$ .....		0.202	0.19	0.221
T stack, R'.....		1771.4	1775.8	1777.1
Stack area,ft2 .....		12.25	12.25	12.25
<hr/>				
Vs-fps .....		20.84	19.75	22.97
Qstd-dscfm .....		4174	3834	4492
<hr/>				
Area noz,ft2 .....		1.28E-03	1.28E-03	1.30E-03
Sample time .....		60	40	60
<hr/>				
% Isokinetic .....		109.2	117.9	103.5



## OMENCLATURE (concl.)

Symbol	units	explanation	equation
<b>P</b>			
$\Delta P$	in H <sub>2</sub> O	pitot diff. press-velocity head of stack gas	read from measuring device
$P_s$	in Hg	barometric pressure at sampling pt.	read from press measuring device
$\pi$ (pi)	none	the ratio of the circumference of a circle to its diameter	3.14165 (see CRC)
$P_m$	in Hg	absolute meter pressure	$P_{bar} + (\Delta H / 13.6)$
$P_s$	in Hg	absolute stack pressure	$P_{bar} + (P_{static} / 13.6)$
$P_g$	in H <sub>2</sub> O	static pressure of stack	read from pressure sensing device
$P_{std}$	in Hg	press at std conditions (29.92)	see CFR
<b>Q</b>			
$Q_s$	acfm	flow rate	$v_s \cdot A_o \cdot 60$
$Q_{std}$	dscfm	dry volumetric stack gas flow rate, corrected to STP	$17.64 \cdot Q_s (1 - B_{ws}) \cdot (P_s / T_s)$
<b>R</b>			
$R$	in Hg-ft <sup>3</sup> /°R-lb-mo	ideal gas constant	21.85 (see CRC)
<b>S</b>			
S.L.	none	Sea Level	read from a relief map
<b>T</b>			
$t_1$	°F	dry gas meter inlet temp, uncorrected	read from temp sensing device
$t_2$	°F	dry gas meter outlet temp, uncorrected	read from temp sensing device
$t_1$ corr	°F	dry gas meter outlet temp, corrected	$t_1 + \text{temperature correction}$
$t_2$ corr	°F	dry gas meter outlet temp, corrected	$t_2 + \text{temperature correction}$
$\theta$ (theta)	min	sampling time/point	$\theta / \ln$
$\Theta$ (Theta)	min	total sampling time	none
$t_i$	°F	impinger outlet temp	read from temp sensing device
$t_m$	°F	dry gas meter temp in F	$(t_1 + t_2) / 2$
$t_r$	°R	dry gas meter temp in R	$t_m + 460$
$n$	none	$t_i$ number or traverse pts	summation of the traverse points
$t_s$	°F	stack temp in F	read from temp sensing device
$t_{sR}$	°R	stack temp in R	$t_s + 460$
$T_{std}$	°R	temp at std conditions (528)	see CFR
<b>U</b>			
$V_{lc}$	ml	water collected from impingers and the silica gel (if applicable)	from lab analysis
$V_m$	ft <sup>3</sup>	sample gas volume, uncorrected	read from dry gas meter
$V_m'$	ft <sup>3</sup>	sample gas volume, corrected	$V_m \cdot Y$
$V_m$ std	ft <sup>3</sup>	volume of gas sample by the dry gas meter, corrected to STP	$((V_m \cdot T_{std}) / P_m) / ((P_{std} \cdot T_m) - \text{corr } V_m)$
$V_{pw@ts}$	in Hg	vapor pressure of water at $t_s$	see CRC water vapor press. tables
$V_{pw@ti}$	in Hg	vapor pressure of water at $t_i$	see CRC water vapor press. tables
$V_s$	ft/sec	stack gas velocity	$85.49 \cdot C_p \cdot (T_s \cdot \Delta P) / (P_s \cdot M_s) \cdot 0.5$
$V_w$ std	ft <sup>3</sup>	Vol. of water vapor in gas sample, corrected to STP	$(V_{lc} \cdot \rho \cdot R \cdot T_{std}) / (P_{std} \cdot MW_{H_2O}) + \text{corr } V_{wm}$
<b>Y</b>			
$Y$	none	dry gas meter calibration factor	see CFR 40, parts 53-60

### Conversion Factors

(multiply by the number)

0.002669	in Hg-ft <sup>3</sup> /°R-ml	conversion to get in Hg-ft <sup>3</sup> /R	see CRC
0.00857	lb/gr-min/hr	conv from gr/min to lb/hr (60/7000)	see Lange's Handbook of Chemistry
0.04707	ft <sup>3</sup> /ml	conversion from ml to ft <sup>3</sup>	see Lange's Handbook of Chemistry
15.43	gr/g	conversion from g to gr	see Lange's Handbook of Chemistry
17.64	°R/in H <sub>2</sub> O	$T_{std} / P_{std}$ (528/29.92)	see Lange's Handbook of Chemistry
85.49	(ft/sec)-(lb-in Hg/lb-mo-°R-in H <sub>2</sub> O)) <sup>0.5</sup>	conversion factor to get velocity in ft/sec	see CRC

(divide by the number)

4	in <sup>2</sup> /ft <sup>2</sup>	conversion from in <sup>2</sup> to ft <sup>2</sup>	see CRC
3.6	in H <sub>2</sub> O/in Hg	conversion from in H <sub>2</sub> O to in Hg	see CRC

add to the number)

	°R/°F	conversion from F to R	see CRC
--	-------	------------------------	---------

TEST SITE: Bell Junior High Landfill Flare  
 620 South Briarwood Road  
 Paradise Hills, CA

**TEST WITNESS - RUN #1**

TEST #: 92098.1

P.O.# 880614

TEST DATE: 4/7/92

Type of plant (Asphalt / Perlite / Combustion): **COMBUSTION**

UNIT TESTED: INCINERATOR

EQUIPMENT: LANDFILL FLARE

TESTED BY: Russ Logan & Ted Jackman of SCEC

DATE: 4/7/92

SITE PERSONNEL: Bob Hanley

DATE: 4/7/92

APCD ENGINEER: Archi de la Cruz

DATE: 4/7/92

LAB ANALYSIS BY: SCEC

DATE: 4/21/92

REPORT BY: SCEC (Russ Logan)

DATE: 5/14/92

REVIEWED BY: David N. Shina

DATE: 6/17/92

APPROVED BY:

DATE:

ROBERT YELENOSKY, SENIOR AIR POLLUTION CHEMIST

This report has been reviewed and found to be representative of the testing that was performed.

**SDAPCD RULES**

TEST	LIMIT	MEASURED	PASS/FAIL
RULE 53 SPECIFIC CONT.	0.10 gr/dscf	0.010 gr/dscf	NON-EXCEEDANCE

**TEST RESULTS SUMMARY:**

ITEM	I	Cs(12%)	E
UNITS	%	gr/dscf	lbs/hr
VALUE	109	0.0097	0.23

**ENGINEERING SUMMARY**

Qstd	TYPE OF FUEL	LOAD	RATE
dscfm		Tons/Hr	Tons
4192			

**TEST PARAMETERS:**

**SYSTEM DESCRIPTION:**

Landfill gas is allowed to accumulate in the wells and piping of a flare system. Every 12 hours the incinerator ignites its flare to destroy by combustion, the accumulated landfill gases. The flare is at the bottom of the incinerator stack. The sampling points are near the top of the stack. The particulate emissions from this process are the subject of the report.

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA New Source Performance guidelines and from EPA CFR 40, Standards Method 5. The sampling train utilized a front-end filter.

**CALCULATIONS**

All calculations are based on the EPA CFR 40 Standards Method 5, July 1, 1991, Parts 53-60, Appendix A.

**PARTICULATE SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way, because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to SDAPCD rules.

**ANALYSES:**

**Gas:** A CEM analysis was performed by SCEC.

**Particulate:** All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.



FACSIMILE TRANSMISSION

DATE:

7/30/92

TO:

SOARCS David Shina

COMPANY:

TRANSMITTING TO TELECOPY #: (619) 694-2730

FROM: RUSS LOGAN

TELEPHONE #: (714) 282-8240

TELECOPY #: (714) 282-8247

REGARDING:

Sox Excursion

TOTAL NUMBER OF PAGES INCLUDING COVER SHEET: 3

\*\*If there is a transmission problem, please call ASAP\*\*

TRANSMISSION SENT FROM:

SCEC  
1582-1 N. Batavia Street  
Orange, CA 92667  
(714) 282-8240  
FAX (714) 282-8247

COMMENTS:

David, I hope this helps!

I'll be in the office all

day Thursday + then Friday

Afternoon. Charles Furr

MESSAGE # 2666

**CALCULATIONS:**

**TEMPERATURES:**

01)	$ts = (\sum ts(n))/total\ n's$	
02)	$Ts = ts + 460$	1311 °F
03)	$tm = (\sum \{(t1(n) + t2(n))/2\} / total\ n's = (t1 + t2) / 2$	1771 °F
04)	$Tm = (t1 + t2) / 2 + 460$	81 °F
05)	$ti = (\sum ti(n)) / total\ n's$	541 °F
06)	$Tstd$	68 °F

**PRESSURES:**

07)	$Pbar = \{(P @\ S.L.) + [ft.\ above\ S.L. * (-0.1\ in\ Hg/100ft)]\}$	29.85 in Hg
08)	$Pg = \text{read from pressure sensing device}$	0.00 in H2O
09)	$Ps = Pbar + (Pg/13.6)$	29.85 in Hg
10)	$\Delta H$	0.79 in H2O
11)	$Pm = Pbar + (\Delta H/13.6)$	29.91 in Hg
12)	$Pstd$	29.92 in Hg

**VOLUME:**

13)	$Vm = Vm(end) - Vm(begin)$	
14)	$Y$	30.054 ft <sup>3</sup>
15)	$Vm' = Vm * Y$	0.9766
16)	$Vpw @\ ti = \text{from appendix}$	29.351 ft <sup>3</sup>
17)	$corr\ Vwm = \{[(Vm' * Vpw @\ imp / Ps) * Pm * Tstd] / (Tm * Pstd)\}$	N/A in Hg
18)	$Vm\ std = \{[Vm' * (Tstd / Tm) * (Pm / Pstd)] - corr\ Vwm\}$	0.0000 ft <sup>3</sup>
19)	$Vic = (\sum\ \text{Volume of impingers})$	28.647 ft <sup>3</sup>
20)	$\rho$	55.50 ml
21)	$R$	0.002010 lb/ml
22)	$MwH2O$	21.85 in Hg-ft <sup>3</sup> /°R-lb-mo
23)	$Vw\ std = \{[(Vic * \rho * R * Tstd) / (Pstd * MwH2O)] + corr\ Vwm\}$	18.00 g/g-mo
		2.6196 ft <sup>3</sup>

**MOISTURE:**

24)	$Bws(1) = (Vw\ std) / (Vw\ std + Vm\ std) * 100$	8.38 %
25)	$Vpw @\ ts = \text{from appendix}$	29.92 in Hg
26)	$Bws(2) = [(Vpw @\ ts) / Ps] * 100$	100.23 %
27)	$Bws = \text{lower value of equation 24 or 26}$	8.38 %

**MOLECULAR WEIGHT:**

28)	%O2	
29)	%CO2	11.43 %
30)	%N2+inerts+%CO	8.04 %
31)	$Md = [0.440(\%CO2)] + [0.320(\%O2)] + [0.280(\%N2+inerts+%CO)]$	80.53 %
32)	$Ms = Md * (1 - Bws) + 18.0 * (Bws)$	29.74 g/g*mole
		28.76 g/g*mole

**FLOW:**

33)	$\Delta P$	
34)	$Cp$	0.0412 in H2O
35)	$vs = 85.49 * Cp * \{[(Ts * \Delta P) / (Ps * Ms)]^{.5}\}$	0.840
36)	$As = 3.14 * [(Ds)^2 / 4]$	20.941 ft/sec
37)	$Qs = (vs) * As * 60$	12.250 ft <sup>2</sup>
38)	$Qstd = 17.64 * Qs * (1 - Bws) * Ps / Ts$	15392 acfm
		4192 dscfm

**EMISSIONS:**

**FRONT HALF**

39)	$mn\ (front)$	
40)	$Cs\ (front) = 15.43 * mn(front) / Vm\ std$	0.01090 g
41)	$Cs(12\%,\ front) = (12 / \%CO2) * Cs(front)$	0.00587 grains/dscf
42)	$E\ (front) = (0.00857) * (Qstd) * Cs\ (front)$	0.00876 grains/dscf
		0.21 lbs/hr

**BACK HALF**

43)	$mn\ (back)$	
44)	$Cs\ (back) = 15.43 * mn(back) / Vm\ std$	0.00117 g
45)	$Cs(12\%,\ back) = (12 / \%CO2) * Cs(back)$	0.00063 grains/dscf
46)	$E\ (back) = (0.00857) * (Qstd) * Cs\ (back)$	0.00094 grains/dscf
		0.02 lbs/hr

**TOTAL**

47)	$mn\ (total) = mn(front) + mn(back)$	
48)	$Cs\ (total) = 15.43 * mn(total) / Vm\ std$	0.01207 g
49)	$Cs(12\%,\ total) = (12 / \%CO2) * Cs(total)$	0.00650 grains/dscf
50)	$E\ (total) = (0.00857) * (Qstd) * Cs\ (total)$	0.00970 grains/dscf
51)	$E.A. = [(\%O2 - .5(\%CO) * 100) / (0.264(\%N2) - (\%O2) - 0.5(\%CO))]$	0.23 lbs/hr
		116.28 %

**KINETICS:**

52)	$Dn =$	
53)	$An = 3.14 * [(Dn)^2 / 4]$	0.485 in
54)	$I = .09450 * (Ts * Vm\ std) / (Ps * Vs * An * \rho * (1 - Bws))$	0.1847 in <sup>2</sup>
		108.77 % =
		109 %

**FIELD DATA & DATA SUMMARY:**

Trav. Pt	Vm (ft <sup>3</sup> )	ΔP (in H2O)	ΔH (in H2O)	Stack Temp (°F)	Box Temp (°F)	Imp Temp (°F)	t 1 (in) (°F)	t 2 (out) (°F)	velocity (ft/sec)
1	487.162	0.930	0.540	1303		68	75.00	73.00	017.82
2		0.050	0.900	1307		68	78.00	76.00	023.04
3		0.030	0.530	1331		68	78.00	77.00	017.97
4		0.020	0.360	1313		68	83.00	85.00	014.59
5		0.040	0.720	1312		68	82.00	81.00	020.63
6		0.030	0.540	1325		68	84.00	82.00	017.94
7		0.100	1.820	1311		68	84.00	83.00	032.62
8	517.216	0.050	0.920	1289		68	86.00	84.00	022.92

Average:	Vm	ΔP	ΔH	ts	tbox	ti	t 1 (in)	t 2 (out)	vs
	30.054	0.041	0.791	1311	not done	68	81.38	80.13	20.94

<b>METER BOX PARAMETERS:</b> Box ID = <u>NUTECH</u> ΔH@ = _____ Y = <u>0.9766</u>		<b>NOZZLE &amp; PROBE:</b> Dn = <u>0.485</u> in An = <u>0.1847</u> in <sup>2</sup> Cp = <u>0.840</u>		<b>MISCELLANEOUS:</b> Maximum vacuum = <u>5.0</u> in. Hg. Circular stack (Y/N) = <u>NO</u> Silica gel (Y/N) = <u>YES</u>	
<b>VOLUME:</b> start leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> final leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> Vm <u>30.054</u> ft <sup>3</sup>		<b>PRESSURES:</b> Pbar = <u>29.85</u> in Hg Pg = <u>0.00</u> in H2O Vpw @ ts = <u>29.9200</u> in Hg Vpw @ ti = <u>N/A</u> in Hg		<b>LABORATORY DATA:</b> mn(front) = <u>0.01090</u> g CO2 = <u>8.04</u> % mn(back) = <u>0.00117</u> g O2 = <u>11.43</u> % mn(total) = <u>0.01207</u> g CO = <u>0.00</u> % Vic <u>55.50</u> ml N2 = <u>80.53</u> %	
<b>STACK PARAMETERS:</b> Width = <u>3.50</u> ft Length = <u>3.50</u> ft As = <u>12.250</u> ft <sup>2</sup>		<b>TIME:</b> Ø = <u>60.0</u> min tn = <u>8</u> points σ = <u>7.5</u> min/pt		<b>TEMPERATURES:</b> t1 = <u>81.38</u> °F ti = <u>68</u> °F t2 = <u>80.13</u> °F tbox = <u>not done</u> °F tm = <u>80.75</u> °F ts = <u>1311</u> °F	

# **CONTRACTOR TEST REPORT**

Bell Jr. High (Run #1) on 4/7/92

O. #: 880614 TEST#: 92098.1

SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA 92123

**PARTICULATE TEST LABORATORY ANALYSIS DATA SHEET**

TEST SITE: Bell Jr. High  
620 South Briarwood Road.  
Paradise Hills, CA

**TEST WITNESS - RUN # 1**

TEST #: 92098.1

P.O.#: 880614

TEST DATE: 4/7/92

LAB ANALYSIS BY: Russ Logan (of SCEC)

DATE: 4/21/92

LAB REPORT BY: Russ Logan (of SCEC)

DATE: 5/14/92

REVIEWED BY: David Shina (of SDAPCD)

DATE: 6/17/92

**(1) IMPINGER VOLUMES**

	FINAL WGT.	INIT WGT.	NET WGT.
# 1	572.70 g	545.90 g	26.80 g
# 2	486.80 g	481.80 g	5.00 g
# 3	579.70 g	566.80 g	12.90 g
# 4	476.30 g	476.80 g	-0.50 g
# 5	787.20 g	775.90 g	11.30 g

Was silica gel used (Y/N) ? =

Total impinger charge =  ml

Total weight collected =  g

Total volume collected, V<sub>ic</sub> =  ml

**(2) BLANKS**

A	B	C	D	E	F	G	STANDARDS				
LOCATION	SOLVENT	ID	END WGT	INIT WGT	NET WGT.	RINSES	H	I	J	K	L
			g	g	(E-F) g	ml	g/ml (G/D)	% (H*100)	ppm (H*10^6)	PASS FAIL	LIMITS
BLANK	ACETONE	E9	99.63435	99.63420	0.00015	100.00	0.0000015	0.0001500	1.50	P	0.0010% = 10ppm
BLANK	WATER	E14	96.75430	96.75430	0.00000	100.00	0.0000000	0.0000000	0.00	P	0.0004% = 4ppm

**(3) WEIGHTS & RINSES**

a	b	c	d	e	f	g	h	i	j	k
LOCATION	SOLVENT	ID	END WGT	INIT. WGT	NET WGT.	RINSES	SOLV. WGT	WGT (corr)	ALIQUOTS	Totals
			g	g	(e-f) g	ml	(g*H) g	(f-h) g	g	(ΣSubtotals(i+j)) g
FRONT	ACETONE									
FRONT	WATER									
FRONT	TOTAL	E7	99.50250	99.49420	0.00830	50	0.000075	0.008225	0.00208	
FRONT	FILTER	F5	0.52620	0.52560	0.00060	N/A	N/A	0.000600	N/A	
FRONT	Subtotals (Σcolumn)=							0.00882	0.00208	0.01090 g
BACK	ACETONE									
BACK	WATER									
BACK	TOTAL	E5	95.42080	95.42000	0.00080	0.00	0.000000	0.000800	0.00037	
BACK	FILTER	N/A								
BACK	Subtotals (Σcolumn)=							0.00080	0.00037	0.00117 g
TOTAL	Totals = (Σsubtotals - Σcolumn k(front & back))=									0.01207 g

SCEC did not charge the Impingers with water, because they were analyzing for SO<sub>x</sub> and needed a different charge. This was acceptable to the District.

SCEC used only 50 mls of acetone for the FRONT half rinses. The water blank is 0 ppm, so there will be no SOLV. WGT. value.

SCEC did not wash out the BACK half with acetone, so the SOLV. WGT. contribution will be zero

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #1  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	10.38	0.005581	0.005114	0.008330	0.2
Filter:	0.6	0.000322	0.000295	0.000481	0.01
Condensables:	1.173333	0.000630	0.000578	0.000941	0.02
Total:	12.15333	0.006534	0.005988	0.009753	0.23

N BaCl = 0.00971

SULFATE RESULTS:	Vol aliq.	Vt	gr/dscf	gr/scf	gr/dscf @ 12% CO2	lbs/hr
Probe & Nozzle:	25	0.2	0.001266	0.001160	0.001889	0.05
Filter:	10	0	0	0	0	0
Condensables:	22	0.1	0.000557	0.000510	0.000831	0.02
Total:			0.001823	0.001670	0.002721	0.07

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1030	1130	11.43	8.04	8.36	28.64	4174

SAN DIEGO AIR POLLUTION CONTROL DISTRICT  
MONITORING AND TECHNICAL SERVICES  
9150 CHESAPEAKE DRIVE  
SAN DIEGO, CA 92123

NITROGEN OXIDES, CARBON MONOXIDE, PARTICULATE,  
AND SULFUR EMISSIONS SUMMARY REPORT

SITE: Bell Jr. High School

P/O NUMBER: 56896 and 59383 JOB NO: T1482-2  
TEST DATE: 4/7/92

EQUIPMENT: Bell Jr. High Landfill Gas Collection and  
Incineration System

REPORT BY: *R.P. Logan* DATE: 5/14/92  
R.P. Logan - SCEC

APCD PERSONNEL: Janet Cawyer/David Shina

SITE PERSONNEL: Bob Hanley/Bob Hobbs

APPROVED BY: *Justin M. Loh* DATE: 10/12/92

PLANT FLARE TEST TYPE Method 8 FIELD TEST DATA SHEET

SOUTH COAST ENVIRONMENTAL COMPANY

Date 4/7/92 Barometric Pressure 29.85  
 Test Location Belle Outlet Static In. wg. 0.0  
 Run Number # 1 Probe Type/Length 6' H20  
 Stack Diameter 42 x 42 Pilot Coefficient 0.84  
 Operator TJS Meter Box No. MJ Tech  
 Filter No. [redacted] Nozzle No./Size .485  
Start: 10:30

Contents	Impinger Volumes/Heights		Gas Composition				
	Final	Initial	Net	Time	CO2	O2	CO
TPA	572.7	555.9	26.80		8.04	11.43	
K.O.	486.8	481.3	5.00				
K.O.	577.2	568.8	12.90				
K.O.	476.3	476.8	-0.5	Leak Rate	cfm	"Hg	
Silica Gel	788.2	775.9	11.30	Initial	0.00	20"	
				Final	0.00	15"	
		Total	55.50				

Sample Point	Time	ΔP In wg	ΔH In wg	Gas Meter Volume Ft <sup>3</sup>	Stack	Probe	Temperature of		Imp.	Gas Meter In	Gas Meter Out	Pump Vacuum In. Hg	√ΔP	Comments
							Oven	Imp.						
1	0:00	.03	.54	487.162	1303					75	73	5		
2	7:30	.05	.90	490.42	1307					78	76	5		
3	15:00	.03	.53	494.38	1331					79	77	5		
4	22:30	.02	.36	497.35	1313					83	85	5		Vm = 30.05
1	30:00	.04	0.72	500.00	1312					82	81	5		ΔP = 0.041
2	37:30	.03	0.54	503.81	1325					84	82	5		ΔH = 0.791
3	45:00	.00	1.01	507.003	1311					84	83	5		Ts = 1311.4°F
4	52:30	.05	0.92	511.48	1289					86	84	5		Tm = 80.8°F
				517.216										Duration = 60 min

Client: DAVID BELL TIT

Analyst: ---

Report #: T-1452-2

Site: ---

Test Date: 4-29-92

Run No: 1

GRAVIMETRIC ANALYSIS

Fraction: Probes and Nozzle Washings

REF: ST17

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final: 98.5025	98.5024	98.5025	98.5025 grms.
Tare:			98.4200 grms.
NET:			73.0825 mg.

Fraction: Filter

Filter No: F5

Date: 4/21/92	Date: 4/21/92	Date:	
Time: 1200 #1	Time: 1800 #2	Time: #3	AVERAGE
Final: 0.5251	0.5262		0.5262 grms.
Tare:			0.5256 grms.
NET:			0.0006 mg.

Fraction: Condensables

Aliquot: 1.50 Total Sample: 2.25

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final: 95.4202	95.4209		95.4208 grms.
Tare:			95.4200 grms.
NET:			0.0008 mg.
TOTAL:			0.0008 mg.

Fraction: Condensable Organics

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final:			grms.
Tare:			grms.
NET:			mg.

**FIELD DATA & DATA SUMMARY:**

Trav. Pt	Vm (ft <sup>3</sup> )	ΔP (in H2O)	ΔH (in H2O)	Stack Temp (°F)	Box Temp (°F)	Imp Temp (°F)	t 1 (in) (°F)	t 2 (out) (°F)	velocity (ft/sec)
	<b>517.487</b>								
1		0.030	0.550	1293		68	81.00	81.00	017.89
2		0.030	0.540	1318		68	83.00	82.00	018.01
3		0.030	0.540	1328		68	82.00	82.00	018.07
4		0.030	0.540	1321		68	82.00	82.00	018.03
5		0.050	0.920	1303		68	88.00	86.00	023.16
6	<b>537.478</b>	0.050	0.910	1332		68	90.00	87.00	023.35

Average:	Vm	ΔP	ΔH	ts	tbox	ti	t 1 (in)	t 2 (out)	vs
	19.991	0.036	0.667	1316	not done	68	84.33	83.33	19.75

<b>METER BOX PARAMETERS:</b> Box ID = <u>NUTECH</u> ΔH@ = _____ Y = <u>0.9766</u>		<b>NOZZLE &amp; PROBE:</b> Dn = <u>0.485</u> in An = <u>0.1847</u> in <sup>2</sup> Cp = <u>0.840</u>		<b>MISCELLANEOUS:</b> Maximum vacuum = <u>5.0</u> in. Hg. Circular stack (Y/N) = <u>NO</u> Silica gel (Y/N) = <u>YES</u>	
<b>VOLUME:</b> start leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> final leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> Vm <u>19.991</u> ft <sup>3</sup>		<b>PRESSURES:</b> Pbar = <u>29.85</u> in Hg Pg = <u>0.00</u> in H2O Vpw @ ts = <u>29.92</u> in Hg Vpw @ ti = _____ in Hg		<b>LABORATORY DATA:</b> mn(front) = <u>0.00120</u> g CO2 = <u>7.47</u> % mn(back) = <u>0.01452</u> g O2 = <u>12.11</u> % mn(total) = <u>0.01572</u> g CO = <u>0.00</u> % Vlc <u>49.60</u> ml N2 = <u>80.42</u> %	
<b>STACK PARAMETERS:</b> Width = <u>3.50</u> ft Length = <u>3.50</u> ft As = <u>12.250</u> ft <sup>2</sup>		<b>TIME:</b> θ = <u>40</u> min tn = <u>6</u> points s = <u>6.7</u> min/pt		<b>TEMPERATURES:</b> t1 = <u>84.33</u> °F ti = <u>68</u> °F t2 = <u>83.33</u> °F tbox = <u>not done</u> °F tm = <u>83.83</u> °F ts = <u>1316</u> °F	

SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE

TEST SITE: Bell Junior High Landfill Flare  
 620 South Briarwood Road  
 Paradise Hills, CA

**TEST WITNESS - RUN #2**

TEST #: 92098.2

P.O.# 880614

TEST DATE: 4/7/92

Type of plant (Asphalt/Perlite/Combustion): **COMBUSTION**

UNIT TESTED: INCINERATOR

EQUIPMENT: LANDFILL FLARE

TESTED BY: Russ Logan & Ted Jackman of SCEC	DATE: 4/7/92
SITE PERSONNEL: Bob Hanley	DATE: 4/7/92
APCD ENGINEER: Archi de la Cruz	DATE: 4/7/92
LAB ANALYSIS BY: SCEC	DATE: 4/21/92
REPORT BY: SCEC (Russ Logan)	DATE: 5/14/92
REVIEWED BY: David N. Shina	DATE: 6/17/92
APPROVED BY:	DATE:

ROBERT YELENOSKY, SENIOR AIR POLLUTION CHEMIST

This report has been reviewed and found to be representative of the testing that was performed.

**SDAPCD RULES**

TEST	LIMIT	MEASURED	PASS/FAIL
RULE 53 SPECIFIC CONT.	0.10 gr/dscf	0.02428 gr/dscf	NON-EXCEEDANCE

**TEST RESULTS SUMMARY:**

ITEM	I	Cs(12%)	E
UNITS	%	gr/dscf	lbs/hr
VALUE	118	0.02428	0.42

**ENGINEERING SUMMARY**

Qstd	TYPE OF FUEL	LOAD	RATE
dscfm		Tons/Hr	Tons
3831			

**TEST PARAMETERS:**

**SYSTEM DESCRIPTION:**

Landfill gas is allowed to accumulate in the wells and piping of a flare system. Every 12 hours the incinerator ignites its flare to destroy by combustion, the accumulated landfill gases. The flare is at the bottom of the incinerator stack. The sampling points are near the top of the stack.

The particulate emissions from this process are the subject of the report.

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA New Source Performance guidelines and from EPA CFR 40, Standards Method 5. The sampling train utilized a front-end filter.

**CALCULATIONS**

All calculations are based on the EPA CFR 40 Standards Method 5, July 1, 1991, Parts 53-60, Appendix A.

**PARTICULATE SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way, because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to SDAPCD rules.

**ANALYSES:**

**Gas:** A CEM analysis was performed by SCEC.

**Particulate:** All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.

**PARTICULATE TEST LABORATORY ANALYSIS DATA SHEET**

TEST SITE: Bell Jr. High  
620 South Briarwood Road  
Paradise Hills, CA

**TEST WITNESS - RUN #2**

TEST #: 92098.2

P.O.#: 880614

TEST DATE: 4/7/92

LAB ANALYSIS BY: Russ Logan (of SCEC)

DATE: 4/21/92

LAB REPORT BY: Russ Logan (of SCEC)

DATE: 5/14/92

REVIEWED BY: David Shina (of SDAPCD)

DATE: 6/17/92

**(1) IMPINGER VOLUMES**

	FINAL WGT.	INIT WGT.	NET WGT.
#1	546.30 g	524.10 g	22.20 g
#2	489.90 g	486.80 g	3.10 g
#3	577.50 g	565.60 g	11.90 g
#4	478.00 g	476.30 g	1.70 g
#5	749.80 g	739.10 g	10.70 g

Was silica gel used (Y/N) ?=  y

Total impinger charge=  0 ml

Total weight collected=  49.60 g

Total volume collected, Vic=  49.60 ml

**(2) BLANKS**

							STANDARDS				
A	B	C	D	E	F	G	H	I	J	K	L
LOCATION	SOLVENT	ID	END WGT	INIT WGT	NET WGT.	RINSES	g/ml	%	ppm	PASS	LIMITS
			g	g	(E-F) g	ml	(G/D)	(H*100)	(H*10^6)	FAIL	
BLANK	ACETONE	E9	99.63435	99.63420	0.00015	100.00	0.0000015	0.0001500	1.50	P	0.0010%=10ppm
BLANK	WATER	E14	96.75430	96.75430	0.00000	100.00	0.0000000	0.0000000	0.00	P	0.0004%=4ppm

**(3) WEIGHTS & RINSES**

a	b	c	d	e	f	g	h	i	j	k
LOCATION	SOLVENT	ID	END WGT	INIT. WGT	NET WGT.	RINSES	SOLV. WGT	WGT (corr)	ALIQUOTS	Totals
			g	g	(e-f) g	ml	(g*H)	(f-h) g	g	(ΣSubtotals(i+j)) g
FRONT	ACETONE									
FRONT	WATER									
FRONT	TOTAL	**E12	96.81510	96.81540	0.00000	***50	0.000075	N/A	N/A	
FRONT	FILTER	F6	0.52790	0.52670	0.00120	N/A	N/A	0.001200	N/A	
FRONT	Subtotals (Σcolumn)=							0.00120	N/A	0.00120 g
BACK	ACETONE									
BACK	WATER									
BACK	TOTAL	E3	101.93670	101.93010	0.00660	****0.00	0.000000	0.006600	0.00792	
BACK	FILTER	N/A								
BACK	Subtotals (Σcolumn)=							0.00660	0.00792	0.01452 g
TOTAL	Totals = (Σsubtotals - Σcolumn k(front & back))=									0.01572 g

\* SCEC did not charge the impingers with water, because they were analyzing for SOx and needed a different charge. This was acceptable to the District.

\*\* For the FRONT HALF totals, SCEC did NOT allow the beakers to come to a constant weight and they took an incorrect average weight. To get a weight, I took the last recorded weight and deemed it the 'official average' weight.

\*\*\* SCEC used only 50 mls of acetone for the FRONT half rinses. The waterblank is 0-ppm, so there will be no SOLV. WGT. value.

\*\*\*\* SCEC did not wash out the BACK half with acetone, so the SOLV. WGT. contribution will be zero

**CALCULATIONS:**

**TEMPERATURES:**

01)	$ts = (\sum ts(n))/total\ n's$	1316 °F
02)	$Ts = ts + 460$	1776 °R
03)	$tm = (\sum \{(t\ 1(n) + t\ 2(n))/2\}/total\ n's = (t1 + t2)/2$	84 °F
04)	$Tm = (t1 + t2)/2 + 460$	544 °R
05)	$ti = (\sum ti(n))/total\ n's$	68 °F
06)	$Tstd$	528 °R

**PRESSURES:**

07)	$Pbar = \{(P\ @\ S.L.) + [ft.\ above\ S.L. \cdot (-0.1\ in\ Hg/100ft)]\}$	29.85 in Hg
08)	$Pg = \text{read from pressure sensing device}$	0.00 in H2O
09)	$Ps = Pbar + (Pg/13.6)$	29.85 in Hg
10)	$\Delta H$	0.67 in H2O
11)	$Pm = Pbar + (\Delta H/13.6)$	29.90 in Hg
12)	$Pstd$	29.92 in Hg

**VOLUME:**

13)	$Vm = Vm(end) - Vm(begin)$	19.991 ft <sup>3</sup>
14)	$Y$	0.9766
15)	$Vm' = Vm \cdot Y$	19.523 ft <sup>3</sup>
16)	$Vpw\ @\ ti = \text{from appendix}$	N/A in Hg
17)	$corr\ Vwm = \{(Vm' \cdot Vpw@imp/Ps) \cdot Pm \cdot Tstd\} / (Tm \cdot Pstd)$	0.0000 ft <sup>3</sup>
18)	$Vm\ std = \{Vm' \cdot (Tstd/Tm) \cdot (Pm/Pstd)\} - corr\ Vwm$	18.942 ft <sup>3</sup>
19)	$Vlc = (\sum\ \text{Volume of impingers})$	49.60 ml
20)	$\rho$	0.002010 lb/ml
21)	$R$	21.85 in Hg-ft <sup>3</sup> /°R-lb-mo
22)	$MwH2O$	18.00 g/g-mo
23)	$Vw\ std = \{(Vlc \cdot \rho \cdot R \cdot Tstd) / (Pstd \cdot MwH2O)\} + corr\ Vwm$	2.3411 ft <sup>3</sup>

**MOISTURE:**

24)	$Bws(1) = (Vw\ std) / (Vw\ std + Vm\ std) \cdot 100$	11.00 %
25)	$Vpw\ @\ ts = \text{from appendix}$	29.92 in Hg
26)	$Bws(2) = (Vpw\ @\ ts) / Ps \cdot 100$	100.23 %
27)	$Bws = \text{lower value of equation 24 or 26}$	11.00 %

**MOLECULAR WEIGHTS:**

28)	%O2	12.11 %
29)	%CO2	7.47 %
30)	%N2+inerts+%CO	80.42 %
31)	$Md = [0.440(\%CO2)] + [0.320(\%O2)] + [0.280(\%N2+inerts+%CO)]$	29.68 g/g-mole
32)	$Ms = Md \cdot (1 - Bws) + 18.0 \cdot (Bws)$	28.39 g/g-mole

**FLOW:**

33)	$\Delta P$	0.0361 in H2O
34)	$Cp$	0.840
35)	$vs = 85.49 \cdot Cp \cdot \{(Ts \cdot \Delta P) / (Ps \cdot Ms)\}^{.5}$	19.751 ft/sec
36)	$As = 3.14 \cdot [(Ds)^2 / 4]$	12.250 ft <sup>2</sup>
37)	$Qs = (vs) \cdot As \cdot 60$	14517 acfm
38)	$Qstd = 17.64 \cdot Qs \cdot (1 - Bws) \cdot Ps / Ts$	3831 dscfm

**EMISSIONS:**

**FRONT HALF**

39)	$mn\ (front)$	0.00120 g
40)	$Cs\ (front) = 15.43 \cdot mn(front) / Vm\ std$	0.00098 grains/dscf
41)	$Cs(12\%,\ front) = (12/\%CO2) \cdot Cs(front)$	0.00157 grains/dscf
42)	$E\ (front) = (0.00857) \cdot (Qstd) \cdot Cs\ (front)$	0.03 lbs/hr

**BACK HALF**

43)	$mn\ (back)$	0.01452 g
44)	$Cs\ (back) = 15.43 \cdot mn(back) / Vm\ std$	0.01183 grains/dscf
45)	$Cs(12\%,\ back) = (12/\%CO2) \cdot Cs(back)$	0.01900 grains/dscf
46)	$E\ (back) = (0.00857) \cdot (Qstd) \cdot Cs\ (back)$	0.39 lbs/hr

**TOTAL**

47)	$mn\ (total) = mn(front) + mn(back)$	0.01572 g
48)	$Cs\ (total) = 15.43 \cdot mn(total) / Vm\ std$	0.01281 grains/dscf
49)	$Cs(12\%,\ total) = (12/\%CO2) \cdot Cs(total)$	0.02057 grains/dscf
50)	$E\ (total) = (0.00857) \cdot (Qstd) \cdot Cs\ (total)$	0.42 lbs/hr
51)	$E.A. = [(\%O2 \cdot .5(\%CO) \cdot 100) / (0.264(\%N2) - (\%O2) - 0.5(\%CO))]$	132.77 %

**ISOKINETICS:**

52)	$Dn =$	0.485 in
53)	$An = 3.14 \cdot [(Dn)^2 / 4]$	0.1847 in <sup>2</sup>
54)	$I = .09450 \cdot (Ts \cdot Vm\ std) / Ps \cdot Vs \cdot An \cdot (1 - Bws)$	118.05 % = 118 %

**RECTION FOR NON-ISOKINETIC CONDITIONS:**

$Cs(12\%,\ total) - \text{corrected} = (Cs(12\%,\ total)) \cdot (I/100)$	0.02428 grains/dscf
$E\ (total) - \text{corrected} = (0.00857) \cdot (Qstd) \cdot \{Cs\ (total) - \text{corrected}\}$	0.42 lbs/hr

SAN DIEGO AIR POLLUTION CONTROL DISTRICT  
MONITORING AND TECHNICAL SERVICES  
9150 CHESAPEAKE DRIVE  
SAN DIEGO, CA 92123

NITROGEN OXIDES, CARBON MONOXIDE, PARTICULATE,  
AND SULFUR EMISSIONS SUMMARY REPORT

SITE: Bell Jr. High School

P/O NUMBER: 56896 and 59383 JOB NO: T1482-2  
TEST DATE: 4/7/92

EQUIPMENT: Bell Jr. High Landfill Gas Collection and  
Incineration System

REPORT BY: *R.P. Logan* DATE: 5/14/92  
R.P. Logan - SCEC

APCD PERSONNEL: Janet Cawyer/David Shina

SITE PERSONNEL: Bob Hanley/Bob Hobbs

APPROVED BY: *Judith A. Hall* DATE: 10/12/92

# **CONTRACTOR TEST REPORT**

Client: 7-142-2

Analyst: \_\_\_\_\_

Report #: 7-142-2

Site: 2411 E. 11th

Test Date: 4-7-92

Run No: 2

### GRAVIMETRIC ANALYSIS

Fraction: Probes and Nozzle Washings

REF: ST17

Date:	Date:	Date:	AVERAGE
Time: #1	Time: #2	Time: #3	
Final: 96.8156	96.8173	96.8151	
Tare:			96.8154 grms.
NET:			96.8154 grms.
			mg.

Fraction: Filter

Filter No: F6

Date: 4/21/92	Date: 4/21/92	Date:	AVERAGE
Time: 1200 #1	Time: 1200 #2	Time: #3	
Final: 0.5279	0.5280	.	
Tare:			0.5279 grms.
NET:			0.5282 grms.
			mg.

Fraction: Condensables

Aliquot: 100 Total Sample: 230

Date:	Date:	Date:	AVERAGE
Time: #1	Time: #2	Time: #3	
Final: 101.9369	101.9365		
Tare:			101.9367 grms.
NET:			101.9301 grms.
TOTAL:			mg.

Fraction: Condensable Organics

Date:	Date:	Date:	AVERAGE
Time: #1	Time: #2	Time: #3	
Final:			
Tare:			grms.
NET:			grms.
			mg.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #2  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @	
				12% CO2	lbs/hr
Probe & Nozzle:	0	0	0	0	0
Filter:	1.2	0.000975	0.000868	0.001567	0.03
Condensables:	14.52	0.011806	0.010510	0.018965	0.39
Total:	15.72	0.012781	0.011379	0.020533	0.42

N BaCl = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @	
					12% CO2	lbs/hr
Probe & Nozzle:	13	0.05	0.000248	0.000221	0.000399	0.01
Filter:	10	0	0	0	0	0
Condensables:	22	0.1	0.000842	0.000749	0.001353	0.03
Total:			0.001091	0.000971	0.001753	0.04

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1220	1302	12.11	7.47	10.97	18.94	3834

SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE

TEST SITE: Bell Junior High Landfill Flare  
 620 South Briarwood Road  
 Paradise Hills, CA

**TEST WITNESS - RUN #3**

TEST #: 92098.3

P.O.# 880614

TEST DATE: 4/7/92

Type of plant (Asphalt /Perlite / Combustion): **COMBUSTION**

UNIT TESTED: INCINERATOR

EQUIPMENT: LANDFILL FLARE

TESTED BY: Russ Logan & Ted Jackman of SCEC	DATE: 4/7/92
SITE PERSONNEL: Bob Hanley	DATE: 4/7/92
APCD ENGINEER: Archi de la Cruz	DATE: 4/7/92
LAB ANALYSIS BY: SCEC	DATE: 4/21/92
REPORT BY: SCEC (Russ Logan)	DATE: 5/14/92
REVIEWED BY: David N. Shina	DATE: 6/17/92
APPROVED BY:	DATE:

ROBERT YELENOSKY, SENIOR AIR POLLUTION CHEMIST

This report has been reviewed and found to be representative of the testing that was performed.

**SDAPCD RULES**

TEST	LIMIT	MEASURED	PASS/FAIL
RULE 53 SPECIFIC CONT.	0.10 gr/dscf	0.009 gr/dscf	NON-EXCEEDANCE

**TEST RESULTS SUMMARY:**

ITEM	I	Cs(12%)	E
UNITS	%	gr/dscf	lbs/hr
VALUE	104	0.0092	0.20

**ENGINEERING SUMMARY**

Qstd	TYPE OF FUEL	LOAD	RATE
dscfm		Tons/Hr	Tons
4478			

**TEST PARAMETERS:**

**SYSTEM DESCRIPTION:**

Landfill gas is allowed to accumulate in the wells and piping of a flare system. Every 12 hours the incinerator ignites its flare to destroy by combustion, the accumulated landfill gases. The flare is at the bottom of the incinerator stack. The sampling points are near the top of the stack. The particulate emissions from this process are the subject of the report.

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA New Source Performance guidelines and from EPA CFR 40, Standards Method 5. The sampling train utilized a front-end filter.

**CALCULATIONS**

All calculations are based on the EPA CFR 40 Standards Method 5, July 1, 1991, Parts 53-60, Appendix A.

**PARTICULATE SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way, because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to SDAPCD rules.

**ANALYSES:**

**Gas:** A CEM analysis was performed by SCEC.

**Particulate:** All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.



**CALCULATIONS:**

**TEMPERATURES:**

01)	$t_s = (\sum t_s(n))/\text{total } n\text{'s}$	
02)	$T_s = t_s + 460$	1321 °F
03)	$t_m = (\sum \{(t_1(n) + t_2(n))/2\})/\text{total } n\text{'s} = (t_1 + t_2)/2$	1781 °F
04)	$T_m = (t_1 + t_2)/2 + 460$	76 °F
05)	$t_i = (\sum t_i(n))/\text{total } n\text{'s}$	536 °F
06)	$T_{std}$	68 °F 528 °R

**PRESSURES:**

07)	$P_{bar} = \{(P @ \text{S.L.}) + [\text{ft. above S.L.} \cdot (-0.1 \text{ in Hg}/100\text{ft})]\}$	29.85 in Hg
08)	$P_g = \text{read from pressure sensing device}$	0.00 in H <sub>2</sub> O
09)	$P_s = P_{bar} + (P_g/13.6)$	29.85 in Hg
10)	$\Delta H$	0.87 in H <sub>2</sub> O
11)	$P_m = P_{bar} + (\Delta H/13.6)$	29.91 in Hg
12)	$P_{std}$	29.92 in Hg

**VOLUME:**

13)	$V_m = V_m(\text{end}) - V_m(\text{begin})$	30.755 ft <sup>3</sup>
14)	$Y$	0.9766
15)	$V_m' = V_m \cdot Y$	30.035 ft <sup>3</sup>
16)	$V_{pw} @ t_i = \text{from appendix}$	N/A in Hg
17)	$\text{corr } V_{wm} = \{[(V_m' \cdot V_{pw} @ \text{imp}/P_s) \cdot P_m \cdot T_{std}]/(T_m \cdot P_{std})\}$	0.0000 ft <sup>3</sup>
18)	$V_m \text{ std} = \{[V_m' \cdot (T_{std}/T_m) \cdot (P_m/P_{std})] - \text{corr } V_{wm}\}$	29.578 ft <sup>3</sup>
19)	$V_{ic} = (\sum \text{Volume of impingers})$	71.70 ml
20)	$\rho$	0.002010 lb/ml
21)	$R$	21.85 in Hg-ft <sup>3</sup> /°R-lb-mo
22)	$M_{wH_2O}$	18.00 g/g-mo
23)	$V_w \text{ std} = \{[(V_{ic} \cdot \rho \cdot R \cdot T_{std})/(P_{std} \cdot M_{wH_2O})] + \text{corr } V_{wm}\}$	3.3842 ft <sup>3</sup>

**MOISTURE:**

24)	$B_{ws}(1) = (V_w \text{ std})/(V_w \text{ std} + V_m \text{ std}) \cdot 100$	10.27 %
25)	$V_{pw} @ t_s = \text{from appendix}$	29.92 in Hg
26)	$B_{ws}(2) = [(V_{pw} @ t_s)/P_s] \cdot 100$	100.23 %
27)	$B_{ws} = \text{lower value of equation 24 or 26}$	10.27 %

**MOLECULAR WEIGHT:**

28)	%O <sub>2</sub>	12.33 %
29)	%CO <sub>2</sub>	6.90 %
30)	%N <sub>2</sub> +inerts+%CO	80.77 %
31)	$M_d = [0.440(\%CO_2)] + [0.320(\%O_2)] + [0.280(\%N_2 + \text{inerts} + \%CO)]$	29.60 g/g*mole
32)	$M_s = M_d \cdot (1 - B_{ws}) + 18.0 \cdot (B_{ws})$	28.41 g/g*mole

**FLOW:**

33)	$\Delta P$	0.0487 in H <sub>2</sub> O
34)	$C_p$	0.840
35)	$v_s = 85.49 \cdot C_p \cdot \{[(T_s \cdot \Delta P)/(P_s \cdot M_s)]^{.5}\}$	22.963 ft/sec
36)	$A_s = 3.14 \cdot [(D_s)^2/4]$	12.250 ft <sup>2</sup>
37)	$Q_s = (v_s) \cdot A_s \cdot 60$	16878 acfm
38)	$Q_{std} = 17.64 \cdot Q_s \cdot (1 - B_{ws}) \cdot P_s/T_s$	4478 dscfm

**EMISSIONS:**

**FRONT HALF**

39)	$m_n$ (front)	0.00044 g
40)	$C_s$ (front) = $15.43 \cdot m_n(\text{front})/V_m \text{ std}$	0.00023 grains/dscf
41)	$C_s(12\%, \text{front}) = (12/\%CO_2) \cdot C_s(\text{front})$	0.00040 grains/dscf
42)	$E$ (front) = $(0.00857) \cdot (Q_{std}) \cdot C_s$ (front)	0.01 lbs/hr

**BACK HALF**

43)	$m_n$ (back)	0.00974 g
44)	$C_s$ (back) = $15.43 \cdot m_n(\text{back})/V_m \text{ std}$	0.00508 grains/dscf
45)	$C_s(12\%, \text{back}) = (12/\%CO_2) \cdot C_s(\text{back})$	0.00884 grains/dscf
46)	$E$ (back) = $(0.00857) \cdot (Q_{std}) \cdot C_s$ (back)	0.20 lbs/hr

**TOTAL**

47)	$m_n$ (total) = $m_n(\text{front}) + m_n(\text{back})$	0.01018 g
48)	$C_s$ (total) = $15.43 \cdot m_n(\text{total})/V_m \text{ std}$	0.00531 grains/dscf
49)	$C_s(12\%, \text{total}) = (12/\%CO_2) \cdot C_s(\text{total})$	0.00924 grains/dscf
50)	$E$ (total) = $(0.00857) \cdot (Q_{std}) \cdot C_s$ (total)	0.20 lbs/hr
51)	$E.A. = [(\%O_2 - .5(\%CO) \cdot 100)]/[0.264(\%N_2) - (\%O_2) - 0.5(\%CO)]$	137.10 %

**KINETICS:**

52)	$D_n$	0.488 in
53)	$A_n = 3.14 \cdot [(D_n)^2/4]$	0.1870 in <sup>2</sup>
54)	$I_n = 0.09450 \cdot (T_s \cdot V_m \text{ std})/P_s \cdot V_s \cdot A_n \cdot (1 - B_{ws})$	103.84 % = 104 %

**FIELD DATA & DATA SUMMARY:**

Trav. Pt	Vm (ft <sup>3</sup> )	ΔP (in H2O)	ΔH (in H2O)	Stack Temp (°F)	Box Temp (°F)	Imp Temp (°F)	t 1 (in) (°F)	t 2 (out) (°F)	velocity (ft/sec)
	<b>537.875</b>								
1		0.050	0.880	1316		68	77.00	77.00	023.24
2		0.050	0.890	1335		68	77.00	77.00	023.36
3		0.050	0.880	1335		68	75.00	75.00	023.36
4		0.050	0.880	1343		68	76.00	77.00	023.42
5		0.040	0.710	1320		68	76.00	76.00	020.81
6		0.050	0.890	1320		68	77.00	76.00	023.27
7		0.050	0.900	1307		68	75.00	75.00	023.18
8	<b>568.630</b>	0.050	0.910	1290		68	75.00	75.00	023.07

Average:	Vm	ΔP	ΔH	ts	tbox	ti	t 1 (in)	t 2 (out)	vs
	30.755	0.049	0.870	1321	not done	68	76.00	76.13	22.96

<b>METER BOX PARAMETERS:</b> Box ID = <u>NUTECH</u> ΔH@ = _____ Y = <u>0.9766</u>		<b>NOZZLE &amp; PROBE:</b> Dn = <u>0.488</u> in An = <u>0.1870</u> in <sup>2</sup> Cp = <u>0.840</u>		<b>MISCELLANEOUS:</b> Maximum vacuum = <u>5.0</u> in. Hg. Circular stack (Y/N) = <u>NO</u> Silica gel (Y/N) = <u>YES</u>	
<b>VOLUME:</b> start leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> final leak rate = <u>0.000</u> cfm Pass/Fail <u>PASS</u> Vm <u>30.755</u> ft <sup>3</sup>		<b>PRESSURES:</b> Pbar = <u>29.85</u> in Hg Pg = <u>0.00</u> in H2O Vpw @ ts = <u>29.92</u> in Hg Vpw @ ti = _____ in Hg		<b>LABORATORY DATA:</b> mn(front) = <u>0.00044</u> g CO2 = <u>6.90</u> % mn(back) = <u>0.00974</u> g O2 = <u>12.33</u> % mn(total) = <u>0.01018</u> g CO = <u>0.00</u> % Vlc <u>71.70</u> ml N2 = <u>80.77</u> %	
<b>STACK PARAMETERS:</b> Width = <u>3.50</u> ft Length = <u>3.50</u> ft As = <u>12.250</u> ft <sup>2</sup>		<b>TIME:</b> Ø = <u>60</u> min tn = <u>8</u> points ø = <u>7.5</u> min/pt		<b>TEMPERATURES:</b> t1 = <u>76.00</u> °F ti = <u>68</u> °F t2 = <u>76.13</u> °F tbox = <u>not done</u> °F tm = <u>76.06</u> °F ts = <u>1321</u> °F	

# **CONTRACTOR TEST REPORT**

**PARTICULATE TEST LABORATORY ANALYSIS DATA SHEET**

TEST SITE: Bell Jr. High  
620 South Briarwood Road  
Paradise Hills, CA

**TEST WITNESS - RUN #3**

TEST #: 92098.3

P.O.#: 880614

TEST DATE: 4/7/92

LAB ANALYSIS BY: Russ Logan (of SCEC)

DATE: 4/21/92

LAB REPORT BY: Russ Logan (of SCEC)

DATE: 5/14/92

REVIEWED BY: David Shina (of SDAPCD)

DATE: 6/17/92

**(1) IMPINGER VOLUMES**

	FINAL WGT.	INIT WGT.	NET WGT.
#1	591.90 g	547.10 g	44.80 g
#2	491.70 g	489.90 g	1.80 g
#3	566.50 g	553.60 g	12.90 g
#4	478.90 g	478.00 g	0.90 g
#5	760.40 g	749.10 g	11.30 g

Was silica gel used (Y/N) ?=  y

Total impinger charge=  0 ml

Total weight collected=  71.70 g

Total volume collected, Vlc=  71.70 ml

**(2) BLANKS**

							STANDARDS				
A	B	C	D	E	F	G	H	I	J	K	L
LOCATION	SOLVENT	ID	END WGT g	INIT WGT g	NET WGT. (E-F) g	RINSES ml	g/ml (G/D)	% (H*100)	ppm (J*10^6)	PASS FAIL	LIMITS
BLANK	ACETONE	E9	99.63435	99.63420	0.00015	100.00	0.0000015	0.0001500	1.50	P	0.0010%=10ppm
BLANK	WATER	E14	96.75430	96.75430	0.00000	100.00	0.0000000	0.0000000	0.00	P	0.0004%=4ppm

**(3) WEIGHTS & RINSES**

a	b	c	d	e	f	g	h	i	j	k
LOCATION	SOLVENT	ID	END WGT g	INIT. WGT g	NET WGT. (e-f) g	RINSES ml	SOLV. WGT (g*H) g	WGT (corr) (f-h) g	ALIQUOTS g	Totals (ΣSubtotals(i+j)) g
FRONT	ACETONE									
FRONT	WATER									
FRONT	TOTAL	E6	101.33585	101.33560	0.00025	**50	0.000075	0.000175	0.00016	
FRONT	FILTER	F4	0.49280	0.49270	0.00010	N/A	N/A	0.000100	N/A	
FRONT	Subtotals (Σcolumn)=							0.00027	0.00016	0.00044 g
BACK	ACETONE									
BACK	WATER									
BACK	TOTAL	E5***	95.42560	95.42080	0.00480	0.00	0.000000	0.004800	0.00494	
BACK	FILTER	N/A								
BACK	Subtotals (Σcolumn)=							0.00480	0.00494	0.00974 g
TOTAL	Totals = (Σsubtotals = Σcolumn k(front & back))=									0.01018 g

\* SCEC did not charge the impingers with water, because they were analyzing for SOx and needed a different charge. This was acceptable to the District.

\*\* SCEC used only 50 mls of acetone for the FRONT half rinses. The water blank is 0 ppm, so there will be no SOLV. WGT. value.

\*\*\* (1) SCEC did not wash out the BACK half with acetone, so the SOLV. WGT. contribution will be zero.  
 (2) For the BACK HALF-END WGT, SCEC did NOT allow the beakers to come to a constant weight and they took an incorrect average weight. To get a weight, I took the last recorded weight and deemed it the 'official average' weight.  
 (3) For the BACK HALF-INIT. WGT of Run #3, SCEC used the BACK HALF-END WGT. of Bell Jr. High Lab Run #1. They used the same beaker for 2 different laboratory analyses.  
 (4) SCEC used an incorrect value for the NET WGT.

COMPANY: BELL JR. HIGH  
 DATE: 4-7-92  
 UNIT: FLARE  
 REPORT #: T1482-2

RUN #3  
 @ 68°F  
 EPA METHOD 5/8

PARTICULATE RESULTS:	net mg	gr/dscf	gr/scf	gr/dscf @	
				12% CO2	lbs/hr
Probe & Nozzle:	0.33	0.000171	0.000154	0.000298	0.01
Filter:	0.1	0.000052	0.000046	0.000090	0
Condensables:	13.804	0.007184	0.006448	0.012494	0.28
Total:	14.234	0.007408	0.006649	0.012883	0.29

N BaCl = 0.00971

SULFATE RESULTS:	Vol aliq	Vt	gr/dscf	gr/scf	gr/dscf @	
					12% CO2	lbs/hr
Probe & Nozzle:	16.5	0.1	0.000404	0.000362	0.000703	0.02
Filter:	10	0	0	0	0	0
Condensables:	20.3	0.24	0.001194	0.001071	0.002076	0.05
Total:			0.001598	0.001434	0.002780	0.07

ADDITIONAL DATA:

TIME		%O2	%CO2	%H2O	Vm(std)	SDCFM
start	finish					
1445	1555	12.33	6.9	10.24	29.59	4497

SAN DIEGO AIR POLLUTION CONTROL DISTRICT  
MONITORING AND TECHNICAL SERVICES  
9150 CHESAPEAKE DRIVE  
SAN DIEGO, CA 92123

NITROGEN OXIDES, CARBON MONOXIDE, PARTICULATE,  
AND SULFUR EMISSIONS SUMMARY REPORT

SITE: Bell Jr. High School

P/O NUMBER: 56896 and 59383 JOB NO: T1482-2  
TEST DATE: 4/7/92

EQUIPMENT: Bell Jr. High Landfill Gas Collection and  
Incineration System

REPORT BY: *R.P. Logan* DATE: 5/14/92  
R.P. Logan - SCEC

APCD PERSONNEL: Janet Cawyer/David Shina

SITE PERSONNEL: Bob Hanley/Bob Hobbs

APPROVED BY: *Judith M. Latta* DATE: 10/12/92

EVAPORATION DISH TARE WEIGHTS

use new anti-static gloves!

D/T	T/RH	BP	4/8/92 <sup>100</sup>	4/4/92 <sup>120</sup>	4/12/92 <sup>110</sup>	
DISH #			TARE 1	TARE 2	TARE 3	AVERAGE
<del>E 1</del>						
E 2			97.2815	97.2817	97.2817	97.2816
E 3			101.9300	101.9300	101.9302	101.9301
E 4			99.8116	99.8115	99.8112	99.8114
E 5			95.4200	95.4202	95.4200	95.4200
E 6			101.3355	101.3356	101.3356	101.3356
E 7			98.4943	98.4942	98.4941	98.4942
E 8						
E 9			99.6342	<del>99.6342</del> weight 44 97.6342 <del>99.6342</del> ?	99.6341	99.6342
E 10						
E 11			Hacked final			
E 12			96.8153	96.8155	96.8155	96.8154
E 13			Hacked			
E 14			96.7543	96.7543		96.7543
E 15			Hacked final weights			
<del>E 16</del>						
E 17			95.8822	95.8824	95.8822	95.8824
E 18			96.3234	96.3234	96.3231	96.3233
E 19			Hacked final			
E 20			99.0757	99.0758	99.0757	99.0757
E 21						
<del>E 22</del>						

broken, opps!

MTS

SCEC

FACSIMILE TRANSMISSION

DATE: 7-8-92

TO: David Shiwa

COMPANY: SDAPCD

TRANSMITTING TO TELECOPY #: (619) 694-2730

FROM: RUSS LOGAN

TELEPHONE #: (714) 282-8240

TELECOPY #: (714) 282-8247

REGARDING: TARE WEIGHTS

TOTAL NUMBER OF PAGES INCLUDING COVER SHEET: 2

\*\*If there is a transmission problem, please call ASAP\*\*

TRANSMISSION SENT FROM: SCEC  
1582-1 N. Batavia Street  
Orange, CA 92667  
(714) 282-8240  
FAX (714) 282-8247

COMMENTS:

David.  
Here's the Tare weights  
sheet.  
Russ

MESSAGE # 2613



PLANT FLARE Exhaust TEST TYPE Carb Method FIELD TEST DATA SHEET  
5/8

Date 4-7-92  
 Test Location Bell Jr. Hill  
 Run Number #3  
 Stack Diameter 42 x 42  
 Operator TSE  
 Filter No. \_\_\_\_\_  
 Barometric Pressure 29.85  
 Static In. wg. 0.00  
 Probe Type/Length 6' H2O  
 Pitot Coefficient 0.84  
 Meter Box No. Nu Tech  
 Nozzle No./Size .488

START: 14:45

Impinger Volumes/Heights				Gas Composition			
Contents	Final	Initial	Net	Time	CO2	O2	CO
IPA 80%	571.7	547.1	44.80		6.9	12.33	
H.O.	491.7	487.9	1.80				
H2O 2%	566.5	553.6	12.90				
H.O.	478.9	478.0	0.90	Leak Rate			
Silicobel	760.4	747.1	11.30	Initial			"Hg
				Final	0.00		20"
		Total	71.70	Final	0.00		15"

Sample Point	Time	ΔP In wg	ΔP In wg	Gas Meter Volume Ft <sup>3</sup>	Stack	Temperature °F			Gas Meter In	Gas Meter Out	Pump Vacuum In. Hg	Comments
						Probe	Oven	Imp.				
1	0:00	.05	.90	537.875	1316				77	77		
2	5:00	.05	.89	540.61	1335				77	77		
3	10:00	.05	.88	543.00	1335				75	76		V <sub>m</sub> = 30,755
4	15-	.05	.88	545.81	1343				76	77		DP = 0.0419
1	20-	.04	.71	548.105	1320				76	76		ΔH = 0.873
2	30-	.05	.89	553.24	1326				77	76		T <sub>s</sub> = 1317.1
3	40-	.05	.90	558.51	1307				75	75		T <sub>m</sub> = 75.9
4	50-	.05	.91	563.54	1290				75	75		Duration = 60 min
	60-	.05	.90	568.63	1288				75	75		

NO. 117

Client: Amoco Fuel Co.

Analyst: \_\_\_\_\_

Report #: 71482-3

Site: Star Line

Test Date: 4-2-92

Run No: 3

**GRAVIMETRIC ANALYSIS**

REF: ST17

Fraction: Probes and Nozzle Washings

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final: 101.220	101.225		grms.
Tare:			101.226 grms.
NET:			mg.

Fraction: Filter

Filter No: F4

Date: 4/21/92	Date: 4/21/92	Date:	
Time: 1200 #1	Time: 1800 #2	Time: #3	AVERAGE
Final: 0.4925	0.4920		0.4928 grms.
Tare:			0.4923 grms.
NET:			mg.

Fraction: Condensables

Aliquot: 100

Total Sample: 22

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final: 95.4300	95.4275	95.4256	grms.
Tare:			95.4263 grms.
NET:			mg.
TOTAL:			mg.

*They used ES before*

Fraction: Condensable Organics

Date:	Date:	Date:	
Time: #1	Time: #2	Time: #3	AVERAGE
Final:			grms.
Tare:			grms.
NET:			mg.

EVAPORATION DISH TARE WEIGHTS

use new anti-static gloves!

D/T	T/RH	BP	4/8/92 <sup>160</sup>	4/4/92 <sup>120</sup>	4/2/92 <sup>110</sup>	
DISH #			TARE 1	TARE 2	TARE 3	AVERAGE
<del>E 1</del>						
E 2			97.2815	97.2817	97.2817	97.2816
E 3			101.9300	101.9300	101.9302	101.9301
E 4			99.8116	99.8115	99.8112	99.8114
E 5			95.4200	95.4202	95.4 <sup>199</sup> <del>25</del>	95.4200
E 6			101.3355	101.3356	101.3356	101.3356
E 7			98.4943	98.4942	98.4941	98.4942
E 8						
E 9			99.6342	<del>99.6342</del> weight #4 99.6342 <del>99.6342</del>	99.6341	99.6342
E 10						
E 11			Herkel final			
E 12			96.8153	96.8155	96.8155	96.8154
E 13			Herkel			
E 14			96.7543	96.7543		96.7543
E 15			Herkel final weights			
<del>E 16</del>						
E 17			95.8822	95.8824	95.8824	95.8824
E 18			96.3234	96.3234	96.3231	96.3233
E 19			Herkel final			
E 20			99.0757	99.0758	99.0757	99.0757
E 21						
<del>E 22</del>						

↳ broken, opps!

MTS

SCEC

FACSIMILE TRANSMISSION

DATE: 7-8-92

TO: Davis Shiwa

COMPANY: SDAPCO

TRANSMITTING TO TELECOPY #: (619) 694-2730

FROM: RUSS LOGAN

TELEPHONE #: (714) 282-8240

TELECOPY #: (714) 282-8247

REGARDING: TARE Weights

TOTAL NUMBER OF PAGES INCLUDING COVER SHEET: 2

\*\*If there is a transmission problem, please call ASAP\*\*

TRANSMISSION SENT FROM: SCEC  
1582-1 N. Batavia Street  
Orange, CA 92667  
(714) 282-8240  
FAX (714) 282-8247

COMMENTS:

Davis,

Here's the Tare Weights  
sheet.

Russ

MESSAGE # 2613

# NOMENCLATURE

symbol	units	explanation	equation
<b>A</b>			
An	in <sup>2</sup>	nozzle area	$\pi/4(D_n)^2$
As	ft <sup>2</sup>	stack area	$\pi/4(D_s)^2$ or LxW
<b>B</b>			
Bws(1)	%	fractional stack gas moisture-equ 1	$((V_w \text{ std}) / (V_w \text{ std} + V_m \text{ std}))100$
Bws(2)	%	fractional stack gas moisture-equ 2	$((V_{pw} @ ts) / P_s)100$
Bws	%	water vapor in the gas stream	lower of Bws(1) and Bws(2)
<b>C</b>			
CO	%	carbon monoxide	read from measuring device (0 for Asphalt plants)
CO2	%	carbon dioxide	read from measuring device
Corr Vwm	ft <sup>3</sup>	correction for Vw w/o silica gel	$((V_m * (V_{pw} @ ts) / P_s) * P_m * T_{std}) / (P_m * T_{std})$
Cp	none	pitot tube correction factor	see EPA method 3
Cs(front)	gr/dscf	concentration of particulate in stack gas, corrected to STP for front	$(15.43^* \text{mn(front)}) / (V_m \text{ std})$
Cs(back)	gr/dscf	concentration of particulate in stack gas, corrected to STP for back	$(15.43^* \text{mn(back)}) / (V_m \text{ std})$
Cs(total)	gr/dscf	concentration of particulate in stack gas, corrected to STP for total	$(15.43^* \text{mn(total)}) / (V_m \text{ std})$
Cs12(front, back, total)		same as Cs(front, back, total) except corrected for grain loading at 12% CO2	$(12 / \% \text{CO}_2) * (15.43^* \text{mn(fr, back, total)}) / (V_m \text{ std})$
<b>D</b>			
$\rho$ (density)	lb/ml	density of water at STP	0.002201 (see CRC)
Ds	in or ft	stack diameter	measure at site
Dn	in	nozzle diameter	avg of at least three measurements
<b>E</b>			
E.A.	%	Excess air (for combustion)	$((\% \text{O}_2 - 5\% \text{CO}) * 100) / (26.4 * \% \text{N}_2 - \% \text{O}_2 - 5 * \% \text{CO})$
E(front)	lbs/hr	part. emissions rate-front	$(0.00857)(Q_{sd} * C_s(\text{front}))$
E(back)	lbs/hr	part. emissions rate-back	$(0.00857)(Q_{sd} * C_s(\text{back}))$
E(total)	lbs/hr	part. emissions rate-total	$(0.00857)(Q_{sd} * C_s(\text{total}))$
<b>H</b>			
$\Delta H$	in H2O	average differential pressure across the orifice meter	avg of the readings from the pressure measuring device
$\Delta H@$	none	orifice pressure differential at STP	see EPA Method 5 Appendix
<b>I</b>			
I	%	isokinetics	$(0.09450 * T_s * V_m \text{ std}) / (P_s * V_s * Q * (A_n / 144) * (1 - (Bws / 100)))$
<b>M</b>			
Md	g/g-mole	dry stack gas molecular wgt	$0.44(\% \text{CO}_2) + 0.320(\% \text{O}_2) + 0.280(\% \text{N}_2 + \text{inerts} + \text{CO})$
mn(back)	g	particulate in impingers	measurement from lab analysis
mn(front)	g	particulate in nozzle & probe	measurement from lab analysis
mn(total)	g	total particulate collected	measurement from lab analysis
Ms	g/g-mole	wet stack gas molecular wgt	$Md(1 - Bws) + 18.0(Bws)$
MW CO2	g/mole	mo. wgt of carbon dioxide	44 (see periodic table)
MW N2	g/mole	mo. wgt of nitrogen	28 (see periodic table)
MW O2	g/mole	mo. wgt of oxygen	32 (see periodic table)
MW H2O	g/mole	mo. wgt of water	18 (see periodic table)
<b>N</b>			
N2	%	percent nitrogen	$100 - (\% \text{CO}_2 + \% \text{O}_2 + \% \text{CO} + \text{inerts})$
<b>O</b>			
O2	%	percent oxygen	read from measuring device

## NOMENCLATURE (cont.)



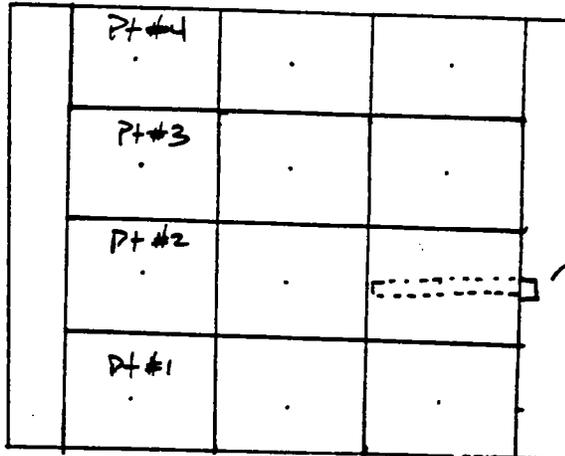
SCEC  
 1582-1 N. BATAVIA  
 ORANGE, CA 92667

FILE REF: ST12

SAMPLE POINT LOCATION DATA SHEET

FACILITY: BELL JR HIGH  
 PROJECT #: T1982-1  
 DATE: 4-7-92  
 STACK DIMENSIONS: L= 42  
                           W= 42  
                           H= \_\_\_\_\_

UPSTREAM DIST. /  
 EQUIVALENT DIAMETERS 5  
 DOWNSTREAM DIST. /  
 EQUIVALENT DIAMETERS 2  
 NO. OF SAMPLING POINTS \_\_\_\_\_  
 SAMPLING PORT DIMENSIONS:  
                           DIA. = 3  
 PROTRUSION DIST. = 3"



Port - #1      #2      #3

SAMPLE POINT <i>Each Port</i>	% OF STACK DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM SAMPLE PORT (IN.)
#1		36.75	39.75
#2		26.25	29.25
#3		15.75	18.75
#4		5.25	8.25

## NOx and CO Analysis

### OFFICIAL TEST RESULTS:

GAS	TEST (PPM)	LIMITS (PPM)	PERFORMANCE EXCEEDANCE/NON-EXCEEDANCE
NOx	18.98	N/A	N/A
CO	0.00	N/A	N/A

### TEST PARAMETERS:

#### PROCEDURES & CALCULATIONS:

All the procedures, calculations, and equipment utilized in these tests are based on EPA NSPS guidelines and from the EPA CFR 40, July 1, 1991, parts 53-60, Method 20, except where noted in the SDAPCD QA manual for Method 20 testing.

#### SAMPLING & EQUIPMENT:

SCEC provided all the sampling and analysis equipment, and they were responsible for all the calibrations according to EPA guidelines.

#### OVERVIEW OF THE TEST:

- (1) SCEC did not perform the NO2 converter equation correctly. The District corrected for this.
- (2) SCEC did not subtract [NO] from [NOx].

RUN #1: *ACCEPTED*

RUN #2: *ACCEPTED*

RUN #3: *ACCEPTED*

### SUMMARY OF ALL 3 TESTS:

	NOx		CO	
	SCEC	APCD	SCEC	APCD
RUN 1	20.00	20.04	0.00	0.00
RUN 2	18.89	18.90	0.00	0.00
RUN 3	17.97	18.00	0.00	0.00
AVERAGE	18.95	18.98	0.00	0.00



# **CONTRACTOR TEST REPORT**

COMPANY: BELL JR. HIGH SCHOOL  
 DATE: MARCH 31, 1992  
 UNIT: FLARE  
 REPORT #: T 1482-1

NO2 - NOx ADJUSTMENTS

---

RUN #	NOX	NO ppm	NO2 ppm	% Recovery	NOx ADJUSTED VALUES		
					NO2 ppm	NOX ppm	
#1	10.5	9.75	0.75	90.2	0.83	10.58	
#2	9.2	8.5	0.7	90.2	0.78	9.28	
#3	8.58	8.25	0.33	90.2	0.37	8.62	
AVERAGE						0.66	9.49

Table 2. Stack Emissions of NO<sub>x</sub>, CO, and O<sub>2</sub>

RUN	SCALE TIME	NO <sub>x</sub> 0-100 PPM			CO 0-500 PPM			O <sub>2</sub> 0-25%	
		CHART (div)	UNCORR (ppm)	CORR 3% O <sub>2</sub> (ppm)	CHART (div)	UNCORR (ppm)	CORR 3% O <sub>2</sub> (ppm)	CHART (div)	%
R1	12:45								
Avg.	13:25	4.23	10.58	20.04	0.0	0.0	0.0	45.7	11.45
PK1									
PK2									
R2	13:30								
Avg.	14:10	3.71	9.28	18.90	0.0	0.0	0.0	48.5	12.11
PK1									
PK2									
R3	14:10								
Avg.	14:50	3.45	8.62	18.00	0.0	0.0	0.0	49.3	12.33
PK1									
PK2									

Peak =

Overall = 3.80 9.49 18.78 0.0 0.0 0.0 47.8 11.96

NO<sub>x</sub> and CO:

- The value reported is the average concentration value at 3% O<sub>2</sub>, when:  
The average pollutant concentration exceeds the permit limit, or the average value is within the permit limit and there are less than two excursions above the limit.
- The value reported is the highest excursion value at 3% O<sub>2</sub>, when:  
There are two or more excursions above the permit limit during the three subtests.
- If it has been determined that stratification exists, the average concentration values of NO<sub>x</sub> and CO, at 3% O<sub>2</sub>, are then reported.

Table 3. Calibration Gases

	CYLINDER	MANUFACTURER	CONCENTRATION (ppm)
NO <sub>x</sub>	CC7297	Scott Marrin	214.2
CO	CC67219	Scott Marrin	476
O <sub>2</sub>	CC106786	Scott Marrin	8.40%
NO <sub>2</sub>	CC648	Scott Marrin	176.0

SAN DIEGO AIR POLLUTION CONTROL DISTRICT  
 MONITORING AND TECHNICAL SERVICES  
 9150 CHESAPEAKE DRIVE  
 SAN DIEGO, CA 92123

NITROGEN OXIDES, CARBON MONOXIDE, PARTICULATE,  
 AND SULFUR EMISSIONS SUMMARY REPORT

SITE: Bell Jr. High School

P/O NUMBER: 56896 and 59383 JOB NO: T1482-2

TEST DATE: 4/7/92

EQUIPMENT: Bell Jr. High Landfill Gas Collection and Incineration System

REPORT BY: *R.P. Logan* DATE: 5/14/92  
 R.P. Logan - SCEC

APCD PERSONNEL: Janet Cawyer/David Shina

SITE PERSONNEL: Bob Hanley/Bob Hobbs

APPROVED BY: \_\_\_\_\_ DATE: \_\_\_\_\_

Table 1. Summary of Results - average NO<sub>x</sub> and CO stack emissions corrected to 3% O<sub>2</sub>

	TEST (ppm)	PERMIT LIMITS (ppm)	PERFORMANCE	HOURS OF TEST
NO <sub>x</sub>	18.98	N/A	N/A	1.9
CO	0.00	N/A	N/A	1.9

\* Particulate and sulfur results can be found on Page 4.

TEST REFERENCE: This testing was performed in accordance with the San Diego Air Pollution Control District Method 20: "Test Procedures For The Determination of Nitrogen Oxides, Carbon Monoxide and Diluent Gases by Continuous Emission Monitoring"



# SCOTT-MARRIN, INC.

6531 BOX SPRINGS BLVD. • RIVERSIDE, CA 92507  
TELEPHONE (714) 653-6780 • FAX (714) 653-2430

## REPORT OF ANALYSIS EPA PROTOCOL GAS MIXTURES

SOCE01

TO:

KEITH SHANNON  
SCEC  
15882-1 NORTH BATAVIA  
ORANGE, CA 92667-

DATE : 03/02/92

CUSTOMER ORDER NUMBER: 446

PAGE 1

COMPONENT	CONCENTRATION (v/v)	REFERENCE STANDARD	ANALYZER MAKE, MODEL, S/N, DETECTION	EXPIRATION DATE	REPLICATE ANALYSIS DATA
<b>CYLINDER NO.: CC29002</b>					
Carbon Dioxide	12.16 ± 0.12 %	GMIS Cylinder # CC60263 @ 17.61 @	Varian Model 1060 S/N None Thermal Conductivity Gas Chromatography Last Cal Date: 12/06/91	08/26/93	02/26/92 12.23 % 11.99 % 12.25 % Mean: 12.16 %
Oxygen	4.08 ± 0.04 %	GMIS Cylinder # CC81219 @ 5.18 @	Varian Model 1060 S/N None Thermal Conductivity Gas Chromatography Last Cal Date: 12/30/91	08/25/93	02/25/92 4.89 % 4.08 % 4.08 % Mean: 4.88 %
Nitrogen	Balance				
Cylinder Pressure: 2000 psig					
<b>CYLINDER NO.: CC106786</b>					
Oxygen	8.40 ± 0.08 %	GMIS Cylinder # CC82350 @ 7.37 @	Varian Model 1060 S/N None Thermal Conductivity Gas Chromatography Last Cal Date: 4/07/92	08/25/93	02/25/92 8.42 % 8.38 % 8.48 % Mean: 8.43 %
Carbon Dioxide	13.47 ± 0.13 %	GMIS Cylinder # CC60263 @ 17.61 @	Varian Model 1060 S/N None Thermal Conductivity Gas Chromatography Last Cal Date: 12/06/91	08/26/93	02/26/92 13.42 % 13.46 % 13.53 % Mean: 13.47 %
Nitrogen	Balance				
Cylinder Pressure: 2000 psig					

ppm = umole/mole      † = mole-%

The above analyses were performed in accordance with EPA-1987 Traceability Protocol # 1, Section 3.0.4, Procedure C1.

Analyst: M.S. Calhoun  
M.S. Calhoun

Approved: J.T. Marrin  
J.T. Marrin

The only liability of this company for gas which fails to comply with this analysis shall be replacement or reanalysis thereof by the company without extra cost.

**ANALYZER CHECK LIST**

	YES	NO	COMMENTS
<b>NO<sub>x</sub> Analyzer</b>			
analyzer calibrated	X		
analyzer set to zero	X		
zero drift < or = 2% of span	X		
reset zero		X	
span drift < or = 2%	X		
reset span		X	
response time within limits	X		
<b>CO Analyzer</b>			
analyzer calibrated	X		
analyzer set to zero	X		
zero drift < or = 2% of span	X		
reset zero		X	
span drift < or = 2%	X		
reset span		X	
<b>O<sub>2</sub> Analyzer</b>			
high calibration set to 20.95%	X		
low cal. set to exhaust gas		X	Set @ 8.4% Gas
zero drift < or = 2% of span	X		
reset zero		X	
span drift < or = 2%	X		
reset span		X	
<b>System Integrity/Leak Check</b>			
pre-testing: performed w/NO/NO <sub>2</sub>	X		
post testing: performed w/NO/NO <sub>2</sub>	X		
<b>System Assembly</b>			
probe installed	X		
moisture removal trap used	X		
particulate filter used	X		
sample manifold pressure set	X		
<b>Data Recording</b>			
annotated	X		
electronic zero set on each pen	X		
chart speed set	X		
convertor efficiency: NO <sub>2</sub> to NO	X		
certificates of cal. gases	X		



SCOTT-MARRIN, INC.  
 2001 THIRD ST. • UNIT H • RIVERSIDE, CA 92507  
 TELEPHONE (714) 784-1240

RECEIVED SEP

REPORT OF ANALYSIS  
 EPA PROTOCOL GAS MIXTURES

SOCE01  
 TO: RUSS LOGAN  
 SOUTH COAST ENVIRONMENTAL CORP  
 1915 MCKINLEY AVE.  
 SUITE E  
 LAVERNE, CA 91750

DATE : 08/30/91

CUSTOMER ORDER NUMBER: 343

PAGE 1

COMPONENT	CONCENTRATION (v/v)	REFERENCE STANDARD	ANALYZER MAKE, MODEL, S/N, DETECTION	EXPIRATION DATE	REPLICATE ANALYSIS DATA
CYLINDER NO.: CC67219					
Carbon Monoxide	476 ± 5 ppm	GMIS Cylinder # CC28362	Carle Insts Model 8888 S/N 8249 Methanation/FID Gas Chromatography	02/29/93	87/28/89 475 ppm 88/29/91 475 ppm
Nitrogen	Balance	496 ppm	Last Cal Date: 07/19/91		473 ppm 481 ppm
Cylinder Pressure:	2000 psig			Mean: 474 ppm	478 ppm

ppm = umole/mole      † = mole-%

The above analyses were performed in accordance with EPA-1987 Traceability Protocol # 1, Section 3.0.4, Procedure G1.

Analyst: Mark Monson  
 M.J. Monson

Approved: J.T. Marrin  
 J.T. Marrin

The only liability of this company for gas which fails to comply with this analysis shall be replacement or reanalysis thereof by the company without extra cost.



# SCOTT-MARRIN, INC.

2001 THIRD ST. • UNIT H • RIVERSIDE, CA 92507  
TELEPHONE (714) 784-1240

RECEIVED 05/23/91

## REPORT OF ANALYSIS EPA PROTOCOL GAS MIXTURES

SOCE01

TO:

KEITH SHANNON  
SOUTH COAST ENVIRONMENTAL CORP  
1915 MCKINLEY AVE., ST. E  
LA VERNE, CA 91750

DATE : 05/14/91

CUSTOMER ORDER NUMBER: 294

PAGE 1

COMPONENT	CONCENTRATION (v/v)	REFERENCE STANDARD	ANALYZER MAKE, MODEL, S/N, DETECTION	EXPIRATION DATE	REPLICATE ANALYSIS DATA										
CYLINDER NO.: CC7297															
Nitric Oxide	214.2 ± 2.1 ppm	GHIS Cylinder # CC7341	Monitor Labs Model 8448 S/N 136 Continuous Chemiluminescence Last Cal Date: 05/01/91	11/14/92	<table border="0"> <tr> <td>05/06/91</td> <td>05/14/91</td> </tr> <tr> <td>213.2 ppm</td> <td>215.8 ppm</td> </tr> <tr> <td>214.9 ppm</td> <td>214.4 ppm</td> </tr> <tr> <td>213.3 ppm</td> <td>214.5 ppm</td> </tr> <tr> <td colspan="2">Mean: 213.8 ppm 214.6 ppm</td> </tr> </table>	05/06/91	05/14/91	213.2 ppm	215.8 ppm	214.9 ppm	214.4 ppm	213.3 ppm	214.5 ppm	Mean: 213.8 ppm 214.6 ppm	
05/06/91	05/14/91														
213.2 ppm	215.8 ppm														
214.9 ppm	214.4 ppm														
213.3 ppm	214.5 ppm														
Mean: 213.8 ppm 214.6 ppm															
Nitrogen, O2-Free Balance Cylinder Pressure: 2000 psig															

ppm = umole/mole

% = mole-%

The above analyses were performed in accordance with EPA-1987 Traceability Protocol # 1, Section 3.0.4, Procedure G1.

Analyst: B.E. Gross

Approved: J.T. Marrin

The only liability of this company for gas which fails to comply with this analysis shall be replacement or reanalysis thereof by the company without extra cost.

STANDARD CALIBRATION CURVE





# SCOTT-MARRIN, INC.

2001 THIRD ST. • UNIT H • RIVERSIDE, CA 92507  
TELEPHONE (714) 784-1240

## REPORT OF ANALYSIS NIST TRACEABLE GAS MIXTURES

SOCE01

TO:

LESLIE JOHNSON  
SOUTH COAST ENVIRONMENTAL  
1582-1 N. BATAVIA STREET  
ORANGE, CA 92667-

DATE: 01/13/92

CUSTOMER ORDER NUMBER: 427

PAGE 1

CYLINDER NUMBER	COMPONENT	CONCENTRATION (v/v)	NIST TRACEABLE REFERENCE STANDARD
CC648	Nitrogen Dioxide Nitrogen	176.8 ± 1.8 ppmv Balance	SRM 2627

Post-it™ brand fax transmittal memo 7671 # of pages 1

To	Russ Logan	From	Dukhile
Co.		Co.	
Dept.		Phone #	(853) 6780
Fax #	(714) 782-8217	Fax #	

ppm = umole/mole

μ = mole-%

The above analysis is traceable to the National Institute of Standards and Technology by intercomparison with the reference standard listed above. Where indicated, volumetric and gravimetric reference standards are traceable thru use of our analytical balance. NIST Report No. NMAP 232.09/202491.

Analyst:

-----  
E.E. Gross

Approved:

-----  
J.T. Marrin



(101) (102)

NO  
MOOT

NO  
MOOT

820/6

Y-4476 (102)

820/6

100 (102)

Ported line  
Zhang's fibre  
Dish

NO  
MOOT

100  
MOOT

NO  
MOOT

NO  
MOOT

NO  
MOOT

NO  
MOOT

LOOKS  
MOVING  
TO  
ADJUST  
820/6  
MOOT

Bell Jr. High: QC M20 JC 7/13/92

SCALES: NOx 0-250 ppm  
 CO 0-1000 ppm (2M) FOR TEST  
 O2 0-25%

176.0 ppm NO2 = 70.0%  
 27.2 ppm NO = 55.2%  
 95.0 ppm CO = 24.2%  
 47.6 ppm CO = 11.0%  
 20.95% O2 = 97.8%  
 8.40% O2 = 33.2%

LOWED = 2 ch div. ( $\pm 2.0$  FS)

GAS	CAL	ACT	DIF	OK	ZWO	ACT	DIF	OK
NO	85.5	85.7	.2	✓	0	0	0	✓
NO	34.1	34.2	.1	✓	0	0	0	✓
CO	95.5	95.2	.3	✓	0	0	0	✓
NO	34.1	34.2	.1	✓	0	0	0	✓
CO	37.1	38.1	1.0	✓	0	0	0	✓
O2	33.2	33.6	.4	✓	.1	0	.1	✓
2	84	83.8	.2	✓	.1	0	.1	✓
NO2	68.2	70.4	2.2	X	0	0	0	0

NO2 (NO mode) = 0  
 NO2 (NO mode) = 68.2  
 OK (RIGHT ON LIMIT)

NO2 = 68.2

converter eff = 96.99% OK

NO system = 85 ch div.

NO R = 85 / 85.5 = 99.4%

NO2 system = 60.2 ch

NO mode = 55.2 ch  
 = 55.2 / 66.2 = 80.9%

Calc:

NO	85	85.7	.7	✓	.2	0	.2	✓
CO	95.5	95.2	.3	✓	0	0	0	✓
O2	34.1	33.6	.5	✓	.5	0	.5	✓

ZUN = UNIT NOT STABLE / RECAL & RUN AGAIN

SYSTEMS = OK (NO2 low - will correct itself)

**DISTRICT QC**

1. Analysis: GC m20

	<u>CAL</u>	<u>ACT</u>	<u>DIF</u>	<u>OK</u>	<u>ZUG</u>	<u>ACT</u>	<u>DIF</u>	<u>OK</u>
NOx	84.5	85.7	1.2	✓	1.3	✓	1.3	✓
O <sub>2</sub>	47.5	47.6	0.1	✓	-1.3	✓	-1.3	✓
CO	34.4	33.6	0.8	✓	1.5	✓	1.5	✓

CALS = OK

ZUG # 3

112-14.52

ch dir ppm = at 37% O<sub>2</sub>  
 CO = ✓ = ✓ = ✓  
 NOx = 3.45 = 8.63 = 17.97  
 O<sub>2</sub> = 49.3 = 12.33 CF = 2.68

	<u>CAL</u>	<u>ACT</u>	<u>DIF</u>	<u>OK</u>	<u>ZUG</u>	<u>ACT</u>	<u>DIF</u>	<u>OK</u>
NOx	84.2	85.7	1.7	✓	1.5	✓	1.5	✓
O <sub>2</sub>	47.4	47.6	0.2	✓	-1	✓	-1	✓
CO	34.1	33.6	0.5	✓	0	✓	0	✓
O <sub>2</sub>	18.3	19.1	0.8	✓	-1	✓	-1	✓

SCALE NOx 0-250 3PT CAL OK (214.2 / 190.6 ppm)  
 O<sub>2</sub> 0-25% " OK (20.95 / 8.4%)  
 CO 0-1000 " OK (476 / 190.6)

CALS = OK

NO SYSTEM = 79.0 / 84.0 = 94.05%

NO<sub>2</sub> conversion: NOx mode NO<sub>2</sub> = 67.0

ACT = 70.4

NO mode = 1.0

NO<sub>2</sub> = 66.0

66.0 / 70.4 = 93.75

O<sub>2</sub> SYSTEM: CO<sub>2</sub> ch dir

NO mode = 1.0 ch dir

61.0 / 66.0 = 92.4%

61.0

High High: @C m24

DES	CAL	ACT	DIF	OK	ZERO	ACT	DIF	OK
O <sub>2</sub>	34.6	33.6	0.4	✓	.5	0	.5	✓
CO (6-1000)	47.5	47.6	0.1	✓	0	0	0	✓
NO <sub>x</sub>	83.8	85.7	1.9	✓	.3	0	.3	✓
CO <sub>x</sub> (RESET)	85.8	85.7	0.1	✓	.3	0	.3	✓

ALS = OK

UN #1:

45-13:27

ch div ✓ ppm at 39% O<sub>2</sub>

CO = 0 = 0 = 0

NO<sub>x</sub> = 4.23 = 10.55 = 20,00

O<sub>2</sub> = 45.7 = 11.45 CF = 1.89

[NO<sub>2</sub>] = 0 → NO STRAT IN STACK

TIME TEST = 30 min + 10 min NO<sub>x</sub> → NO PEAKS

30+ min CO 30+ min O<sub>2</sub>

→ NO PEAKS

AS	CAL	ACT	DIF	OK	ZERO	ACT	DIF	OK
NO <sub>x</sub>	83.6	85.7	2.1	✓	.4	0	.4	✓
CO	47.8	47.6	0.2	✓	-.3	0	-.3	✓
O <sub>2</sub>	34.5	33.6	0.9	✓	.5	0	.5	✓

OK

UN #2:

30-14:10

ch div ✓ ppm = at 39% O<sub>2</sub>

CO = 0 = 0 = 0

NO<sub>x</sub> = 3.71 = 9.28 = 18.89

O<sub>2</sub> = 48.5 = 12.13 CF = 2.04

[NO<sub>2</sub>] = 0 → sample AT CENTRAL PT

TIME: NO<sub>x</sub> = 30 min + 10 min

CO = 30+ min O<sub>2</sub> = 30+ min

→

Table 2. Stack Emissions of NO<sub>x</sub>, CO, and O<sub>2</sub>

RUN	SCALE TIME	NO <sub>x</sub> 0-250 PPM			CO 0-1000 PPM			O <sub>2</sub> 0-25%	
		CHART (div)	UNCORR (ppm)	CORR 3% O <sub>2</sub> (ppm)	CHART (div)	UNCORR (ppm)	CORR 3% O <sub>2</sub> (ppm)	CHART (div)	%
R1	12:45								
Avg.	13:25	4.23	10.58	20.04	0.0	0.0	0.0	45.7	11.45
PK1									
PK2									
R2	13:30								
Avg.	14:10	3.71	9.28	18.90	0.0	0.0	0.0	48.5	12.11
PK1									
PK2									
R3	14:10								
Avg.	14:50	3.45	8.62	18.00	0.0	0.0	0.0	49.3	12.33
PK1									
PK2									

Peak =

Overall = 3.80 9.49 18.98 0.0 0.0 0.0 47.8 11.96

NO<sub>x</sub> and CO:

- The value reported is the average concentration value at 3% O<sub>2</sub>, when:  
The average pollutant concentration exceeds the permit limit, or the average value is within the permit limit and there are less than two excursions above the limit.
- The value reported is the highest excursion value at 3% O<sub>2</sub>, when:  
There are two or more excursions above the permit limit during the three subtests.
- If it is determined that stratification exists, the average concentrations of NO<sub>x</sub> and CO, at 3% O<sub>2</sub>, are then reported.

Table 3. Calibration Gases

	CYLINDER	MANUFACTURER	CONCENTRATION (ppm)
NO <sub>x</sub>	CC7297	Scott Marrin	214.2
CO	CC67219	Scott Marrin	476
O <sub>2</sub>	CC106786	Scott Marrin	8.40%
NO <sub>2</sub>	CC648	Scott Marrin	176.0

# High QC INZ

QC VALUES

NO2 CONVERTER = OK  
 AVE =  $\frac{99.4 + 94.85}{2} = \underline{97.13\%}$

SCEC VALUE  
 $\underline{96.74\%}$

NO2 RECOVERY = OK  
 AVE =  $\frac{96.9 + 93.75}{2} = \underline{95.33\%}$

$\underline{95.17\%}$

NO2 RECOVERY = OK  
 AVE =  $\frac{80.94 + 92.4}{2} = \underline{86.67\%}$  C

$\underline{90.15\%}$  (38.24 / 93.87)

SCEC = DID NOT SUBTRACT NO mode values from NOx  
 " de values for RNO2. Assumed all NOx with  
 SO2

PT CALIBRATION = DONE / ACCEPTABLE

RAT = DONE - NO STRATIFICATION

NO/CAL DEF = NO OFFSETS  $\pm 2\%$  ES / NO CORR NEEDED

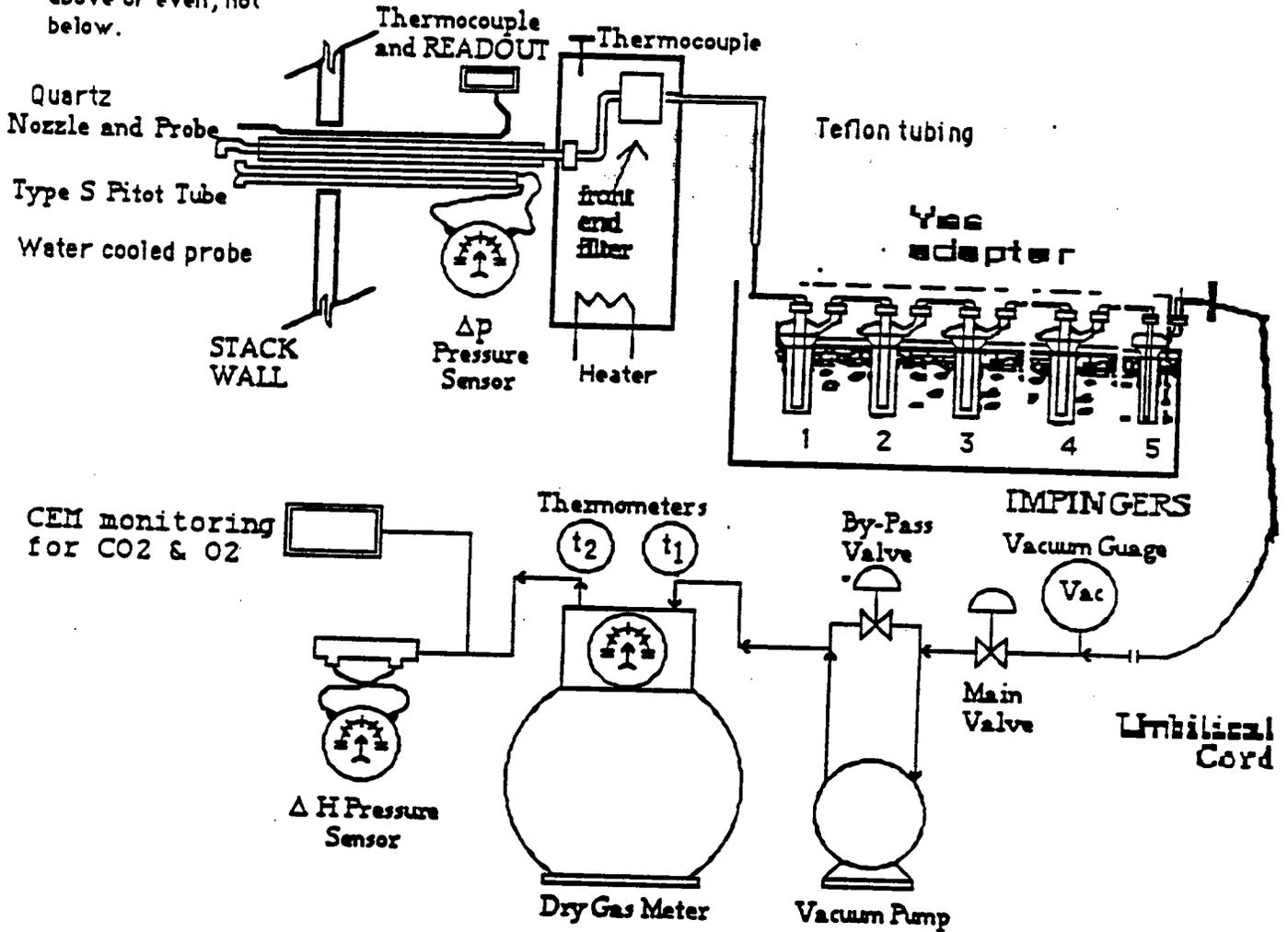
<u>DATA TOTALS</u>	<u>QC ppm</u>	<u>SCEC ppm</u>	<u>CO/NOx AVE = 18.98</u>
CO/NOx	20.00	20.00	CO AVE = 0
CO/CO	0	0	
CO/NOx	18.89	18.90	* SCEC REPORT
" CO	0	0	CO/NOx AVE = <u>18.75</u>
" NOx	17.97	18.00	* REPORT - NEEDS
" CA			

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

FIGURE 1

CONDENSOR SYSTEM

Note: 2.1.3  
Pitot tube should be  
above or even, not  
below.



LEGEND

- No. 1 - IPa
- No. 2 - K.O.
- No. 3 - H2O2
- No. 4 - K.O.
- No. 5 - Silica Gel

FIELD DATA ABBREVIATIONS

- PT = Point Number
- T<sub>s</sub> = Stack Temperature
- ΔP = Pitot Tube Pressure Differential; in H<sub>2</sub>O
- V<sub>s</sub> = Stack Velocity, fps
- ΔH = Orifice Meter Pressure Drop, in H<sub>2</sub>O
- t<sub>1</sub> = Meter Inlet Temperature, °F
- t<sub>2</sub> = Meter Outlet Temperature, °F
- F<sub>m</sub> = Pump Vacuum, in Hg
- t<sub>i</sub> = Impinger Temperature
- P<sub>bar</sub> = Barometric Pressure

FIGURE 1 : PARTICULATE MATTER SAMPLING TRAIN

**Test Witness - Avg**

**TEST PARAMETERS:**

**PROCEDURES:**

... procedures and equipment utilized in these tests are based on EPA NSPS guidelines and from the EPA CFR 40, Standards Method 5. The sampling utilized a front-end filter (fig. 1).

**CALCULATIONS:**

All calculations are based on the EPA CFR 40, Standards Method 5, July 1, 1991, Parts 53-60, Appendix A, Methods 1-5 inclusive.

**PARTICULATE SAMPLING:**

The test consisted of sampling at 8 traverse points, 4 from 1 sampling port (fig.2) and 2 from 2 sample ports, collected from 84 inches below the stack (fig.3). It was done this way, because the stack thermocouple interfered with the last 2 points on the second and third traverse. All field data, SCEC's as well as SDAPCD's, were transferred to the computer printout. All calculations were done by computer and the emissions were compared to SDAPCD rules.

**ANALYSES:**

*Gas:* A CEM analysis was performed by SCEC.

*Particulate.* All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines and performed by SCEC.

**OVERVIEW OF THE TEST:**

<b>RUN #1:</b>	<i>LAB:</i> Passed	<b>RUN #2:</b>	<i>LAB:</i> Eliminated from the test average	<b>RUN #3:</b>	<i>LAB:</i> Passed
	<i>PM:</i> Passed		<i>PM:</i> Eliminated from the test average		<i>PM:</i> Passed

Because of the disparity in numbers between the District and SCEC, it was decided to use the District's values. The District used the values from Runs #1 & 3, because they produced the only reliable numbers. A complete critique of the performance of SCEC's testing procedures and calculations are on page 4 and a data summary of all 3 runs are on page 5.

Figure 3

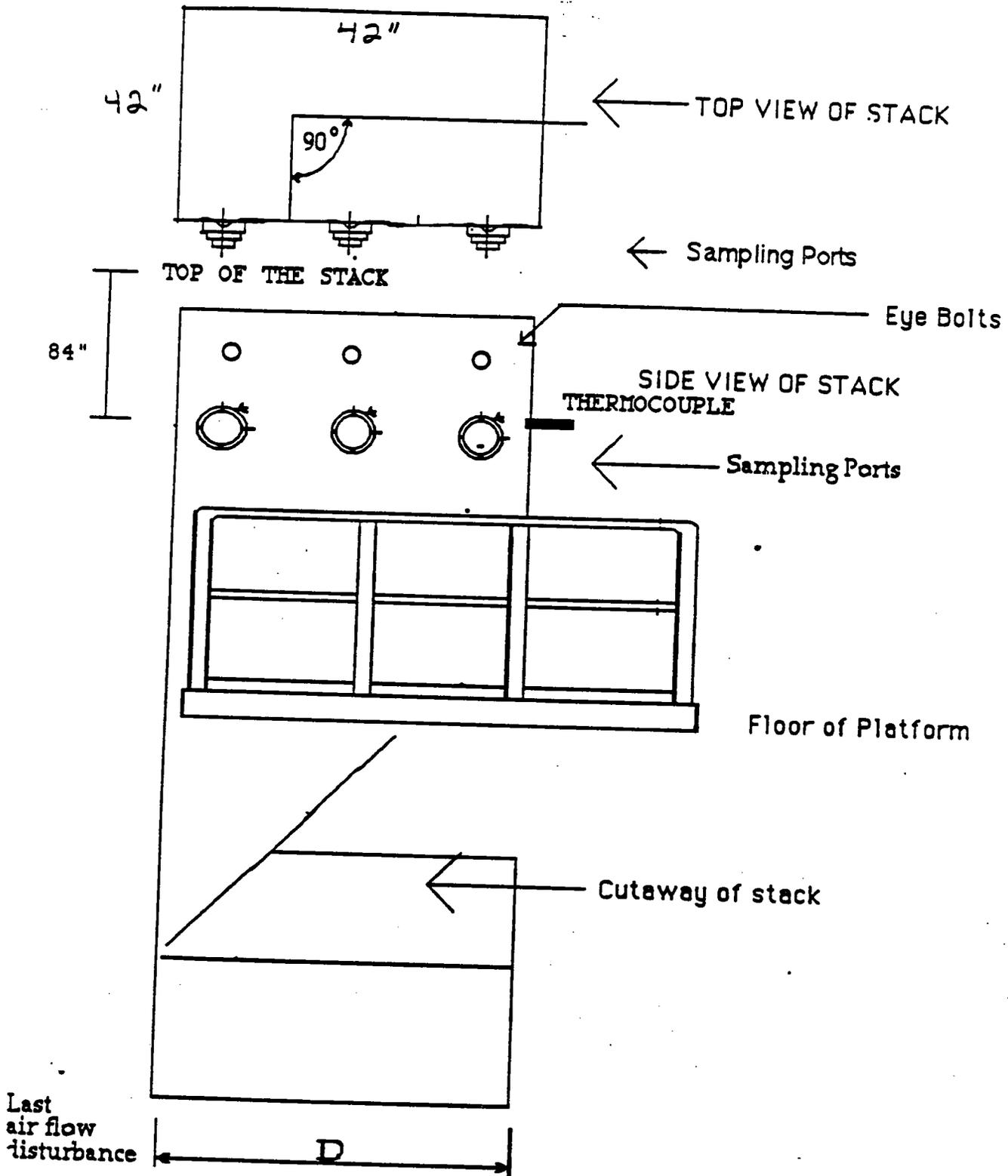


Figure 3





Client: SDAPCD - Bill Ji High

Analyst: XRS

Report #: T-1482-2

Test Date: 4-7-92

TITRIMETRIC ANALYSIS

Sample I.D./Run #	Total Sample (mls)	Aliquot mls	Normality	Titrant mls
P/N #1	250 <sup>25</sup>	10	0.009710	0.20
COND #1	220	10	0.009710	0.10
H <sub>2</sub> O <sub>2</sub> #1	190	10	0.009710	0.34
P/N #2A	130 <sup>15</sup>	10	0.009710	0.05
COND #2A	220	10	0.009710	0.10
H <sub>2</sub> O <sub>2</sub> #2A	210	10	0.009710	0.09
P/N #3	165 <sup>105</sup>	10	0.009710	0.10
COND #3	203	10	0.009710	0.24
H <sub>2</sub> O <sub>2</sub>	210	10	0.009710	0.08

COMMENTS: