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AP-42 Section Number: 1.8

Reference Number: 40

Title: Source Test Report for Particulate Emissions Twin Impingement Wet Scrubbers Boiler Number 5

Talisman Sugar Corporation

December 1991

OSW1 - TSC 6

**SOURCE TEST REPORT
for
PARTICULATE EMISSIONS**

**TWIN IMPINGEMENT WET SCRUBBER
BOILER NUMBER 5**

**TALISMAN SUGAR CORPORATION
SOUTH BAY, FLORIDA**

DECEMBER 10, 1991

Prepared for:

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Prepared by:

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REPORT CERTIFICATION

To the best of my knowledge, all applicable field and analytical procedures comply with Florida Department of Environmental Regulation requirements and all test data and plant operating data are true and correct.

Dagmar Neck

Dagmar Neck

1/15/1992

Date

1.0 INTRODUCTION

On December 10, 1991, Air Consulting and Engineering, Inc. (ACE), conducted particulate emission testing on the Wet Scrubber Outlet of Boiler 5 at Talisman Sugar Corporation located in South Bay, Florida.

Testing was performed to demonstrate compliance with the current Florida Department of Environmental Regulation (FDER) operating permit.

United States Environmental Protection Agency (EPA) Method 5 was utilized for the emission testing.

Mr. Ken Tucker of the FDER observed a portion of the testing.

Mr. Kleeman of Kleeman Engineering, Inc. coordinated testing and provided production data.

2.0 SUMMARY AND DISCUSSION OF RESULTS

Boiler Number 5 demonstrated compliance with the permit conditions.

Table 1 is a summary of the emission results and flue gas parameters.

Particulate emissions averaged 65.96 pounds per hour (lbs/Hr) and 0.264 pounds per million BTU (lbs/MMBTU) which is within the allowable emissions of 74.95 lbs/Hr and 0.300 lbs/MMBTU.

Complete emission summaries, field data sheets and laboratory data are presented in Appendices A, B, and C, respectively.

Production rate summaries are provided in Appendix D. This data was obtained from control room recordings of steam flow, temperature, and pressure as well as feed water temperature and pressure. Residue integrator and oil meter readings were recorded at the beginning and end of each particulate run.

Table 1 Emission Summary
 Boiler Number 5
 Talisman Sugar Corporation
 South Bay, Florida
 December 10, 1991

| Run Number | Flow Rate SCFMD | Stack Temp. °F | Stack Moisture % | <u>Particulate Emissions</u> | | <u>Allowable Emissions</u> | |
|------------|--------------------|----------------------|------------------------|------------------------------|-----------|----------------------------|-----------|
| | | | | lbs/Hr | lbs/MMBTU | lbs/Hr | lbs/MMBTU |
| 1 | 53711 | 163 | 34.3 | 65.19 | 0.254 | 77.01 | 0.300 |
| 2 | 54659 | 164 | 35.5 | 66.63 | 0.276 | 72.32 | 0.300 |
| 3 | 51711 | 164 | 36.1 | 66.05 | 0.262 | 75.53 | 0.300 |
| AVERAGE | 53360 | 164 | 35.3 | 65.96 | 0.264 | 74.95 | 0.300 |

3.0 PROCESS DESCRIPTION AND OPERATION

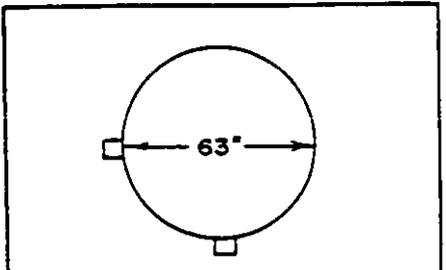
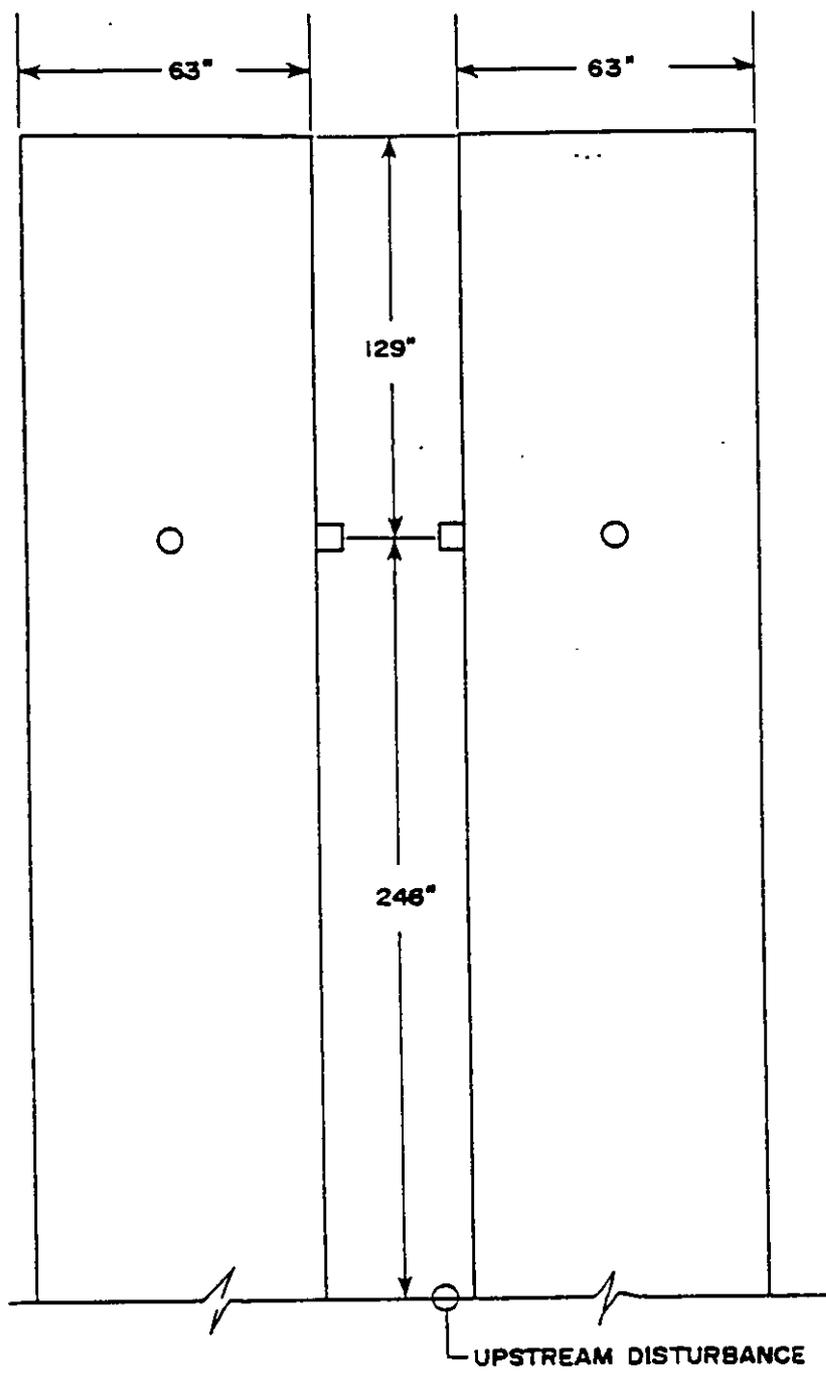
The Number 5 Boiler at Talisman Sugar Corporation is a traveling grate stoker design used primarily for bagasse fuel firing. Supplemental oil firing may also be utilized but was not used during the emission test series.

The Boiler averaged 128,783 pounds per hour (lbs/Hr) steam production over the test run period.

Oil meters, steam integrators, and other production monitoring devices were rigorously calibrated prior to the production season.

4.0 SAMPLING POINT LOCATION

The sampling point location and outlet duct schematic are provided in Figure 1.



| TRAVERSE POINT NUMBER | INCHES INSIDE STACK WALL |
|-----------------------|--------------------------|
| 1 | 1.3 |
| 2 | 4.2 |
| 3 | 7.4 |
| 4 | 11.2 |
| 5 | 15.8 |
| 6 | 22.4 |
| 7 | 40.6 |
| 8 | 47.3 |
| 9 | 51.8 |
| 10 | 55.6 |
| 11 | 58.8 |
| 12 | 61.7 |

NOTE: NOT TO SCALE

**FIGURE I.
 SAMPLING POINT LOCATION
 BOILER NO. 5
 TALISMAN SUGAR CORPORATION
 SOUTH BAY, FLORIDA**

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5.0 FIELD AND ANALYTICAL PROCEDURES

5.1 Particulate Matter Sampling and Analysis--EPA Method 5 (Glass Probe)

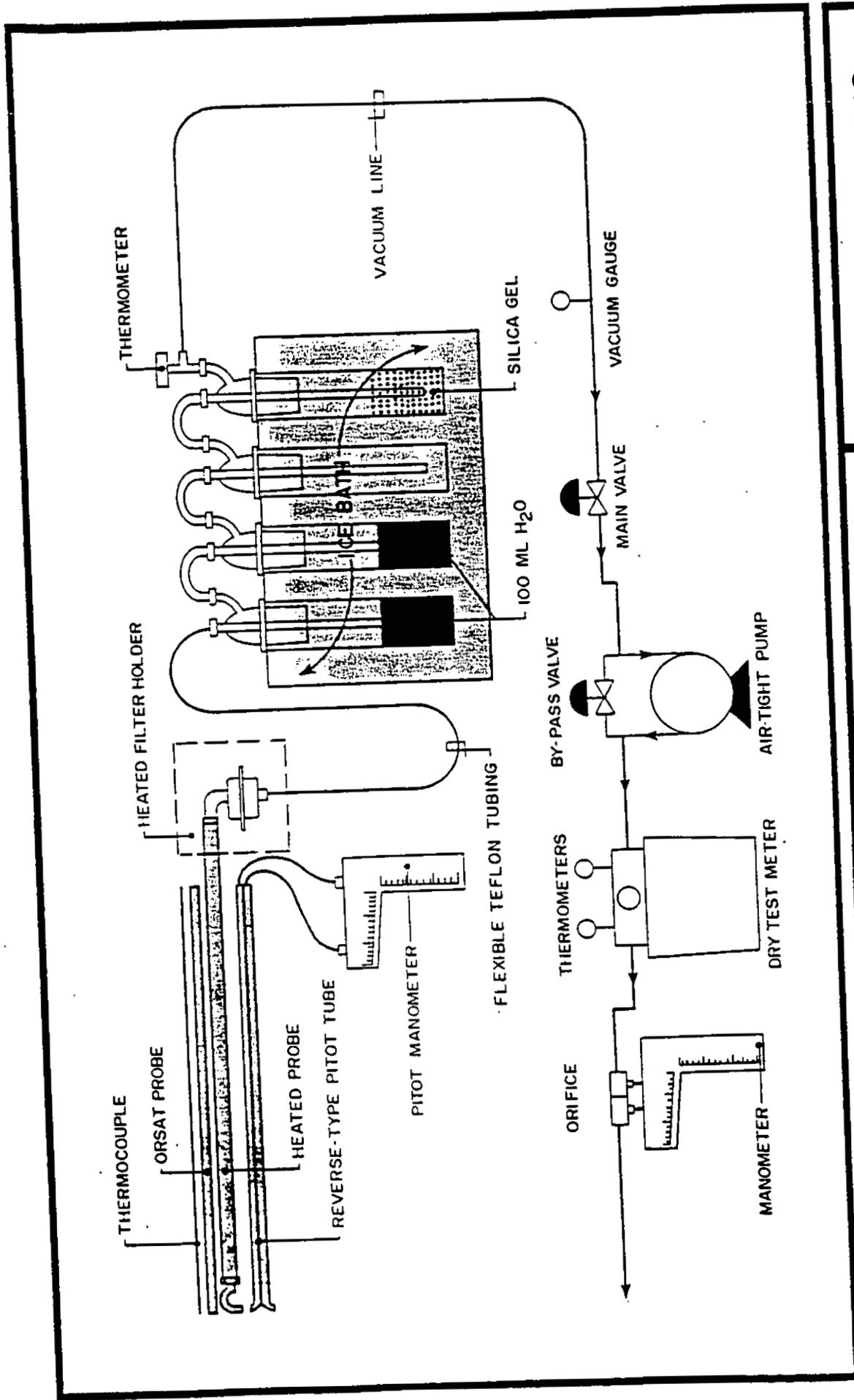
Particulate matter samples were collected by the particulate matter emission measurement method specified by the United States Environmental Protection Agency. A schematic diagram of the sampling train used is shown in Figure 2. All particulate matter captured from the nozzle to, and including, the filter was included in the calculation of the emission rate of particulate matter.

PREPARATION OF EQUIPMENT

1. FILTERS - Gelman type "A" filters were placed in a drying oven for two hours at 105 degrees C, removed and placed in a standard desiccator containing indicating silica gel, allowed to cool for two hours, and weighed to the nearest 0.1 mg. The filters were then re-desiccated for a minimum of six hours and weighed to a constant weight (less than 0.5 mg change from previous weighing). The average of the two constant weights was used as the tare weight.
2. NOZZLE, FILTER HOLDER, AND SAMPLING PROBE - The nozzle, filter holder, and sampling probe were washed vigorously with soapy water and brushes, rinsed with distilled water and acetone, and dried prior to the test program. All openings on the sampling equipment were sealed while in transit to the test site.
3. IMPINGERS - The Greenburg-Smith impingers were cleaned with a warm soapy water solution and brushes, rinsed with distilled water and acetone, and dried. The impingers were sealed tightly during transit.

TEST PROCEDURE

Prior to performing the actual particulate matter sample runs, certain stack and stack gas parameters were measured. These preliminary measurements



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**FIGURE 2
EPA METHOD 5 SAMPLING TRAIN**

included the average gas temperature, the stack gas velocity head, the stack gas moisture content, and the stack dimensions at the point where the tests were being performed. The stack gas temperature was determined by using a bi-metallic thermocouple and calibrated pyrometer. Velocity head measurements were made with calibrated type "S" pitot tube and an inclined manometer. Velocity head measurements of 0.05 inches H₂O or less were measured utilizing a micromanometer.

The sampling traverse points were selected so that a representative sample could be extracted from the gas stream. The traverse points were located in the center of equal areas, the number of which were dependent upon the distance upstream and downstream from flow disturbances.

Each particulate matter test run consisted of sampling for a specific amount of time at each traverse point. The type "S" pitot tube was connected to the sampling probe so that an instantaneous velocity head measurement could be made at each traverse point while making the test run. The stack gas temperature was also measured at each traverse point. Nomographs were used to calculate the isokinetic sampling rate at each traverse point during each test run.

The gases sampled passed through the following components: a stainless steel nozzle and glass probe; a glass fiber filter; two impingers each with 100 ml

of distilled deionized water; one impinger dry; one impinger with 200 grams of silica gel; a flexible sample line; an air-tight pump; a dry test meter; and a calibrated orifice. The second impinger had a standard tip, while the first, third, and fourth impingers had modified tips with a 0.5 inch I.D. opening.

Sample recovery was accomplished by the following procedures:

1. The pre-tared filter was removed from its holder and placed in Container 1 and sealed. (This is usually performed in the lab.)
2. All sample-exposed surfaces prior to the filter were washed with acetone and placed in Container 2, sealed and the liquid level marked.
3. The volume of water from the first three impingers was measured for the purpose of calculating the moisture in the stack gas and then discarded.
4. The used silica gel from the fourth impinger was transferred to the original tared container and sealed.

LABORATORY ANALYSIS

The three sample containers from each sample run were analyzed according to the following procedures:

1. The filter was dried at 105 degrees C for three hours, desiccated for a minimum of one hour, and weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart was made to determine constant weight.
2. The acetone from Container 2 was transferred to a tared beaker and evaporated to dryness at ambient temperature and pressure, desiccated for 24 hours, and weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart were made to determine constant weight.
3. The used silica gel in its tared container was weighed to the nearest 0.1 gram.

The total sample weight included the weight of material collected on the filter plus the weight of material collected in the nozzle, sampling probe, and front half of the filter holder.

DATA

The field data sheets, calculation sheets, and nomenclature definitions are included in the appendices of this report.

**APPENDIX A
COMPLETE EMISSION DATA
AND
SAMPLE CALCULATIONS**

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 5 BOILER
DATE: 12-10-91

| | | | |
|----------------------|------------------|-----------------|-------|
| RUN NO.: | 1 | IMPINGER ml | 395 |
| BEGIN TIME: | 925 | SILICA GEL gms. | 8.7 |
| END TIME: | 1106 | PERCENT O2 | 6.00 |
| TOTAL RUN TIME: | 96.00 min. | PERCENT CO2 | 14.00 |
| BAROMETRIC PRESSURE: | 30.15 "Hg | "F" FACTOR | 0 |
| STACK PRESSURE: | 30.15 "Hg. | | |
| NOZZLE DIAMETER: | .227 inches | PARTICULATE | |
| METER CORR. FACTOR: | 1.009 | | |
| FINAL METER: | 78.472 cubic ft. | FILTER mg. | 323.6 |
| INITIAL METER: | 41.814 cubic ft. | WASH mg. | 13.1 |
| STACK AREA: | 43.300 sq. ft. | | |

STACK 1 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | DRIF. DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|-------------|-------------|-------------|
| 1-1 | .180 | 0.424 | .270 | 163 | 68 |
| 1-2 | .180 | 0.400 | .240 | 163 | 69 |
| 1-3 | .320 | 0.566 | .480 | 163 | 69 |
| 1-4 | .180 | 0.424 | .270 | 163 | 69 |
| 1-5 | .230 | 0.480 | .350 | 163 | 69 |
| 1-6 | .280 | 0.529 | .420 | 163 | 69 |
| 1-7 | .480 | 0.693 | .720 | 162 | 70 |
| 1-8 | .590 | 0.768 | .890 | 163 | 70 |
| 1-9 | .510 | 0.714 | .770 | 163 | 70 |
| 1-10 | .370 | 0.608 | .560 | 163 | 72 |
| 1-11 | .270 | 0.520 | .410 | 162 | 72 |
| 1-12 | .200 | 0.447 | .300 | 160 | 72 |
| 2-1 | .200 | 0.447 | .300 | 163 | 73 |
| 2-2 | .190 | 0.436 | .290 | 163 | 73 |
| 2-3 | .190 | 0.436 | .290 | 163 | 73 |
| 2-4 | .170 | 0.412 | .260 | 163 | 73 |
| 2-5 | .160 | 0.400 | .240 | 163 | 74 |
| 2-6 | .180 | 0.424 | .270 | 163 | 74 |
| 2-7 | .550 | 0.742 | .830 | 163 | 74 |
| 2-8 | .600 | 0.775 | .900 | 162 | 75 |
| 2-9 | .690 | 0.831 | 1.040 | 163 | 75 |
| 2-10 | .710 | 0.843 | 1.070 | 164 | 76 |
| 2-11 | .740 | 0.860 | 1.110 | 163 | 77 |
| 2-12 | .740 | 0.860 | 1.110 | 163 | 77 |
| AVERAGES | 0.370 | 0.585 | 0.558 | 163 | 72 |

EMISSION RESULTS

| | | | |
|-------------------------------|------------|--------------------|-----------|
| NOZZLE AREA(FT ²) | 10.0002814 | | |
| AVG. VELOCITY HEAD | 0.33 "H2O | VOL. FLOW ACFM | 95784 |
| AVG. STACK TEMP.: | 163 F | VOL. FLOW SCFMD | 53711 |
| AVG. METER TEMP.: | 77 F | | |
| AVG. ORIFICE DIFFERENTIAL:--- | 0.54 "H2O | PARTICULATE DATA: | |
| METER STANDARD CUBIC FEET:--- | 36.698 | | |
| % H2O VAPOR: | 34.3 | POUNDS PER HOUR: | 65.185 |
| GAS MOL. WT. DRY: | 30.48 | POUNDS PER SCF: | 0.0000202 |
| GAS MOL. WT. WET: | 26.20 | GRAINS/SCF: | 0.142 |
| % EXCESS AIR: | 39.68 | GRAINS/SCF @ 8% O2 | 0.123 |
| AVG. STACK VEL (FPS): | 36.87 | GRAINS/SCF @50% EA | 0.132 |
| MMBTU INPUT: | 256.71 | POUNDS PER MMBTU: | 0.254 |
| PERCENT ISOKINETIC | 109.50 | | |

STACK 2 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | DRIFICE DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|---------------|-------------|-------------|
| 1-1 | .200 | 0.447 | .300 | 164 | 78 |
| 1-2 | .200 | 0.447 | .300 | 163 | 78 |
| 1-3 | .200 | 0.447 | .300 | 163 | 79 |
| 1-4 | .240 | 0.490 | .360 | 163 | 79 |
| 1-5 | .270 | 0.520 | .410 | 163 | 80 |
| 1-6 | .200 | 0.447 | .300 | 163 | 80 |
| 1-7 | .240 | 0.490 | .360 | 163 | 80 |
| 1-8 | .200 | 0.447 | .300 | 164 | 80 |
| 1-9 | .070 | 0.255 | .110 | 165 | 81 |
| 1-10 | .300 | 0.548 | .450 | 164 | 81 |
| 1-11 | .450 | 0.671 | .680 | 164 | 81 |
| 1-12 | .520 | 0.721 | .780 | 164 | 81 |
| 2-1 | .630 | 0.794 | .950 | 162 | 83 |
| 2-2 | .410 | 0.640 | .620 | 164 | 83 |
| 2-3 | .430 | 0.656 | .650 | 164 | 83 |
| 2-4 | .450 | 0.671 | .680 | 163 | 83 |
| 2-5 | .390 | 0.624 | .590 | 163 | 83 |
| 2-6 | .270 | 0.520 | .410 | 164 | 84 |
| 2-7 | .310 | 0.557 | .470 | 164 | 84 |
| 2-8 | .410 | 0.640 | .620 | 164 | 84 |
| 2-9 | .500 | 0.707 | .750 | 163 | 85 |
| 2-10 | .550 | 0.742 | .830 | 164 | 85 |
| 2-11 | .280 | 0.529 | .420 | 164 | 85 |
| 2-12 | .470 | 0.686 | .710 | 163 | 85 |
| AVERAGES | 0.341 | 0.571 | 0.515 | 164 | 82 |

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COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 5 BOILER
DATE: 12-10-91

| | | | |
|----------------------|-------------------|-----------------|-------|
| RUN NO.: | 2 | IMPINGER #1 | 386 |
| BEGIN TIME: | 1215 | SILICA GEL gms. | 7.4 |
| END TIME: | 1354 | PERCENT O2 | 6.00 |
| TOTAL RUN TIME: | 96.00 min. | PERCENT CO2 | 14.00 |
| BAROMETRIC PRESSURE: | 30.15 "Hg | "F" FACTOR | 0 |
| STACK PRESSURE: | 30.15 "Hg. | | |
| NOZZLE DIAMETER: | .227 inches | PARTICULATE | |
| METER CORR. FACTOR: | 1.009 | | |
| FINAL METER: | 113.180 cubic ft. | FILTER mg. | 304.4 |
| INITIAL METER: | 78.712 cubic ft. | WASH mg. | 9.1 |
| STACK AREA: | 43.300 sq. ft. | | |

STACK 1 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | DRIF. DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|-------------|-------------|-------------|
| 1-1 | .550 | 0.742 | .660 | 162 | 81 |
| 1-2 | .550 | 0.742 | .660 | 162 | 81 |
| 1-3 | .540 | 0.735 | .650 | 164 | 81 |
| 1-4 | .250 | 0.500 | .300 | 163 | 81 |
| 1-5 | .260 | 0.510 | .310 | 163 | 81 |
| 1-6 | .220 | 0.469 | .260 | 163 | 81 |
| 1-7 | .320 | 0.566 | .380 | 165 | 81 |
| 1-8 | .400 | 0.632 | .480 | 164 | 81 |
| 1-9 | .410 | 0.640 | .490 | 164 | 81 |
| 1-10 | .500 | 0.707 | .600 | 164 | 81 |
| 1-11 | .430 | 0.655 | .520 | 162 | 81 |
| 1-12 | .400 | 0.632 | .480 | 162 | 81 |
| 2-1 | .200 | 0.447 | .240 | 165 | 82 |
| 2-2 | .280 | 0.529 | .340 | 165 | 82 |
| 2-3 | .270 | 0.520 | .320 | 165 | 82 |
| 2-4 | .310 | 0.557 | .370 | 165 | 82 |
| 2-5 | .310 | 0.557 | .370 | 165 | 82 |
| 2-6 | .160 | 0.400 | .190 | 164 | 82 |
| 2-7 | .120 | 0.345 | .140 | 165 | 83 |
| 2-8 | .280 | 0.529 | .340 | 164 | 83 |
| 2-9 | .180 | 0.424 | .220 | 165 | 83 |
| 2-10 | .330 | 0.574 | .400 | 164 | 84 |
| 2-11 | .360 | 0.600 | .430 | 164 | 84 |
| 2-12 | .580 | 0.762 | .700 | 164 | 84 |
| AVERAGES | 0.342 | 0.574 | 0.410 | 164 | 82 |

EMISSION RESULTS

| | | | |
|----------------------------|------------|---------------------|-----------|
| NOZZLE AREA(FT2) | 10.0002614 | | |
| AVG. VELOCITY HEAD | 0.36 "H2O | VOL. FLOW ACFM | 99311 |
| AVG. STACK TEMP.: | 164 F | VOL. FLOW SCFMD | 54659 |
| AVG. METER TEMP.: | 85 F | | |
| AVG. ORIFICE DIFFERENTIAL: | 0.45 "H2O | PARTICULATE DATA: | |
| METER STANDARD CUBIC FEET: | 34.019 | | |
| % H2O VAPOR: | 35.5 | POUNDS PER HOUR: | 66.627 |
| GAS MOL. WT. DRY: | 30.48 | POUNDS PER SCF: | 0.0000203 |
| GAS MOL. WT. WET: | 26.05 | GRAINS/SCF: | 0.142 |
| % EXCESS AIR: | 39.68 | GRAINS/SCF @ 8% O2 | 0.123 |
| AVG. STACK VEL. (FPS) | 38.23 | GRAINS/SCF @ 50% EA | 0.132 |
| MMBTU INPUT: | 241.08 | POUNDS PER MMBTU: | 0.276 |
| PERCENT ISOINETIC | 99.74 | | |

STACK 2 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | ORIFICE DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|---------------|-------------|-------------|
| 1-1 | .220 | 0.489 | .260 | 164 | 85 |
| 1-2 | .280 | 0.529 | .340 | 165 | 85 |
| 1-3 | .280 | 0.529 | .340 | 165 | 86 |
| 1-4 | .220 | 0.489 | .260 | 165 | 86 |
| 1-5 | .200 | 0.447 | .240 | 165 | 86 |
| 1-6 | .180 | 0.424 | .220 | 165 | 86 |
| 1-7 | .520 | 0.721 | .620 | 164 | 87 |
| 1-8 | .500 | 0.707 | .600 | 163 | 87 |
| 1-9 | .600 | 0.775 | .720 | 164 | 87 |
| 1-10 | .630 | 0.794 | .760 | 164 | 87 |
| 1-11 | .680 | 0.825 | .820 | 163 | 87 |
| 1-12 | .700 | 0.837 | .840 | 164 | 87 |
| 2-1 | .420 | 0.648 | .500 | 163 | 88 |
| 2-2 | .340 | 0.583 | .410 | 163 | 88 |
| 2-3 | .370 | 0.608 | .440 | 164 | 88 |
| 2-4 | .410 | 0.640 | .490 | 163 | 88 |
| 2-5 | .300 | 0.548 | .360 | 164 | 88 |
| 2-6 | .280 | 0.529 | .340 | 164 | 89 |
| 2-7 | .500 | 0.707 | .600 | 163 | 89 |
| 2-8 | .590 | 0.768 | .710 | 164 | 89 |
| 2-9 | .600 | 0.775 | .720 | 163 | 90 |
| 2-10 | .370 | 0.608 | .440 | 165 | 90 |
| 2-11 | .280 | 0.529 | .340 | 164 | 90 |
| 2-12 | .180 | 0.424 | .220 | 164 | 90 |
| | | | | | 76 |
| AVERAGES | 0.402 | 0.621 | 0.483 | 164 | 87 |

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 5 BOILER
DATE: 12-10-91

| | | | |
|----------------------|-------------------|-----------------|-------|
| RUN NO.: | 3 | IMPINGER ml | 384 |
| BEGIN TIME: | 1445 | SILICA GEL gms. | 8.0 |
| END TIME: | 1625 | PERCENT O2 | 6.00 |
| TOTAL RUN TIME: | 96.00 min. | PERCENT CO2 | 14.00 |
| BAROMETRIC PRESSURE: | 30.15 "Hg | "F" FACTOR | 0 |
| STACK PRESSURE: | 30.15 "Hg. | | |
| NOZZLE DIAMETER: | .227 inches | PARTICULATE | |
| METER CORR. FACTOR: | 1.009 | ----- | |
| FINAL METER: | 147.060 cubic ft. | FILTER mg. | 310.0 |
| INITIAL METER: | 113.400 cubic ft. | WASH mg. | 8.0 |
| STACK AREA: | 43.300 sq. ft. | | |

Avg = 6.0

STACK 1 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | ORIF. DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|-------------|-------------|-------------|
| 1-1 | .150 | 0.387 | .180 | 164 | 87 |
| 1-2 | .300 | 0.548 | .360 | 163 | 87 |
| 1-3 | .250 | 0.500 | .300 | 162 | 87 |
| 1-4 | .240 | 0.490 | .290 | 162 | 87 |
| 1-5 | .300 | 0.548 | .360 | 162 | 87 |
| 1-6 | .450 | 0.671 | .540 | 162 | 87 |
| 1-7 | .550 | 0.742 | .660 | 162 | 87 |
| 1-8 | .660 | 0.812 | .790 | 163 | 87 |
| 1-9 | .840 | 0.883 | .410 | 163 | 87 |
| 1-10 | .400 | 0.632 | .480 | 163 | 87 |
| 1-11 | .150 | 0.387 | .180 | 163 | 87 |
| 1-12 | .150 | 0.387 | .180 | 162 | 87 |
| 2-1 | .200 | 0.447 | .240 | 162 | 87 |
| 2-2 | .200 | 0.447 | .240 | 162 | 87 |
| 2-3 | .240 | 0.490 | .290 | 163 | 88 |
| 2-4 | .250 | 0.500 | .300 | 163 | 88 |
| 2-5 | .180 | 0.424 | .220 | 163 | 88 |
| 2-6 | .110 | 0.332 | .130 | 163 | 88 |
| 2-7 | .520 | 0.721 | .620 | 163 | 88 |
| 2-8 | .620 | 0.787 | .740 | 163 | 88 |
| 2-9 | .680 | 0.825 | .820 | 163 | 88 |
| 2-10 | .500 | 0.707 | .600 | 163 | 89 |
| 2-11 | .800 | 0.894 | .960 | 163 | 89 |
| 2-12 | .890 | 0.943 | 1.070 | 162 | 89 |
| AVERAGES | 0.380 | 0.592 | 0.457 | 163 | 88 |

EMISSION RESULTS

| | | | |
|----------------------------|------------|--------------------|-----------|
| NOZZLE AREA(FT2) | 10.0002814 | | |
| AVG. VELOCITY HEAD | 0.32 "H2O | VOL. FLOW ACFM | 94882 |
| AVG. STACK TEMP.: | 164 F | VOL. FLOW SCFMD | 51711 |
| AVG. METER TEMP.: | 89 F | | |
| AVG. ORIFICE DIFFERENTIAL: | 0.42 "H2O | PARTICULATE DATA: | |
| METER STANDARD CUBIC FEET: | 32.932 | | |
| % H2O VAPOR: | 36.1 | POUNDS PER HOUR: | 66.048 |
| GAS MOL. WT. DRY: | 30.48 | POUNDS PER SCF : | 0.0000213 |
| GAS MOL. WT. WET: | 25.97 | GRAINS/SCF: | 0.149 |
| % EXCESS AIR: | 39.68 | GRAINS/SCF @ 8% O2 | 0.129 |
| AVG. STACK VEL.(FPS) | 36.52 | GRAINS/SCF @50% EA | 0.139 |
| MMBTU INPUT: | 251.78 | POUNDS PER MMBTU: | 0.262 |
| PERCENT ISO KINETIC | 102.08 | | |

avg = 164

Avg = 53,360

STACK 2 DATA INPUTS

| PORT-POINT | VELOCITY HEAD | SQUARE RT. VEL. HEAD | DRIFICE DIFF. | STACK TEMP. | METER TEMP. |
|------------|---------------|----------------------|---------------|-------------|-------------|
| 1-1 | .300 | 0.548 | .360 | 162 | 90 |
| 1-2 | .300 | 0.548 | .360 | 162 | 90 |
| 1-3 | .330 | 0.574 | .400 | 163 | 91 |
| 1-4 | .060 | 0.245 | .070 | 165 | 91 |
| 1-5 | .090 | 0.300 | .110 | 164 | 91 |
| 1-6 | .080 | 0.283 | .090 | 164 | 91 |
| 1-7 | .280 | 0.529 | .340 | 164 | 91 |
| 1-8 | .340 | 0.583 | .410 | 164 | 91 |
| 1-9 | .260 | 0.510 | .310 | 164 | 91 |
| 1-10 | .130 | 0.361 | .160 | 164 | 91 |
| 1-11 | .450 | 0.671 | .540 | 165 | 92 |
| 1-12 | .450 | 0.671 | .540 | 166 | 92 |
| 2-1 | .550 | 0.742 | .660 | 166 | 92 |
| 2-2 | .480 | 0.693 | .580 | 166 | 92 |
| 2-3 | .430 | 0.656 | .520 | 165 | 92 |
| 2-4 | .340 | 0.583 | .410 | 165 | 93 |
| 2-5 | .330 | 0.574 | .400 | 164 | 93 |
| 2-6 | .280 | 0.529 | .340 | 166 | 93 |
| 2-7 | .330 | 0.574 | .400 | 166 | 93 |
| 2-8 | .370 | 0.608 | .440 | 166 | 93 |
| 2-9 | .480 | 0.693 | .580 | 166 | 93 |
| 2-10 | .520 | 0.721 | .620 | 163 | 93 |
| 2-11 | .280 | 0.529 | .340 | 164 | 90 |
| 2-12 | .180 | 0.424 | .220 | 164 | 90 |
| AVERAGES | 0.318 | 0.548 | 0.383 | 165 | 91 |

APPENDIX B
FIELD DATA SHEETS

STACK SAMPLING FIELD DATA SHEET



2106 N. W. 67th PLACE, Suites 9 & 10
GAINESVILLE, FLORIDA 32606

PLANT Talisman Sugar Corporation
 SOURCE Boiler # 5
 PLANT LOCATION South Bay Florida
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES P.M.
 DATE 12-10-91 RUN NO. 1
 TIME START 0925 TIME END 1106
 SAMPLE TIME 2 / 48 (min/pt) = 96 Total min
 ASSUMED MOISTURE 30 % FDA 70
 NOMOGRAPH C_1 1.5 PITOT CORR. .84
 P_b 30.15 "Hg P_s 30.15 "Hg
 WEATHER Clear TEMP. 74 °F
 METER BOX NO. 6 H. 1.91 Y. 1.009
 NOZZLE CAL. .227 .227 .228 = .227
 STACK DIMENSIONS 6.3"
 STACK AREA 43.3 ft² EFFECTIVE _____ ft²
 STACK HEIGHT _____ ft
 STACK DIAMETER: UPSTRM. _____ DNSTRM. _____
 PORT SIZE 4 in. NIPPLE LENGTH 6 in.
 U CORD LENGTH 125"
 REMARKS: _____

TEST ID TSSCIAS
 PAGE 1 OF 3

MAT'L PROCESSING RATE _____
 GAS METER READINGS: FINAL 078.472 ft.³
 INITIAL 041.814 ft.³
 NET 36.658 ft.³
 FILTER NO. 3661 IMP. VOL. GAIN 395 ml.
 SIL GEL NO. 6 WT. GAIN 8.1 ml.
 TOTAL CONDENSATE 403.7 ml.

ORSAT

| | 1 | 2 | 3 | 4 | AVG. |
|-------------------|------|------|---|---|------|
| % CO ₂ | 14.0 | 14.0 | | | 14.0 |
| % O ₂ | 6.0 | 6.0 | | | 6.0 |
| % CO | | | | | |
| % N ₂ | | | | | |

F₀ = _____ F₀ RANGE = _____
 ORSAT ANALYZER _____
 LEAK CHECKS _____
 PRE 0.007 cfm 15 "Hg POST 0.00 cfm 15 "Hg
 METER BOX/PUMP _____ GAS SAMPLE SYST. _____
 ORSAT BAG _____
 PITOT TUBE NO. _____ PRE-TEST OK
 POST-TEST (+) 0.00 / 15 H₂O/Sec
 POST-TEST (-) 0.00 / 15 H₂O/Sec
 PYROMETER NO. 3
 BOX OPERATOR Gowthorpe PROBE HOLDER McFarland

| PORT AND TRAVERSE POINT NUMBER SOURCE | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (FT ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP (°F) | SAMPLE BOX TEMP (°F) | LAST IMPINGER TEMP. F | DRY GAS METER TEMP. (°F) | VACUUM ON SAMPLE TRAIN ("Hg) |
|---------------------------------------|--|------------|--------------------------------------|---------------------|--|--------|---------------------|----------------------|-----------------------|--------------------------|------------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-1 | | 0927 | 042.32 | .18 | .27 | .27 | 163 | 248 | 62 | 68 | 2.0 |
| 2 | | 0929 | 042.99 | .16 | .24 | .24 | 163 | 248 | 60 | 69 | 2.0 |
| 3 | | 0931 | 043.73 | .32 | .48 | .48 | 163 | 253 | 56 | 69 | 2.0 |
| 4 | | 0933 | 044.21 | .18 | .27 | .27 | 163 | 253 | 56 | 69 | 2.0 |
| 5 | | 0935 | 044.86 | .23 | .35 | .35 | 163 | 250 | 56 | 69 | 2.0 |
| 6 | | 0937 | 045.68 | .28 | .42 | .42 | 163 | 250 | 56 | 69 | 2.0 |



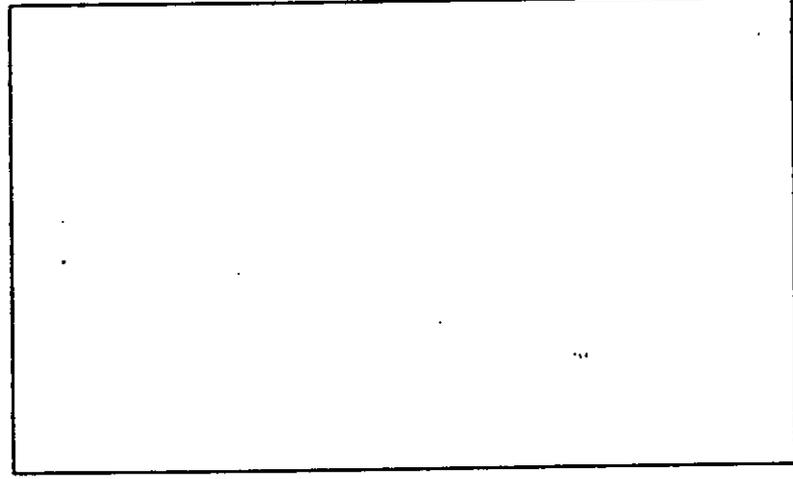
| PORT AND TRAVERSE POINT NUMBER | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (ft ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP (°F) | SAMPLE BOX TEMP (°F) | LAST IMPINGING TEMP (°F) | DRY GAS METER TEMP (°F) | VACUUM ON SAMPLE TRAIN ("Hg) |
|--------------------------------|--|------------|--------------------------------------|---------------------|--|--------|---------------------|----------------------|--------------------------|-------------------------|------------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-7 | | 0939 | 046.42 | .48 | .72 | .72 | 162 | 255 | 52 | 70 | 3.0 |
| 8 | | 0941 | 047.46 | .59 | .89 | .89 | 163 | 254 | 52 | 70 | 4.0 |
| 9 | | 0943 | 048.41 | .51 | .77 | .77 | 163 | 254 | 52 | 70 | 4.0 |
| 10 | | 0945 | 049.14 | .37 | .56 | .56 | 163 | 255 | 54 | 72 | 3.0 |
| 11 | | 0947 | 049.90 | .27 | .41 | .41 | 162 | 255 | 53 | 72 | 3.0 |
| 12 | | 0949 | 050.50 | .20 | .30 | .30 | 160 | 254 | 53 | 72 | 3.0 |
| 2-1 | | 0953 | 051.05 | .20 | .30 | .30 | 163 | 250 | 56 | 73 | 3.0 |
| 2 | | 0955 | 051.62 | .19 | .29 | .29 | 163 | 249 | 55 | 73 | 3.0 |
| 3 | | 0957 | 052.30 | .19 | .29 | .29 | 162 | 248 | 55 | 73 | 3.0 |
| 4 | | 0959 | 052.80 | .17 | .26 | .26 | 163 | 248 | 57 | 73 | 3.0 |
| 5 | | 1001 | 053.31 | .16 | .24 | .24 | 163 | 247 | 58 | 74 | 3.0 |
| 6 | | 1003 | 053.93 | .18 | .27 | .27 | 163 | 247 | 58 | 74 | 3.0 |
| 7 | | 1005 | 054.05 | .55 | .83 | .83 | 163 | 247 | 56 | 74 | 6.0 |
| 8 | | 1007 | 055.80 | .60 | .90 | .90 | 162 | 246 | 56 | 76 | 6.0 |
| 9 | | 1009 | 056.83 | .69 | 1.04 | 1.04 | 163 | 246 | 56 | 76 | 8.0 |
| 10 | | 1011 | 057.92 | .71 | 1.07 | 1.07 | 164 | 250 | 56 | 76 | 8.0 |
| 11 | | 1013 | 059.14 | .74 | 1.11 | 1.11 | 163 | 257 | 56 | 77 | 9.0 |
| 12 | | 1015 | 060.28 | .74 | 1.11 | 1.11 | 163 | 257 | 56 | 77 | 9.0 |
| North | | | | | | | | | | | |
| 1-1 | | 1018 | 060.85 | .20 | .30 | .30 | 164 | 264 | 58 | 78 | 4.0 |
| 2 | | 1020 | 061.37 | .20 | .30 | .30 | 163 | 259 | 57 | 78 | 5.0 |
| 3 | | 1022 | 062.07 | .20 | .30 | .30 | 163 | 258 | 56 | 79 | 5.0 |
| 4 | | 1024 | 062.61 | .24 | .36 | .36 | 163 | 226 | 56 | 79 | 5.0 |
| 5 | | 1026 | 063.42 | .27 | .41 | .41 | 163 | 228 | 57 | 80 | 6.0 |
| 6 | | 1028 | 064.01 | .20 | .30 | .30 | 163 | 243 | 57 | 80 | 5.0 |
| 7 | | 1030 | 064.61 | .24 | .36 | .36 | 163 | 248 | 57 | 80 | 5.0 |

STACK SAMPLING FIELD DATA SHEET



PLANT Talisman Sugar Corporation
 SOURCE Boiler #5
 PLANT LOCATION South Bay, Florida
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES P.M
 DATE 12-10-91 RUN NO. 2
 TIME START 1215 TIME END 1354
 SAMPLE TIME 2 / 48 (min/pt) = 96 Total min
 ASSUMED MOISTURE 34 % FDA .670
 NOMOGRAPH C₁ 1.2 PITOT CORR. .84
 P_b 30.15 "Hg P_s 30.15 "Hg
 WEATHER Clear TEMP. 75 °F
 METER BOX NO. 6 H 1.91 Y 1.009
 NOZZLE CAL. .227 .227 .228 = .227
 STACK DIMENSIONS 63"
 STACK AREA 43.3 ft² EFFECTIVE 112
 STACK HEIGHT ft
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE 4 in. NIPPLE LENGTH 60 in.
 U CORD LENGTH 125'
 REMARKS: _____

2106 N. W. 67th PLACE - Suites 9810
 GAINESVILLE, FLORIDA 32606



TEST ID TS50AAS
 PAGE 1 OF 3

MAT'L PROCESSING RATE _____
 GAS METER READINGS: FINAL 13.180 ft³
 INITIAL 078.712 ft³
 NET 34468 ft³
 FILTER NO. 3662 IMP. VOL. GAIN 386 ml.
 SIL GEL NO. 44 WT. GAIN 7.4 ml.
 TOTAL CONDENSATE 3934 ml.

ORSAT

| | 1 | 2 | 3 | 4 | AVG. |
|-------------------|---|------|---|---|------|
| % CO ₂ | | | | | |
| % O ₂ | | 14.0 | | | |
| % CO | | 6.0 | | | |
| % N ₂ | | | | | |

F₀ = _____ F₀ RANGE = _____
 ORSAT ANALYZER _____
 LEAK CHECKS _____
 PRE 0.00 cfm 15 "Hg POST 0.003 cfm 15 "Hg
 METER BOX/PUMP _____ GAS SAMPLE SYST. _____
 ORSAT BAG _____ PRE-TEST OK
 PITOT TUBE NO. _____
 POST-TEST(+) 0.03 / 15 H₂O/Sec
 POST-TEST(-) 0.00 / 15 H₂O/Sec
 PYROMETER NO. 3
 BOX OPERATOR Gault PROBE HOLDER McFarland

| PORT AND TRAVERSE POINT NUMBER | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (FT. ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP (°F) | SAMPLE BOX TEMP (°F) | LAST IMPINGER TEMP (°F) | DRY GAS METER TEMP (°F) | VACUUM ON SAMPLE TRAIN ("Hg) |
|--------------------------------|--|------------|---------------------------------------|---------------------|--|--------|---------------------|----------------------|-------------------------|-------------------------|------------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-1 | | 1217 | 079.60 | .55 | .66 | .66 | 162 | 262 | 64 | 81 | 2.0 |
| 2 | | 1219 | 080.15 | .55 | .66 | .66 | 162 | 262 | 64 | 81 | 2.0 |
| 3 | | 1221 | 081.72 | .54 | .65 | .65 | 164 | 261 | 60 | 81 | 2.0 |
| 4 | | 1223 | 082.25 | .25 | .30 | .30 | 163 | 264 | 60 | 81 | 2.0 |
| 5 | | 1225 | 082.72 | .26 | .31 | .31 | 163 | 265 | 59 | 81 | 2.0 |
| 6 | | 1227 | 083.22 | .22 | .26 | .26 | 163 | 261 | 59 | 81 | 2.0 |

| PORT AND TRAVERSE POINT NUMBER | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (ft ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP. (°F) | SAMPLE BOX TEMP. (°F) | LAST IMPINGER TEMP. (°F) | DRY GAS METER TEMP. (°F) | VACUUM ON SAMPLE TRAIN ("Hg) |
|--------------------------------|--|------------|--------------------------------------|---------------------|--|--------|----------------------|-----------------------|--------------------------|--------------------------|------------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-7 | | 1229 | 083.92 | .32 | .38 | .38 | 165 | 261 | 56 | 81 | 2.0 |
| 8 | | 1231 | 084.65 | .40 | .48 | .48 | 164 | 261 | 55 | 81 | 2.0 |
| 9 | | 1233 | 085.31 | .41 | .49 | .49 | 164 | 257 | 54 | 81 | 3.0 |
| 10 | | 1235 | 086.25 | .50 | .60 | .60 | 164 | 257 | 54 | 81 | 3.0 |
| 11 | | 1237 | 087.11 | .43 | .52 | .52 | 162 | 264 | 54 | 81 | 3.0 |
| 12 | | 1239 | 087.85 | .40 | .48 | .48 | 162 | 264 | 54 | 81 | 3.0 |
| 2-1 | | 1242 | 088.40 | .20 | .24 | .24 | 165 | 270 | 55 | 82 | 2.5 |
| 2 | | 1244 | 089.02 | .28 | .34 | .34 | 165 | 260 | 54 | 82 | 3.0 |
| 3 | | 1246 | 089.64 | .27 | .32 | .32 | 165 | 260 | 54 | 82 | 3.0 |
| 4 | | 1248 | 090.35 | .31 | .37 | .37 | 165 | 260 | 54 | 82 | 3.0 |
| 5 | | 1250 | 091.00 | .31 | .37 | .37 | 165 | 251 | 54 | 82 | 3.0 |
| 6 | | 1252 | 091.52 | .16 | .19 | .19 | 164 | 245 | 54 | 82 | 3.0 |
| 7 | | 1254 | 092.01 | .12 | .14 | .14 | 165 | 244 | 57 | 83 | 2.0 |
| 8 | | 1256 | 092.56 | .28 | .34 | .34 | 164 | 242 | 55 | 83 | 2.0 |
| 9 | | 1258 | 093.05 | .18 | .22 | .22 | 165 | 241 | 55 | 83 | 3.0 |
| 10 | | 1300 | 093.75 | .33 | .40 | .40 | 164 | 241 | 54 | 84 | 4.0 |
| 11 | | 1302 | 094.55 | .36 | .43 | .43 | 164 | 241 | 52 | 84 | 4.0 |
| 12 | | 1304 | 095.40 | .58 | .70 | .70 | 164 | 241 | 51 | 84 | 5.0 |
| South | | | | | | | | | | | |
| 1-1 | | 1308 | 095.91 | .22 | .26 | .26 | 164 | 253 | 55 | 85 | 4.0 |
| 2 | | 1310 | 096.53 | .28 | .34 | .34 | 165 | 253 | 54 | 85 | 4.0 |
| 3 | | 1312 | 097.23 | .28 | .34 | .34 | 165 | 248 | 54 | 86 | 5.0 |
| 4 | | 1314 | 097.81 | .22 | .26 | .26 | 165 | 249 | 54 | 86 | 4.0 |
| 5 | | 1316 | 098.31 | .20 | .24 | .24 | 165 | 250 | 54 | 86 | 4.0 |
| 6 | | 1318 | 098.85 | .18 | .22 | .22 | 165 | 252 | 55 | 86 | 4.0 |
| 7 | | 1320 | 099.65 | .52 | .62 | .62 | 164 | 251 | 55 | 87 | 6.0 |

STACK SAMPLING FIELD DATA SHEET

PLANT Idalman Sugar Corporation
 SOURCE Boiler #5
 PLANT LOCATION South Bay, Florida
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES P.M.
 DATE 12-10-91 RUN NO. 3
 TIME START 1445 TIME END 1625
 SAMPLE TIME 2 / 48 (min/pt) = 96 Total min
 ASSUMED MOISTURE 30 % FDA .70
 NOMOGRAPH 1.2 PITOT CORR. .84
 P_b 30.15 "Hg P_s 30.15 "Hg
 WEATHER Clear TEMP. 78 °F
 METER BOX NO. 6 H 1.91 Y 1.009
 NOZZLE CAL. .227 .227 .228 .227
 STACK DIMENSIONS 63"
 STACK AREA 43.3 ft² EFFECTIVE _____ ft²
 STACK HEIGHT _____ ft
 STACK DIAMETER: UPSTRM. _____ DNSTRM. _____
 PORT SIZE 4 in. NIPPLE LENGTH 6 in.
 U CORD LENGTH 125"
 REMARKS: _____



2106 N. W. 67th PLACE, Suites 9 & 10
 GAINESVILLE, FLORIDA 32606

TEST ID TS5C3AS
 PAGE 1 OF 3

MAT'L PROCESSING RATE _____
 GAS METER READINGS: FINAL 147.060 ft³
 INITIAL 113.400 ft³
 NET 33.660 ft³
 FILTER NO. 3660 IMP. VOL. GAIN 384 ml.
 SIL GEL NO. 100 WT. GAIN 8.10 ml.
 TOTAL CONDENSATE _____ ml.

ORSAT

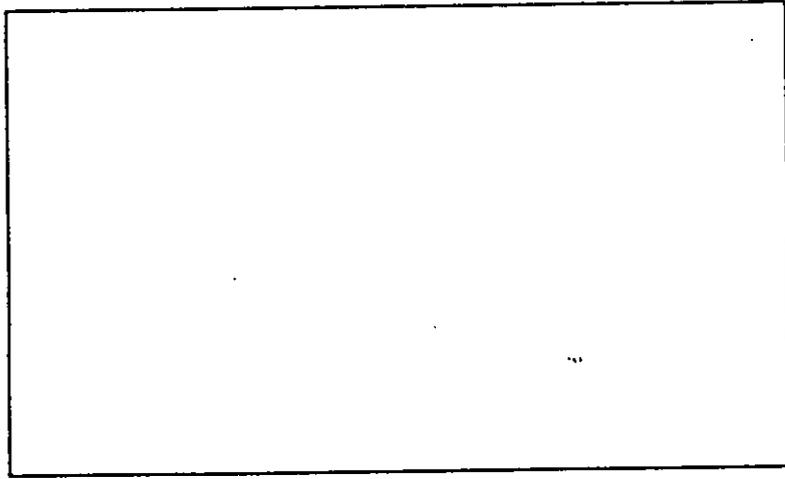
| | 1 | 2 | 3 | 4 | AVG. |
|-------------------|------|------|---|---|------|
| % CO ₂ | 14.0 | 14.0 | | | 14.0 |
| % O ₂ | 6.0 | 6.0 | | | 6.0 |
| % CO | | | | | |
| % N ₂ | | | | | |

F₀ = _____ F₀ RANGE = _____
 ORSAT ANALYZER _____

LEAK CHECKS

PRE 0.02 cfm 15 "Hg POST 0.00 cfm 15 "Hg
 METER BOX/PUMP _____ GAS SAMPLE SYST. _____
 ORSAT BAG _____
 PITOT TUBE NO. _____ PRE-TEST OK
 POST-TEST(+) 0.00 / 15 H₂O/Sec
 POST-TEST(-) 0.00 / 15 H₂O/Sec
 PYROMETER NO. 3

BOX OPERATOR Santhosh PROBE HOLDER McFarland



| PORT AND TRAVERSE POINT NUMBER | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (FT ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP. (°F) | SAMPLE BOX TEMP. (°F) | LAST IMPINGER TEMP. (°F) | DRY GAS METER TEMP. (°F) | VACUUM ON SAMPLE TRAIN ("Hg) |
|--------------------------------|--|------------|--------------------------------------|---------------------|--|--------|----------------------|-----------------------|--------------------------|--------------------------|------------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-1 | | 1447 | 114.57 | .15 | .18 | .18 | 164 | 275 | 62 | 87 | 2.0 |
| 2 | | 1449 | 115.00 | .30 | .36 | .36 | 163 | 265 | 61 | 87 | 2.0 |
| 3 | | 1451 | 115.74 | .25 | .30 | .30 | 162 | 250 | 60 | 87 | 2.0 |
| 4 | | 1453 | 116.55 | .24 | .29 | .29 | 162 | 247 | 60 | 87 | 2.0 |
| 5 | | 1455 | 117.15 | .30 | .36 | .36 | 162 | 247 | 60 | 87 | 2.0 |
| 6 | | 1457 | 117.92 | .45 | .54 | .54 | 162 | 247 | 60 | 87 | 2.0 |

| PORT AND TRAVERSE POINT NUMBER | DISTANCE FROM INSIDE STACK WALL / COMMENTS | CLOCK TIME | GAS METER READING (ft ³) | STACK VELOCITY HEAD | METER ORIFICE PRESS. DIFF. ("H ₂ O) | | STACK GAS TEMP. (°F) | SAMPLE BOX TEMP. (°F) | LAST IMPINGER TEMP. (°F) | DRY GAS METER TEMP. (°F) | VACUUM ON SAMPLE TRAP ("Hg) |
|--------------------------------|--|------------|--------------------------------------|---------------------|--|--------|----------------------|-----------------------|--------------------------|--------------------------|-----------------------------|
| | | | | | CALC. | ACTUAL | | | | | |
| 1-7 | | 1459 | 118.65 | .55 | .66 | .66 | 162 | 251 | 60 | 87 | 3.0 |
| 8 | | 1501 | 119.44 | .66 | .79 | .79 | 163 | 251 | 60 | 87 | 4.0 |
| 9 | | 1503 | 120.20 | .34 | .41 | .41 | 163 | 260 | 59 | 87 | 4.0 |
| 10 | | 1505 | 121.01 | .40 | .48 | .48 | 163 | 260 | 59 | 87 | 4.0 |
| 11 | | 1507 | 121.52 | .15 | .18 | .18 | 163 | 257 | 60 | 87 | 2.0 |
| 12 | | 1509 | 122.07 | .15 | .18 | .18 | 163 | 267 | 60 | 87 | 2.0 |
| 2-1 | | 1512 | 122.58 | .20 | .24 | .24 | 162 | 267 | 60 | 88 | 3.0 |
| 2 | | 1514 | 122.91 | .20 | .24 | .24 | 162 | 265 | 59 | 88 | 3.0 |
| 3 | | 1516 | 123.10 | .24 | .29 | .29 | 163 | 266 | 59 | 88 | 3.0 |
| 4 | | 1518 | 123.70 | .25 | .30 | .30 | 163 | 264 | 59 | 88 | 3.0 |
| 5 | | 1520 | 124.32 | .18 | .22 | .22 | 163 | 231 | 59 | 88 | 3.0 |
| 6 | | 1522 | 124.91 | .11 | .13 | .13 | 163 | 229 | 59 | 88 | 4.0 |
| 7 | | 1524 | 125.50 | .52 | .62 | .62 | 163 | 229 | 59 | 88 | 4.0 |
| 8 | | 1526 | 126.45 | .62 | .74 | .74 | 163 | 235 | 59 | 88 | 5.0 |
| 9 | | 1528 | 127.31 | .68 | .82 | .82 | 163 | 242 | 59 | 88 | 6.0 |
| 10 | | 1530 | 128.10 | .50 | .60 | .60 | 163 | 243 | 59 | 89 | 5.0 |
| 11 | | 1532 | 129.01 | .80 | .96 | .96 | 163 | 238 | 59 | 89 | 7.0 |
| 12 | | 1534 | 130.21 | .89 | 1.07 | 1.07 | 162 | 239 | 58 | 89 | 8.0 |
| North | | | | | | | | | | | |
| 1-1 | | 1538 | 131.06 | .30 | .36 | .36 | 162 | 273 | 59 | 90 | 5.0 |
| 2 | | 1540 | 131.82 | .30 | .36 | .36 | 162 | 270 | 58 | 90 | 5.0 |
| 3 | | 1542 | 122.58 | .33 | .40 | .40 | 163 | 264 | 58 | 91 | 5.0 |
| 4 | | 1544 | 132.90 | .06 | .07 | .07 | 165 | 263 | 58 | 91 | 2.0 |
| 5 | | 1546 | 133.22 | .09 | .11 | .11 | 164 | 265 | 58 | 91 | 2.0 |
| 6 | | 1548 | 133.51 | .08 | .09 | .09 | 164 | 264 | 58 | 91 | 2.0 |
| 7 | | 1550 | 134.00 | .28 | .34 | .34 | 164 | 264 | 58 | 91 | 5.0 |

APPENDIX C
LABORATORY ANALYSIS

AIR CONSULTING & ENGINEERING, inc.

PARTICULATE LAB DATA

SOURCE Talmanitt-SC

| PROBE Rinse | RUN 1 | RUN 2 | RUN 3 | BLANK | Liquid Level |
|--------------------------|---------------------|---------------------|---------------------|---------------------|----------------------------|
| CONTAINER NUMBER | 174 | 136 | 526 | 100 | 100 |
| TOTAL VOLUME (ml) | 174 | 136 | 135 | 100 | |
| 1st GROSS WEIGHT (g) | 106.5021 | 103.5321 | 103.9199 | 110.6271 | DATE & TIME: 12-10-91 5:25 |
| 2nd GROSS WEIGHT (g) | 106.5021 | 103.5821 | 103.5500 | 110.6271 | DATE & TIME: 12-11-91 5:18 |
| AVERAGE GROSS WEIGHT (g) | 106.5021 | 103.5821 | 103.5500 | 110.6271 | |
| TARE WEIGHT (g) | 106.4870 | 103.5730 | 103.5420 | 110.6271 | |
| SUB NET WEIGHT (mg) | 106.4870 | 103.5730 | 103.5420 | 110.6271 | |
| ACETONE BLANK (g) | | | | | |
| TOTAL NET WEIGHT (mg) | 106.4870 | 103.5730 | 103.5420 | 110.6271 | |

NOTE: In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

| FILTER | RUN 1 | RUN 2 | RUN 3 | BLANK | DATE & TIME |
|--------------------------|-------------------|-------------------|-------------------|-------------------|----------------------------|
| FILTER NUMBER | 3661 | 3662 | 3660 | 3150 | 12-10-91 23:09 |
| 1st GROSS WEIGHT (g) | 0.7518 | 0.7269 | 0.7352 | 0.4015 | DATE & TIME: 12-11-91 5:24 |
| 2nd GROSS WEIGHT (g) | 0.7518 | 0.7269 | 0.7352 | 0.4015 | |
| AVERAGE GROSS WEIGHT (g) | 0.7518 | 0.7269 | 0.7352 | 0.4015 | |
| TARE WEIGHT (g) | 0.7518 | 0.7269 | 0.7352 | 0.4015 | |
| SUB NET WEIGHT (g) | 0.3236 | 0.3044 | 0.3100 | 0.0000 | |
| TOTAL NET WEIGHT (mg) | 0.3236 | 0.3044 | 0.3100 | 0.0000 | |

TARE BALANCE CHECK

1st GROSS WEIGHT BALANCE CHECK

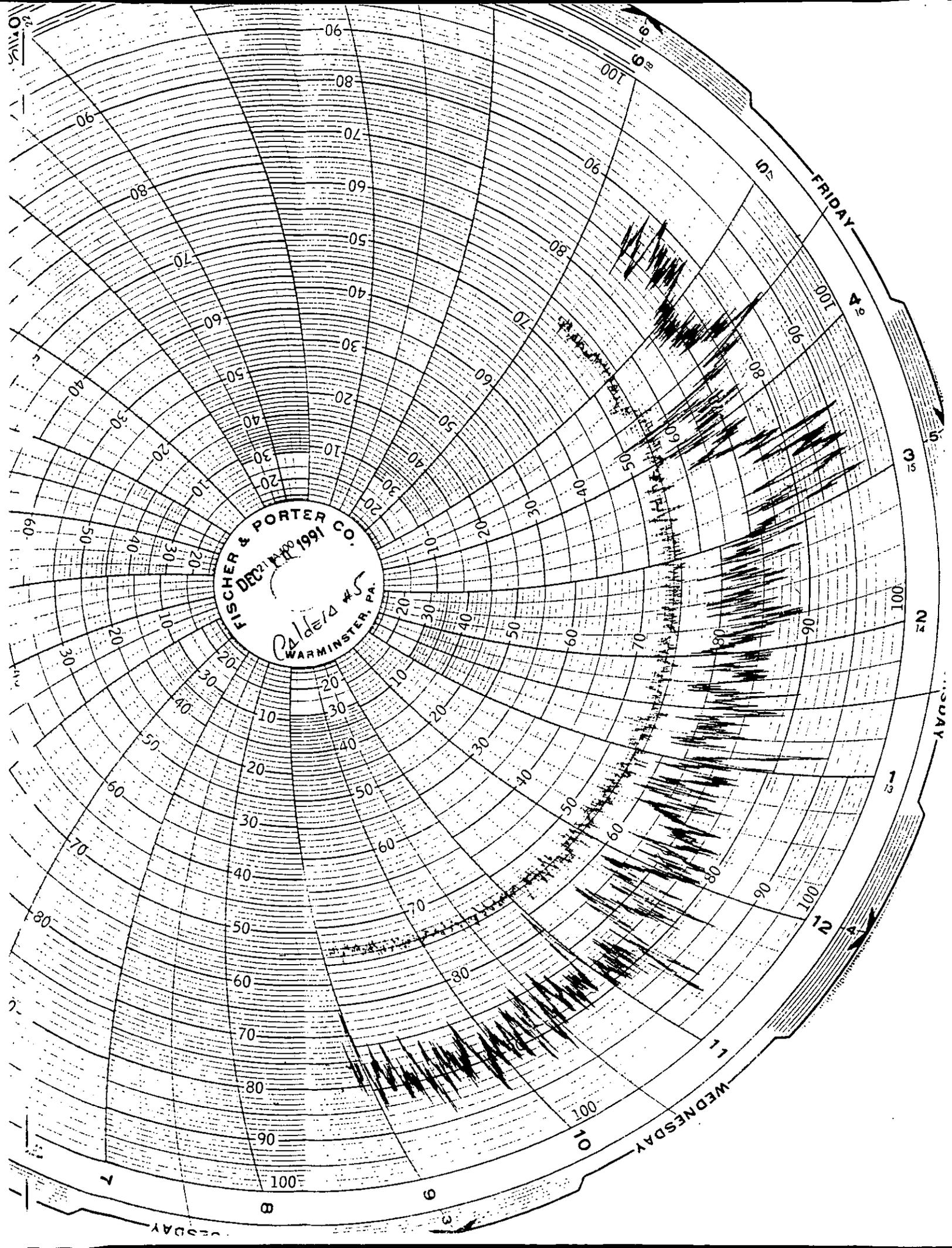
2nd GROSS WEIGHT BALANCE CHECK

SEE LAB BOOK

0 10.0g
 0.5g 100.0g
 %RH 68 DATE 12-10-91
 Signature Christy Z. Mack

0 10.0g
 0.5g 100.0g
 %RH 62 DATE 12-11-91
 Signature Christy Z. Mack

APPENDIX D
PRODUCTION RATE
CERTIFICATION



FISCHER & PORTER CO.
WARMING, PA.
Palder #5

FRIDAY

WEDNESDAY

TUESDAY

PROCESS DATA

INSTALLATION Boiler #5

COMPANY TALISMAN SUGAR CORP.

DATE DEC. 10, 1991

TYPE OF INSTALLATION BAGASSE BOILER

TYPE OF MATERIAL PROCESSED STEAM

TYPE OF FUEL USED BAGASSE

TYPE OF POLLUTION CONTROL SYSTEM VENTURI DUAL WET SCRUBBERS PLUS DRY COLLECTOR

| | NORMAL | RUN 1 | RUN 2 | RUN 3 |
|---------------------------|-------------|-------------|-------------|-------------|
| SCRUBBER WATER FLOW (GPM) | <u>1200</u> | <u>1200</u> | <u>1200</u> | <u>1200</u> |
| PRESSURE DROP (INCHES) | <u>12</u> | <u>11.5</u> | <u>12.0</u> | <u>11.8</u> |

REPORTED BY FRANK KLEEMAN

BOILER DATA SHEET

COMPANY TALISMAN SUGAR CORP REPORTED BY FRANK KLEEMAN

DATE DEC. 10, 1991

INTEGRATOR FACTOR X 100 BOILER NO. 5

FUEL OIL USED No Oil

| TIME | INTEGRATOR | FLOW | STEAM | TEMP. | FEED WATER | |
|-------------------|------------|---------------------|----------------|------------|------------|----------------|
| | | | X 500 PRESSURE | | TEMP. | PRESSURE |
| 9 25 | 635935 | 92 | 295 | 562 | 257 | 380 |
| 10 00 | 6717 | 90 | 295 | 564 | 257 | 390 |
| 10 30 | 7384 | 85 | 295 | 561 | 258 | 380 |
| 11 01 | 8052 | 88 | 295 | 560 | 258 | 390 |
| <u>96 MINUTES</u> | | <u>2117</u> | <u>295</u> | <u>562</u> | <u>258</u> | <u>385 AVG</u> |
| 1.6 HRS. | | | | | | |
| | | $2117 \times 100 =$ | 211700 | | | |
| | | <u>2117.00</u> | | | | |
| | | <u>1.6 HRS.</u> | $=$ 132300 | LBS/HR | | |
| 12 15 | 639638 | 89 | 295 | 562 | 257 | 390 |
| 12 55 | 640464 | 82 | 295 | 559 | 257 | 390 |
| 1 30 | 1192 | 85 | 290 | 560 | 256 | 400 |
| 1 51 | 1627 | 83 | 290 | 558 | 257 | 400 |
| <u>96 MINUTES</u> | | <u>1989</u> | <u>292</u> | <u>560</u> | <u>257</u> | <u>395 AVG</u> |
| 1.6 HRS. | | | | | | |
| | | $1989 \times 100 =$ | 124300 | LBS/HR | | |
| | | <u>1.6</u> | | | | |
| 2 45 | 642747 | 89 | 290 | 560 | 256 | 400 |
| 3 15 | 3402 | 95 | 290 | 560 | 256 | 400 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |

1 RUN 1

2 RUN 2

3 RUN 3

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

```

-----
PLANT:   TALISMAN SUGAR CORPORATION           DATE:   12-10-91
LOCATION:  SOUTH BAY, FLORIDA                 RUN NUMBER   1
SOURCE:  NUMBER 5 BOILER, SCRUBBER OUTLET    TIME:       0925-1101
-----

```

```

TIME INTERVAL----- 96 MINUTES

OIL:
FINAL OIL----- N/A
BEGIN OIL----- N/A
FACTOR----- 1

STEAM:
FINAL STEAM----- 638052
BEGIN STEAM----- 635935
FACTOR----- 100
TEMPERATURE----- 562 DEGREES F
PRESSURE----- 295 PSIG
                310 PSIA

FEEDWATER:
TEMPERATURE----- 257 DEGREES F
PRESSURE----- 380 PSIG
                395 PSIA

HEAT INPUT:
STEAM----- 1292.7 BTU/LB
FEEDWATER----- 225.6 BTU/LB
NET STEAM----- 1067.1 BTU/LB
STEAM RATE----- 132313 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 256.71 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 256.71 MMBTUH

ALLOWABLES:
ALLOWABLE EMISSION (OIL)----- .10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- .30 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 77.01 LB/HR
TOTAL ACTUAL EMISSION----- 65.18 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.300 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.254 LB/MMBTU

```


AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

```

-----
PLANT:   TALISMAN SUGAR CORPORATION      DATE:   12-10-91
LOCATION:  SOUTH BAY, FLORIDA             RUN NUMBER   2
SOURCE:  NUMBER 5 BOILER, SCRUBBER OUTLET TIME:   1215-1351
-----

```

TIME INTERVAL----- 96 MINUTES

OIL:

```

FINAL OIL----- N/A
BEGIN OIL----- N/A
FACTOR----- 1

```

STEAM:

```

FINAL STEAM----- 641627
BEGIN STEAM----- 639638
FACTOR----- 100
TEMPERATURE----- 561 DEGREES F
PRESSURE----- 295 PSIG
                310 PSIA

```

FEEDWATER:

```

TEMPERATURE----- 257 DEGREES F
PRESSURE----- 380 PSIG
                395 PSIA

```

HEAT INPUT:

```

STEAM----- 1292.2 BTU/LB
FEEDWATER----- 225.6 BTU/LB
NET STEAM----- 1066.6 BTU/LB
STEAM RATE----- 124313 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 241.08 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

```

```

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

```

```

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 241.08 MMBTUH

```

ALLOWABLES:

```

ALLOWABLE EMISSION (OIL)----- .10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- .30 LB/MMBTU

```

```

TOTAL ALLOWABLE EMISSION----- 72.32 LB/HR
TOTAL ACTUAL EMISSION----- 66.63 LB/HR

```

```

TOTAL ALLOWABLE EMISSION----- 0.300 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.276 LB/MMBTU

```


AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

```

-----
PLANT:   TALISMAN SUGAR CORPORATION           DATE:   12-10-91
LOCATION:  SOUTH BAY, FLORIDA                 RUN NUMBER   3
SOURCE:  NUMBER 5 BOILER, SCRUBBER OUTLET    TIME:       1445-1641
-----

```

TIME INTERVAL----- 116 MINUTES

OIL:

```

FINAL OIL----- N/A
BEGIN OIL----- N/A
FACTOR----- 1

```

STEAM:

```

FINAL STEAM----- 645255
BEGIN STEAM----- 642747
FACTOR----- 100
TEMPERATURE----- 560 DEGREES F
PRESSURE----- 290 PSIG
                305 PSIA

```

FEEDWATER:

```

TEMPERATURE----- 256 DEGREES F
PRESSURE----- 400 PSIG
                415 PSIA

```

HEAT INPUT:

```

STEAM----- 1292.1 BTU/LB
FEEDWATER----- 224.6 BTU/LB
NET STEAM----- 1067.5 BTU/LB
STEAM RATE----- 125724 LB/HR
BOILER EFFICIENCY----- 85.0 %
TOTAL FUEL HEAT INPUT----- 251.78 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

```

```

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

```

```

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 251.78 MMBTUH

```

ALLOWABLES:

```

ALLOWABLE EMISSION (OIL)----- .10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- .30 LB/MMBTU

```

```

TOTAL ALLOWABLE EMISSION----- 75.53 LB/HR
TOTAL ACTUAL EMISSION----- 66.05 LB/HR

```

```

TOTAL ALLOWABLE EMISSION----- 0.300 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.262 LB/MMBTU

```

AVG = 249.84

APPENDIX E
QUALITY ASSURANCE
AND
CHAIN OF CUSTODY

STANDARD METER CALIBRATION
Meter Number 1040616

Air Consulting and Engineering, Inc. (ACE) uses a dry gas meter for the calibration standard. This meter has been calibrated against a wet test meter in triplicate. This data was used to generate a standard meter calibration curve (see next page). Field meter calibrations are corrected to this curve using the following formula:

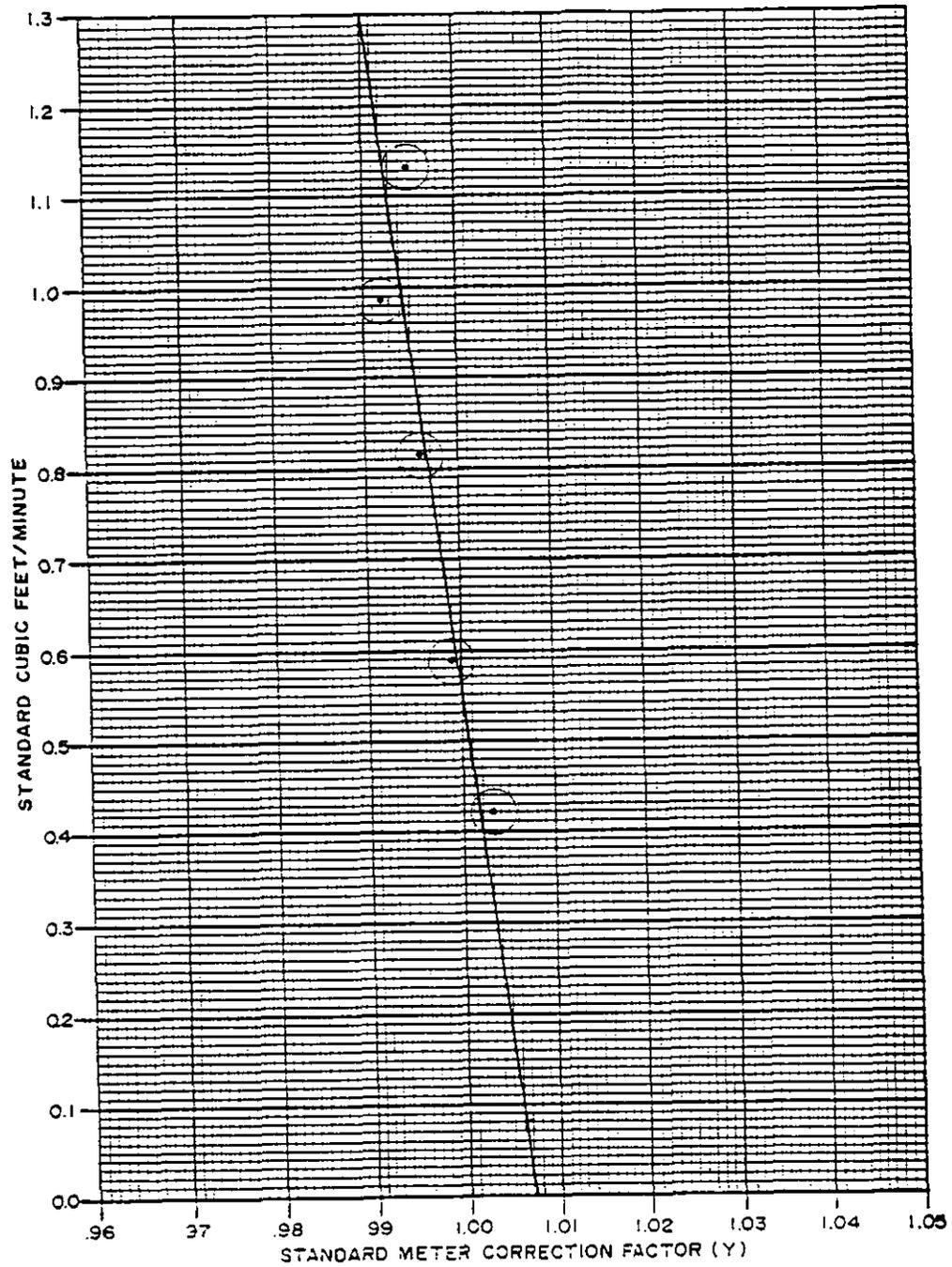
$$Y_a \times Y_s = Y$$

Y_a = actual ratio of field meter to standard meter

Y_s = ratio of standard meter to wet test meter at a given
flow rate (from Calibration Curve)

Y = corrected ratio of field meter

The dry standard meter was calibrated on June 11, 1991, and is checked and/or recalibrated at least annually.



STANDARD METER CALIBRATION
CURVE

JUNE 11, 1991

AIR CONSULTING
and
ENGINEERING

AIR CONSULTING & ENGINEERING

STANDARD METER CALIBRATION

DATE 6-13-91

LEAK CHECK 0.000 CFM at 13 In Hg.

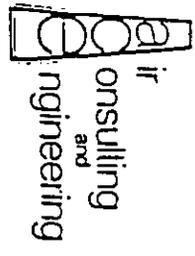
METER SERIAL NUMBER 107 Dells

BAROMETRIC PRESSURE 30.12 In Hg.

STD GAS METER TEMPERATURE 71 °F / ASTM GLASS THERMOMETER TEMPERATURE 74 °F

| WET ΔH | STD ΔH | GAS VOLUME, WET TEST METER | | | GAS VOLUME, STD GAS METER | | | TEMP WET TEST METER (°F) | TEMP OF STD METER (°F) | TIME (Minutes) |
|-----------|-----------|----------------------------|--------|---------------------------|---------------------------|--------|---------------------------|-----------------------------------|---------------------------------|-------------------|
| | | INITIAL | FINAL | ACTUAL ft ³ | INITIAL | FINAL | ACTUAL ft ³ | | | |
| -0.3 | -0.60 | 6.012 | 11.553 | 5.511 | 0.003 | 5.500 | 5.497 | -7.1 | 7.1 | 13 |
| -0.3 | -0.60 | 1.553 | 7.030 | 5.479 | 5.500 | 10.979 | 5.479 | 7.5 | 7.5 | 13 |
| -0.3 | -0.60 | 1.030 | 12.509 | 5.411 | 10.979 | 16.450 | 5.411 | 7.5 | 7.5 | 13 |
| -0.3 | -0.60 | 0.843 | 8.143 | 5.390 | 16.804 | 22.127 | 5.323 | 7.5 | 7.6 | 9 |
| -0.3 | -0.60 | 6.143 | 13.430 | 5.387 | 22.127 | 27.442 | 5.315 | 7.5 | 7.6 | 9 |
| -0.3 | -0.60 | 3.430 | 8.703 | 5.273 | 27.442 | 32.753 | 5.311 | 7.5 | 7.7 | 9 |
| -0.4 | -1.6 | 9.252 | 14.995 | 5.743 | 33.311 | 39.123 | 5.812 | 7.6 | 7.8 | 7 |
| -0.4 | -1.6 | 4.995 | 10.713 | 5.718 | 39.123 | 44.909 | 5.786 | 7.6 | 7.8 | 7 |
| -0.4 | -1.6 | 0.113 | 6.445 | 5.732 | 44.909 | 50.701 | 5.798 | 7.6 | 7.8 | 7 |
| -0.5 | -2.1 | 6.941 | 12.917 | 5.976 | 51.214 | 57.292 | 6.018 | 7.6 | 7.8 | 6 |
| -0.5 | -2.1 | 3.917 | 8.898 | 5.981 | 57.292 | 63.375 | 6.083 | 7.6 | 7.8 | 6 |
| -0.5 | -2.1 | 8.898 | 14.873 | 5.975 | 63.375 | 69.452 | 6.077 | 7.6 | 7.8 | 6 |
| -0.5 | -2.1 | 5.278 | 10.488 | 5.710 | 69.452 | 75.663 | 5.797 | 7.6 | 7.8 | 5 |
| -0.7 | -2.7 | 0.983 | 6.708 | 5.720 | 75.663 | 81.474 | 5.811 | -7.6 | 7.8 | 5 |
| -0.7 | -2.7 | 6.708 | 12.386 | 5.678 | 81.474 | 87.247 | 5.773 | 7.6 | 7.8 | 5 |

CALIBRATED BY: R. F. Stalder



Air Consulting
and
Engineering

| Run | Y | SCFM |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Run 1 | 1.004 | 0.422 | 0.998 | 0.584 | 0.996 | 0.814 | 0.992 | 0.988 | 0.995 | 1.132 |
| Run 2 | 1.001 | 0.419 | 0.999 | 0.584 | 0.996 | 0.810 | 0.992 | 0.989 | 0.995 | 1.134 |
| Run 3 | 1.003 | 0.419 | 0.999 | 0.582 | 0.996 | 0.812 | 0.992 | 0.988 | 0.994 | 1.126 |
| Average | 1.003 | 0.420 | 0.999 | 0.583 | 0.996 | 0.812 | 0.992 | 0.988 | 0.995 | 1.131 |

AIR CONSULTING & ENGINEERING ANNUAL METER CALIBRATION

DATE 10-3-91 LEAK CHECK 0.500 CFM at 15 in. Hg.

METER BOX NUMBER 6 BAROMETRIC PRESSURE 29.94 in. Hg.

DRY GAS METER TEMPERATURE 82 °F / ASTM GLASS THERMOMETER TEMPERATURE 82 °F

| ΔHS | AVERAGE ΔHD | GAS VOLUME, STANDARD METER | | GAS VOLUME, DRY GAS METER | | TEMP. STD. METER | TEMP. OF DRY METER | TIME (Minutes) | TIMER | | |
|-----|-------------|----------------------------|---------|---------------------------|---------|------------------|--------------------|----------------|-------|-------|------------------------|
| | | INITIAL | FINAL | ACTUAL ft ³ | INITIAL | | | | | FINAL | ACTUAL ft ³ |
| -08 | 0.5 | 65.936 | 72.128 | 6.192 | 550.574 | 556.690 | 6.176 | 81 | 82 | 16 | 16 |
| -13 | 1.0 | 72.551 | 78.148 | 5.597 | 557.102 | 562.651 | 5.549 | 81 | 82 | 10 | 10 |
| -18 | 1.5 | 78.417 | 84.504 | 6.087 | 562.914 | 568.942 | 6.028 | 81 | 83 | 9 | 9 |
| -24 | 2.0 | 84.709 | 90.083 | 5.374 | 569.145 | 574.456 | 5.311 | 81 | 83 | 7 | 7 |
| -35 | 3.0 | 90.361 | 96.607 | 5.646 | 574.724 | 580.290 | 5.566 | 81 | 84 | 6 | 6 |
| -46 | 4.0 | 96.243 | 101.631 | 5.388 | 580.521 | 585.818 | 5.297 | 81 | 85 | 5 | 5 |

| DELTA H | Y _a | SCFM | Y _s | Y |
|---------|----------------|-------|----------------|-------|
| 1.909 | 1.003 | 0.378 | 1.004 | 1.007 |
| 1.825 | 1.008 | 0.547 | 1.001 | 1.009 |
| 1.871 | 1.010 | 0.661 | 1.000 | 1.009 |
| 1.937 | 1.011 | 0.750 | 0.998 | 1.009 |
| 1.930 | 1.013 | 0.919 | 0.996 | 1.008 |
| 1.959 | 1.015 | 1.052 | 0.994 | 1.008 |
| MEAN: | 1.905 | 1.010 | 0.999 | 1.009 |

CALIBRATED BY: A. F. Gabel

AIR CONSULTING & ENGINEERING, inc.

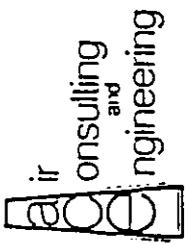
POST TEST CALIBRATION

DATE 12-20-91 METER BOX NUMBER 6 LEAK CHECK 0.00 CFM at 12 in. Hg
 CLIENT TALISMAN SUGAR SOURCE ALL THERMOCOUPLE NUMBER _____ PYROMETER NUMBER _____
 FLIGHT SERVICE Pb 30.48 in. Hg ACE BAROMETER Pb 20.48 in. Hg
 ASTM GLASS THERMOMETER 150 °F / THERMOCOUPLE 150 °F ASIM GLASS THERMOMETER 68 °F / METER TEMP 68 °F

| ΔHS | AVERAGE ΔHD | GAS VOLUME, STANDARD METER | | | GAS VOLUME, DRY GAS METER | | | TEMP STANDARD METER | TEMP OF DRY METER (Minutes) | MAX. VACUUM in. Hg | |
|-----|-------------|----------------------------|---------|------------------------|---------------------------|---------|------------------------|---------------------|-----------------------------|--------------------|----|
| | | INITIAL | FINAL | ACTUAL ft ³ | INITIAL | FINAL | ACTUAL ft ³ | | | | |
| .56 | .55 | 554.039 | 559.628 | 5.589 | 843.390 | 849.146 | 5.756 | 75 74 | 81 83 | 14 | 12 |
| .51 | .47 | 559.628 | 565.175 | 5.547 | 849.146 | 854.877 | 5.731 | 74 73 | 83 84 | 15 | 12 |
| .67 | .74 | 565.175 | 590.212 | 5.537 | 854.877 | 860.615 | 5.738 | 73 73 | 84 85 | 12 | 12 |

CALIBRATED BY: Carolyn Mitchell

DELTA H
 1.885
 1.867
 1.935
 Y_a
 0.986
 0.987
 0.985
 SCFM
 0.402
 0.373
 0.466
 Y_S
 1.000
 1.000
 0.999
 Y
 0.986
 0.987
 0.984



MEAN: 1.896 0.986 1.000 0.986

AIR CONSULTING & ENGINEERING, INC. PYROMETER CALIBRATION

DATE 9-4-90 PYROMETER NUMBER #3

| SOURCE (SPECIFY) | GLASS THERMOMETER WITH NBS MERCURY (°F) | PYROMETER (°F) | DEGREE DIFFERENCE | PERCENT DIFFERENCE |
|------------------|---|----------------|-------------------|--------------------|
| ICE BATH | <u>32</u> | <u>34</u> | <u>2</u> | <u>0.4</u> |
| AMBIENT | <u>80</u> | <u>81</u> | <u>1</u> | <u>0.2</u> |
| HOT OVEN | <u>268</u> | <u>264</u> | <u>4</u> | <u>0.6</u> |

FDER - MAXIMUM 5° DIFFERENCE

EPA
$$\left[\frac{(\text{REF. TEMP } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$$

CALIBRATED BY: Sup B Row

AIR CONSULTING & ENGINEERING, INC. PITOT TUBE CALIBRATION

DATE CALIBRATED 10-7-91 PITOT TUBE 59

IS PITOT TUBE ASSEMBLY LEVEL YES ARE PITOT TUBE OPENINGS DAMAGED NO

$\alpha_1 =$ 0 ° (<10°), $\alpha_2 =$ 1 ° (<10°), $\beta_1 =$ 2 ° (<5°), $\beta_2 =$ 1 ° (<5°)

$\gamma =$ 1 ° $\theta =$ 1 ° $A =$ 1.165 in. = ($P_a + P_b$)

$z = A \sin \gamma =$ 0.017 in.; $< 0.32 / < 1/8$ in.

$w = A \sin \theta =$ 0.017 in.; $< 0.08 / < 1/32$ in.

P_a 0.583 in. P_b 0.582 in. D_1 .375

WAS CALIBRATION REQUIRED NO

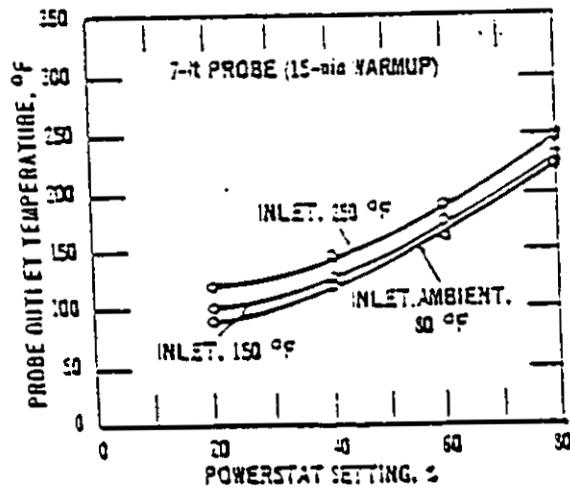
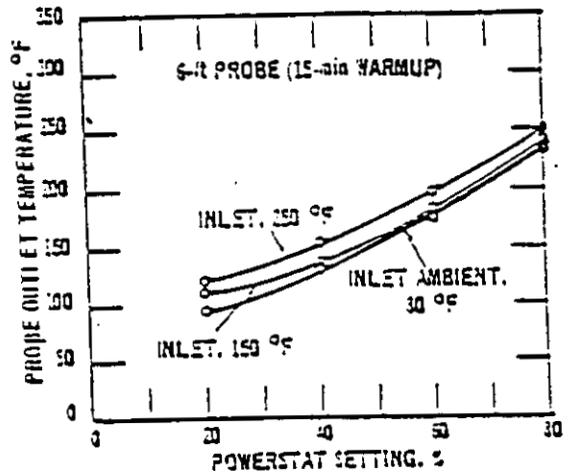
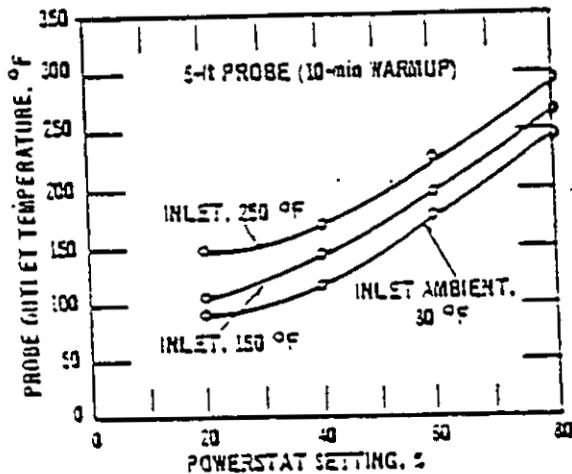
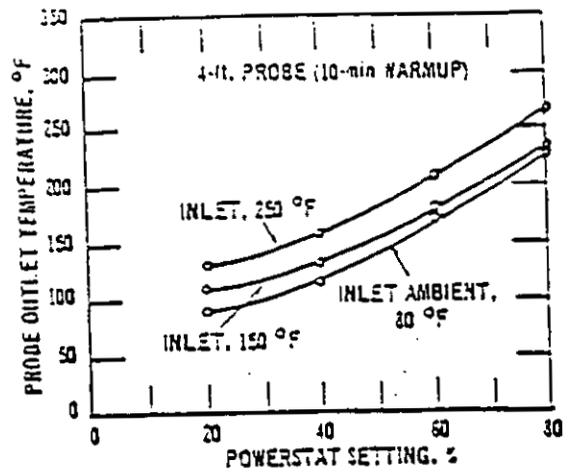
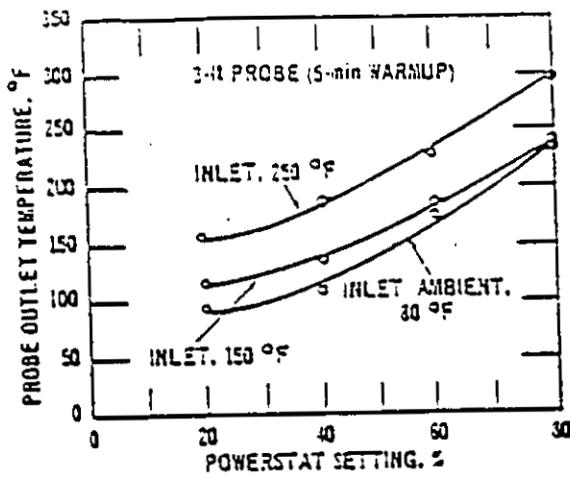
THERMOCOUPLE CALIBRATION

| SOURCE (SPECIFY) | ASTM GLASS THERMOMETER WITH MERCURY (°F) | PYROMETER (°F) | PERCENT DIFFERENCE |
|------------------|--|----------------|--------------------|
| ICE BATH | <u>42</u> | <u>42</u> | <u>0</u> |
| AMBIENT | <u>78</u> | <u>78</u> | <u>0</u> |
| HOT OVEN | <u>402</u> | <u>400</u> | <u>0.38</u> |

FDER - MAXIMUM 0° DIFFERENCE

CALIBRATED BY: Sid Carter

EPA [(REF. TEMP. °F + 460°) - (PYROMETER TEMP. °F + 480°)] 100 ≤ 1.5%
REF. TEMP. °F + 460°



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

Probe temperatures.

APPENDIX F
PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

AIR CONSULTING AND ENGINEERING, INC.

Stephen L. Neck, P.E.
Project Manager

Early McFarland
Field Participant

Gerard Gauthreaux
Field Participant

Christy Neck
Laboratory Analysis

Dagmar Neck
Report Preparation

Candace V. Taylor
Document Production

KLEEMAN ENGINEERING

Frank Kleeman
Test Coordinator
Production Data

FDER

Ken Tucker
Test Observer