

Potential Drinking Water Effects of Bromide Discharges from Coal-Fired Electric Power Plants

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1.0 Introduction

Production of wastewater containing bromide is associated with fossil fuel extraction and utilization (i.e., oil and gas production and coal-fired steam electric power plants). When discharged to receiving water, these wastewaters can increase bromide concentrations in surface waters that are used as potable drinking water supplies. The presence of bromide in source waters significantly increases the formation of carcinogenic disinfection by-products (DBPs) in finished drinking water, increasing the population's exposure to these by-products.

Bromide concentrations in surface waters in the United States have typically been quite low, with average values inland ranging from 0.014-0.2 mg/L. Furthermore, bromide has a relatively high human toxicity threshold, and ecotoxicity is observed only at high concentrations. Thus, the discharge of bromide has been left largely unregulated in the United States. While naturally occurring bromide poses low risk to humans, anthropogenic brominated organic compounds are well known to exhibit significant ecotoxicity and to be associated with negative endocrine, reproductive, and carcinogenic outcomes in humans upon consumption or inhalation.

Many brominated organics are used in industrial and consumer products in ways designed to limit human exposure (e.g., brominated flame retardants are applied to foam inside furniture). However, incidental production of brominated organics can occur in treating drinking water, and these compounds persist in the finished water that is consumed. Brominated disinfection by-products form when source waters containing bromide are disinfected with chemical oxidants (e.g., chlorine, ozone). During the disinfection, bromide is oxidized to form bromine, which then reacts with naturally occurring organic matter present in the source water. Because brominated DBPs have higher health risks than chlorinated DBPs that form in drinking water, the presence of bromide in source waters increases the risk associated with exposure (through consumption, inhalation and contact) to chlorinated drinking water. Thus, while bromide discharges to surface waters are unlikely to have direct health or ecological impacts, they have significant potential to affect downstream water users through drinking water treatment processes that convert bromide to brominated organics of concern.

In addition to current bromide discharges associated with coal-fired steam electric power plants, altered treatment processes designed to control sulfur dioxide and airborne mercury emissions may change the concentrations of bromide in permitted discharges. Higher bromide loads to surface water systems have the potential to affect downstream drinking water plants, causing higher bromide concentrations, as well as more bromination, of disinfection by-products that pose a risk to consumers of treated drinking water.

Understanding the potential role of bromide discharges on downstream drinking water sources requires a fundamental understanding of the sources of bromide, the fate of bromide in coal-fired power plant wastewaters, the effect of bromide on drinking water treatment, and the potential chemical changes in these natural and engineered systems.

2.0 Background

2.1 Bromine Chemistry

Bromine is element number 35 on the periodic table, in the family with other halogens (e.g., chlorine, fluorine). Bromine is a liquid at standard temperature (0°C), and readily volatilizes at room temperature to a red vapor with an unpleasant odor. The vapor and liquid are irritants and oxidants. Bromine is soluble in water, and hydrolyzes (reacts with water) to form hypobromous acid (HOBr), with disinfection properties similar to hypochlorous acid (HOCl, or bleach). HOBr is more stable in higher temperature waters, accounting for its preferential use as a disinfectant in hot water applications (e.g., hot tubs, cooling towers). The ionic form, bromide, Br⁻, is generally found in a variety of salts (e.g., CaBr₂, NaBr) and is highly soluble in water. Bromide salts are more soluble than chloride salts, thus evaporation-induced precipitation produces solids that are enriched in chloride and residual brines that are enriched in bromide. These differences between bromine and chlorine account for differences in the relative concentration of these ions in minerals (e.g., mined salt, coal) and in production brines (from saline aquifers or oil and gas development). Bromine is easily incorporated into organic compounds, and most bromine is bound to organic carbon in natural systems (Leri and Myneni 2012). Like chlorine, bromine is extensively used in chemical and industrial applications. It is produced for these uses by extraction from seawater or naturally-occurring brines (Hirayama 2008; Vainikka and Hupa 2012), using either the blowing out or steaming out methods, as originally developed by Dow Chemical Company (Stewart 1934; ACS 1997).

2.2 Naturally Occurring Bromide

Natural levels of bromide are low in the environment, except in sources associated with fossil fuels. Bromide is a trace element in the earth's crust, with typical concentrations less than 6 mg/kg (Bowen 1966; Bowen 1979), except in shales, which can have bromide concentrations up to 24 mg/kg. Bromide is a trace element in seawater, with a concentration of 66-68 mg/L, which is about 300 times lower than the typical concentration of chloride. Coastal groundwater and soils, due to the intrusion of seawater, have higher bromide concentrations (up to 2.3 mg/L in groundwater and as high as 850 mg/kg in soil) than inland locations. Davis et al. (Davis, Fabryka-Martin and Wolfsberg 2004) surveyed groundwaters in the U.S. and reported concentrations that varied from 0.0032 to 0.058 mg/L (median value 0.016 mg/L) in *potable* groundwater. Bromide is rarely observed at significant concentrations in fresh surface water systems (e.g., inland rivers and lakes in the U.S.); Bowen reports concentrations of 0.014-0.2 mg/L (Bowen 1966; Bowen 1979)¹. Concentrations of bromide in rain, in the form of bromide ions, are typically below 0.01 mg/L (Flury and Papritz 1993), with slightly higher values in coastal areas due to seaborne aerosols. U.S. drinking water sources were characterized during the 1996 EPA Information Collection Rule (ICR) with bromide values reported as 0.095±0.132 mg/L (USEPA 2000). Significant regional variation was observed, with the highest values in Texas and Florida and lower values inland. Ground waters were associated with higher bromide concentrations, while surface waters were associated with lower values.

¹ EPA 821-R-13-003 April 2013 indicates a range of naturally occurring bromide from "trace to 0.5mg/L in freshwater to 65 mg/L in seawater." The low value is significantly above naturally occurring ranges for freshwaters and the high value is significantly lower than values reported in many naturally-occurring brines.

Bromide is naturally present in fossil fuels, most notably in coal. Coals vary in the concentration of bromide present (USGS 2006), and coal-associated wastewaters are also highly variable. Acidic mine drainage from former coal extraction activities is quite low in bromide, reported as 0.108 ± 0.137 mg/L in Pennsylvania (Cravotta 2008). Currently operating mines (data also for PA) indicate a range of bromide levels in mine pools (25 ± 24 mg/L) (Schwartz 2010a; Schwartz 2010b). Coal bed methane operations also generate a wastewater where chemistry is determined by the coal characteristics. In the western United States, coal bed methane wastewaters are reported at 0.41 ± 1.50 mg/L bromide (Rice, Ellis and Bullock 2000; Rice 2003; Dahm, Guerra, Xu and Drewes 2011). Coal-fired power plant effluent bromide concentrations are also variable [e.g. (USEPA 2009; Frank 2011)]. Additional details related to effluent bromide concentrations for power plant-associated wastewaters are provided in section 3.3 below.

Bromide is also present in organic-rich shale, and as a result, it is present in produced water associated with extraction of oil and gas from shale formations. The presence of bromide in oil and gas brines has been exploited in the past for commercial development (Collins 1970; Kogel, Trivedi, Barker and Krukowski 2006). Initial production of commercial bromide (and iodide) in the U.S. was pioneered by the Dow Chemical Company using oil field brines (Stewart 1934; ACS 1997). Concentrations of bromide in oil and gas produced waters shows significant variation. In Pennsylvania, for example, quite high levels are reported: conventional gas produced waters contain bromide at 1287 ± 425 mg/L (Dresel and Rose 2010), while Marcellus shale produced water contains 1179 ± 558 mg/L (Hayes 2009). Oil produced waters contain bromide as well; reported as 537.2 ± 249.8 mg/L for Pennsylvania sites (Dresel and Rose 2010).

Figure 1 presents concentrations of bromide found in natural sources, including background waters, produced waters from oil and gas development, and wastewaters associated with coal mining and utilization. Note that the scale is log based, with natural waters several orders of magnitude lower in bromide than oil and gas associated wastewaters. The range of coal mine discharges (active and abandoned) of bromide is very similar to the range seen in natural waters. Coal-fired power plants contain higher levels of bromide than background waters, but lower levels than those in oil and gas produced waters.

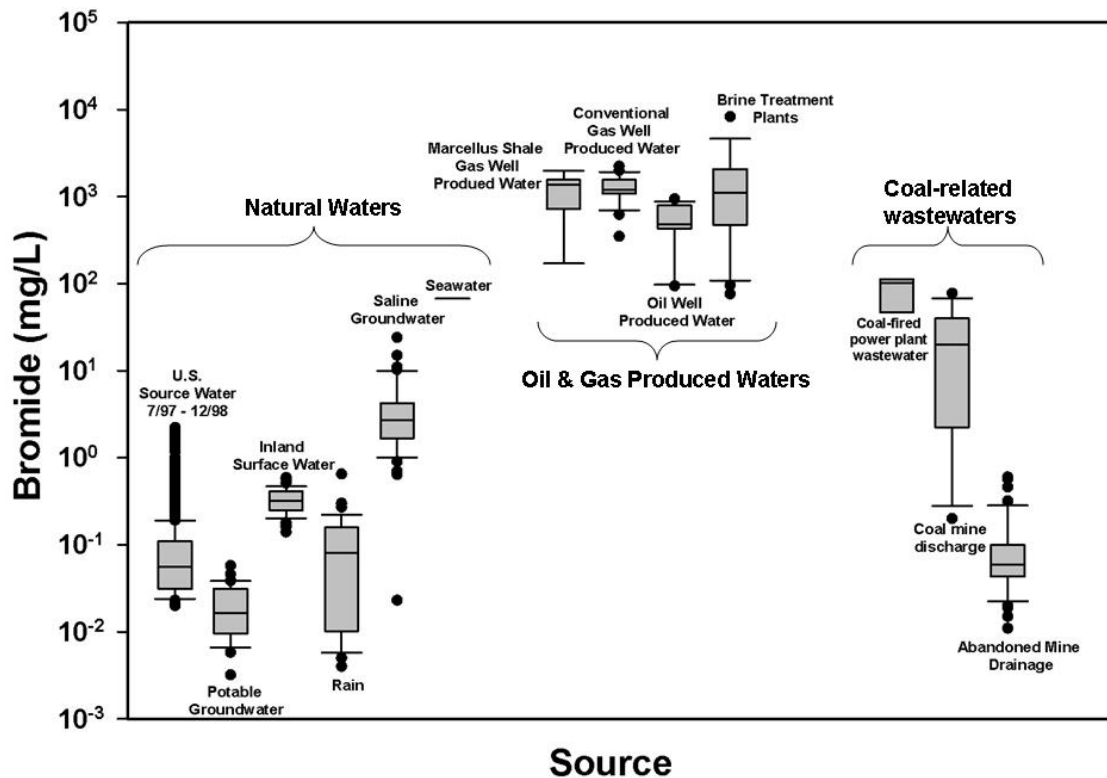


Figure 1. Bromide concentrations (mg/L on log scale) in natural waters, oil and gas produced waters, and coal-related wastewaters. All oil and gas produced waters and coal-related wastewater data from Southwestern Pennsylvania (EPRI 2007; Cravotta 2008; Hayes 2009; Dresel and Rose 2010; Schwartz 2010a; Schwartz 2010b; Frank 2011; USEPA 2012) Natural water data from US sources (Harriss and Williams 1969; Hem 1985; Fuge 1988; USEPA 2000; Davis, Fabryka-Martin et al. 2004; Root, Jones, Schwartz and Gibbons 2004; Stanley 2009; Stanley, Churchill, Mobley and Coffman 2010). Figure is from (Wilson, Wang and VanBriesen 2013).

2.3 Anthropogenic Sources of Bromide

Historical anthropogenic sources of bromide include potassium mining, emissions from an anti-knock additive in leaded gasoline (1,2, dibromoethane, also called ethylene dibromide (EDB)), and pesticides used in agriculture (e.g., methyl bromide, 1,2, dibromo-3-chloro propane) (Norberg-Bohm, Yanowitz and Prince 1988; Flury and Papritz 1993). EDB was implicated in bromide loading from urban runoff, but its use was phased out with the removal of lead in gasoline (Sollars, Peter and Perry 1982). The pesticide, methyl bromide, is an ozone-depleting chemical, and its use was phased out under the Montreal Protocol (Taylor 1994). Trace bromide amounts in fertilizers and some deicing agents can contribute bromide to the environment as well. Road salt is generally low in bromide (Corsi, Graczyk, Geis, Booth and Richards 2010); and its bromide:chloride ratio is significantly below that in seawater. Bromide is currently used in flame retardants (de Wit 2002), drilling fluids as stabilizers for deep wells (USGS 2011), pesticides (Wegman, Hamaker and Deheer 1983), dyes, and pharmaceuticals. Bromide can also

be used as a non-reactive tracer in environmental studies [see for example: (Constantz, Cox and Su 2003; Watzlaf, Schroeder, Kleinmann, Kaires and Nairn 2004)].

2.4 Environmental and Human Health Concerns Associated with Bromide in the Environment

Bromide has been used medicinally for more than 100 years, and its low human toxicity is well established (see review by (Vanleeuwen and Sangster 1987)). Chronic toxicity effects on the endocrine and reproductive systems in animals have been observed at high doses, while acute toxicity is very rare in humans. Several Acceptable Daily Intake (ADI) values have been suggested, including 0.1 mg/kg (Vanleeuwen, Dentonkelaar and Vanlogten 1983) and 1.0 mg/kg (WHO 2009). The World Health Organization recommends less than 6 mg/L for adults and 2 mg/L for children in drinking water; values unlikely to be encountered in treated freshwaters used for drinking in developed countries. Bromide is found naturally in human food and animal feedstocks; it can also be found at higher levels in foods treated with the pesticide, methyl bromide (Winteringham, Harrison, Bridges and Bridges 1955). Ecotoxicity of bromide is also low with impaired growth of evaluated organisms found only at high bromide concentrations (>2 g Br/L for microorganisms and >2.5-7.8 g/L for fish) (Flury and Papritz 1993). A critical acceptable maximum concentration for water based on the ecotoxicology effects of 1.0 g Br/L has been proposed (Canton, Wester and Mathijssen-Spiekman 1983).

The ecotoxicity of brominated organic compounds and their potential impacts on human health are much more significant. For example, brominated flame retardants have been widely studied for ecotoxicity (de Wit 2002; Wollenberger, Dinan and Breitholtz 2005; Debenest, Gagne, Petit, Andre, Kohli and Blaise 2010) and human health impacts (Helleday, Tuominen, Bergman and Jenssen 1999; Darnerud, Eriksen, Johannesson, Larsen and Viluksela 2001; Birnbaum and Staskal 2004). Chlorination of wastewater creates chlorinated and brominated organic compounds that are of concern when released into the environment (Chen, Nam, Westerhoff, Krasner and Amy 2009; Krasner, Westerhoff, Chen, Rittmann, Nam and Amy 2009). Human exposure to brominated organics can occur through treated drinking water when source waters contain elevated bromide (Krasner, McGuire, Jacangelo, Patania, Reagan and Aieta 1989; Symons, Krasner, Simms and Scilimenti 1993). When water containing bromide is disinfected, the bromide is oxidized to form bromine, which then reacts with organic matter to form brominated organics, commonly called disinfection by-products (DBPs) (Singer 1994; Singer 2004). Negative human health outcomes, including cancer and reproductive and endocrine system problems are well documented for chlorinated and brominated compounds, including the halogenated organics that form in drinking water treatment (Reif, Hatch, Bracken, Holmes, Schwetz and Singer 1996; Darnerud, Eriksen et al. 2001; Kogevinas and Villanueva 2011). More information on the role of bromide in disinfection by-product formation in drinking water is presented in section 4 below.

2.5 Role of fossil fuel activities in recent changes in bromide concentrations in surface waters

It is very difficult to evaluate changes in bromide concentrations in the surface waters of the United States. Bromide is rarely monitored in routine water quality testing. One source of historical data is the 1996 EPA Information Collection Rule, which required large drinking water utilities in the United States to measure source water characteristics and finished water disinfection by-products over a period of a year. Data from this source are shown in Figure 1 at

the far left. As noted above, these data suggest source water levels of 0.095 ± 0.132 mg/L for 1995-1996 in the U.S. (USEPA 2000); however, the data are not normally distributed, as evidenced by the significant outliers in the distribution shown. Several researchers have investigated the distribution of bromide in source waters, and have found that ground waters tend to have higher bromide levels than surface waters. Francis et al. (Francis, Vanbriesen and Small 2010) identified two groups of waters within the ICR data: low organic carbon/higher bromide ground waters, and high organic carbon/low bromide surface waters. Thus, we expect inland surface waters to be in the lower range of the ICR data, with values below 0.1 mg/L generally.

Recently, some inland surface water treatment plants have reported increased difficulty meeting regulatory limits on disinfection by-products (see detailed discussion of these products below), and have implicated increasing bromide concentrations in source waters as the cause (Handke 2009; Fiske, Oppenheimer, Moore and Everett 2011; States, Cyprych, Stoner, Wydra, Kuchta, Monnell and Casson 2013; Wilson, Wang et al. 2013). Bromide data from these studies could be compared with data from the 1996 ICR to evaluate the relative increase of bromide concentrations (and, separately, bromide loads) within these specific basins. States et al. (2013) sampled background locations, upstream of any anthropogenic inputs (from below detection to $52 \mu\text{g/L}$), and compared these results with values at the drinking water intake ($25\text{-}299 \mu\text{g/L}$ from 2010-2011). They also sampled upstream and downstream of all putative bromide sources, including coal-fired power plants, industrial sites, and brine treatment plants. The bulk of the bromide load to the Allegheny River came from the discharge of oil and gas wastewater at brine treatment plants after utilizing treatment processes that do not remove bromide. However, they also observed increases (up to ninefold) in concentrations of bromide downstream of two coal-fired power plants, “suggesting periodic releases of bromide from these facilities.” States et al. (2013) suggest these bromide releases may be from seasonal use of brominated antifouling compounds in the cooling towers; however, they did not have any information on the use of FGD scrubbers at these facilities. Wilson et al. (2013) did not identify specific sources associated with increased bromide concentrations; however, several power plants on the Monongahela did add FGD scrubbers for sulfur dioxide control within the past decade. Ongoing studies by the West Virginia Water Research Institute in the Allegheny, Monongahela and Ohio rivers includes bromide with a suite of water quality parameters (detection limit 0.13 mg/L). Data are available online; however, no specific links to sources have been assessed (Ziemkiewicz 2013).

Thus, while it is difficult to attribute increasing bromide concentrations to specific activities, these studies do highlight the sensitivity of surface waters used as drinking water sources to even small increases in bromide loads, especially during low flow conditions when dilution is at a minimum. The impact of these small bromide increases on drinking water treatment will be discussed in sections 4 and 5 below.

3.0 Bromide and Coal-Fired Power Plants

Halogens (Cl, Br, I) are trace elements in coal, as mentioned above. Halogen-based disinfectants can also be found in various cleaning agents and anti-foulants used at power plants. Further, bromide addition, or the use of brominated sorbents, is a well-known application for mercury control in plants with flue-gas desulfurization units. The fate of these halogens in coal-fired power plants depends significantly on process controls, most notably pollution control systems designed to remove sulfur dioxide from flue gas emissions.

3.1 Bromide in Coal

As noted above, bromide is present in coal at trace levels (<0.001 %). Bromide is likely associated with the organic fraction of the coal; however, association with clay minerals and iron oxides has also been reported (Swaine 1990). Coals vary in the concentration of bromide present (USGS 2006), with bituminous coals exceeding subbituminous and lignite. Halogen content is generally controlled by a source's surrounding geochemistry, and thus, deeper mined coals generally contain more halogen salts (Bragg, Finkelman and Tewalt 1991). Details of bromide concentrations for U.S. coals are available in the U.S. Geological Survey Coal Quality (COALQUAL) Database (see <http://energy.er.usgs.gov/products/databases/CoalQual/>). For example, West Virginia coals generally contain 20-40 ppm bromide ($\mu=23.88$, $\sigma=11.47$) with low bromide in Pittsburgh and Redstone coal and highest bromide in Sewell Coal (>50 ppm). The USGS also maintains a World Coal Quality Inventory (see <http://energy.usgs.gov/Coal.aspx>). While many analyses have been generated from these databases and trace metals are routinely measured in coal samples, halogen data are less available [see for example:(Tewalt, Willett and Finkelman 2005; Hatch, Bullock and Finkelman 2006)]. Studies specifically focused on mercury removal (see below) have included careful analysis of bromide and chloride concentrations in coal, as this ratio (Br/Cl) affects mercury removal efficiency. An analysis by Kolker et al. (Kolker, Quick, Senior and Belkin 2012) indicates that most coal-bromide concentrations are below 50ppm, while chloride concentrations are typically below 2000 ppm; an average Br/Cl ratio of 0.02 is reported.

3.2 Coal Combustion and Halogens

Chloride (Cl^-) and bromide (Br^-) ions present in the coal or added prior to combustion are reduced to chlorine ($\text{Cl}_{2(g)}$) and bromine ($\text{Br}_{2(g)}$) through reaction with oxygen at high temperatures during the combustion process. This converts the very soluble ions to gases, thus affecting their fate in the system. Chlorine that is formed in this process can be reduced back to chloride through a reaction with SO_2 , a reaction that is largely controlled by the concentration of SO_2 . Bromine is less susceptible to this reaction in the furnace; however, some bromine can be consumed in a similar reaction with SO_2 that can take place at low temperature in wet flue gas desulfurization (FGD) systems.

Bromine and chlorine are strong oxidants that react with other reduced elements present in the coal, most notably mercury (Hg^0). Bromine and chlorine can oxidize mercury to Hg^{2+} , while being reduced themselves back to ionic form (Cl^- and Br^-). Again, this reaction alters the fate of the Cl and Br. The ionic forms are highly soluble, while the gas phase forms otherwise exit in the flue gases. Thus, the chemistry of oxidation and reduction reactions that take place in the

furnace and in various pollution control units will control the mode of release of chloride and bromide originally present in the coal.

3.3. Fate of Bromide from Coal in Power Plant Residuals

Coal combustion produces multiple residual streams, including: bottom ash, fly ash, gypsum, and flue gases. In general, after combustion, 99% of the halogens originally in ionic form in the coal are found as gaseous forms (chlorine, bromine) in flue gas (Klein, Andren, Carter, Emery, Feldman, Fulkerson, Lyon, Ogle, Talmi, VanHook and Bolton 1975; Germani and Zoller 1988). Bottom ash and associated wastewaters from its wet handling do not contain significant halogen residuals. However, the installation of pollution control units for flue gas alters the chemistry of halogens and their ultimate fate in the system.

Flue gas desulfurization (FGD) systems are designed to convert gaseous SO_2 to the soluble acid, H_2SO_4 . Although the chemistry is more complex, and affected by the presence of metals (including Hg), the process has a similar effect on halogens, converting gaseous Cl_2 and Br_2 to their soluble ionic forms (Cl^- and Br^-). The result of this shift from gas to soluble phase is the capture of chlorine and bromine as chloride and bromide in the FGD wastewater rather than the release of the gases in the stack. A number of researchers have reported that wet and dry flue gas desulfurization (FGD) systems remove halogens in coal from the stack gas, and wet systems transfer them to FGD wastewaters [e.g.(Clare and Sloss 1992; Sloss 1992; Srivastava, Hutson, Martin, Princiotta and Staudt 2006)]. Thus, the addition of wet FGD will increase discharges of bromide in soluble form (Br^-) from power plants to the environment, unless FGD wastewater treatment incorporates bromide removal.

Wastewater characterization at coal-fired steam electric utilities has been undertaken by a variety of industry and regulatory groups. The Electric Power Research Institute (EPRI) released a characterization of residuals in 1987 that included FGD sludge. Chloride and fluoride were measured, but bromide was not (EPRI 1987). EPRI released guidance for wastewater characterization in 2007 that identified 10 sampling locations, including FGD blowdown water, but sampling for bromide was not included (EPRI 2007). Although the preliminary results for FGD wastewater characterization (EPRI 2006) did not include bromide, the recommendations made for future research suggested that bromide should be included. Characterization for metals and other anions is reported by a number of sources, but bromide data are scarce.

Wilson et al. (Wilson, Wang et al. 2013), citing data (EPRI 2007; Frank 2011) for Pennsylvania, report values in effluent streams (type not identified) as $89 \pm 37\text{mg/L}$, as shown in Figure 1 above. At a national level, EPRI conducted a number of studies for different locations associated with evaluation of co-management of low volume wastes with high volume coal combustion by-products. The data for this are provided in Table 1 below, with bromide concentrations ranging from below detection limits ($<0.1\text{ mg/L}$) to 118 mg/L , with higher values always associated with FGD wastewaters. EPA (USEPA 2009) evaluated waste streams from power plants and reported concentration ranges of $43\text{-}96\text{ mg/L}$ for flue-gas desulfurization units, and $180\text{-}260\text{ mg/L}$ for chemical precipitation systems.

The data in Table 1 suggest that FGD wastewaters contain higher bromide levels than most other wastewaters reported from these sites. Further, FGD wastewaters are reported to have *higher* bromide to chloride ratios than other power plant wastewaters and higher ratios than naturally occurring groundwaters (EPRI 2007). The results indicate “the FGD system adds both chloride

and bromide to the water, and the proportion of bromide to chloride added in the FGD system is greater than that added to the bottom ash and low-volume waste streams.”(EPRI 2007)

Specific plant studies have looked at the fate of trace elements in coal-fired power plants with different air quality control devices (Meij 1989; Meij 1991; Meij 1994). Results confirm that bromine is present in the vapor phase in the flue gas exiting the furnace (not in the bottom ash), prior to air quality control systems. For example, Zevenhoven and Kilpinen (Zevenhoven and Kilpinen 2002) report 95% removal of bromide in FGD, with most of the halogen products in the FGD wastewater.

While not a focus of the analysis in the current regulatory rule-making, bromide concentrations measured in the FGD wastewater screening study (EPRI 2006) were used in load calculations (Finseth 2009). Bromide was reported as 67,300µg/L (67.3 mg/L) in FGD wastewater, and this was used to calculate a small model plant load value of 51,700 lbs/year and a large model plant load value of 177,000 lbs/year. No settling pond data were evaluated. An evaluation of a different plant using chemical precipitation treatment reported a concentration of 225 mg/L bromide, leading to loads of 173,000 lbs/year for the small model plant and 592,000 lbs/year for the large model plant. While these data are quite limited, a reasonable conclusion from them is that power plant treatment systems do not remove bromide, but rather will discharge it in wastewater effluent, which may pose a problem for downstream drinking water plants (see Section 4 below).

Table 1. Bromide Concentrations in Wastewater Effluent from Coal-Fired Power Plants in the U.S. (Most data from EPRI’s multi-year study of co-management of low volume wastes with high volume coal combustion by-products²).

Facility Type	Wastewater Type	Bromide Concentration (mg/L)	Reference
Zero discharge waste handling site	Evaporation pond	25, 42, 60	(EPRI 2007)
	Ash Sluice, Ash Pond	3.3, 3.5, 3.4, 3.4	
	Cooling Tower Blowdown	3.5	
	Brine Decant Pit	24, 24	
	Fly Ash Landfill Standing Water	16	
	Economizer and Bottom Ash Tanks	<0.2, <0.2, <0.2, <0.2	
Power Plant Southwestern US	Coal Storage and demineralizer wastes	<0.2, <0.2, <20, <2.0	(EPRI 2002)
	Economizer and bottom ash sluice	<4, <6	
Zero discharge waste handling site	FGD slurry	<1	(EPRI 2005)
	Demineralization regeneration wastewater	<40, <4	
	Boiler blow down	<0.2	
	Ash pond waters	<4, <2, <4	
	Impoundment water	0.19, 0.14, 0.17, 0.14	

² This study was not focused specifically on all liquid wastewater streams from power plants, and thus, most sites did not analyze cooling waters or cooling tower blowdown. Many sites did not have FGD systems or treat and manage FGD waste streams.

	Bottom Ash Settling Tank	0.75, <1.0	
Power Plant Midwestern US	FGD Decantate	78, 69, 74	(EPRI 2000)
Power Plant South Central US (lignite)	Chemical waste treatment basin	<1.0, <0.1	(EPRI 2007)
	Solid Waste Disposal Area Runoff Pond and moisturizing water	90, 89, 108, 31 96, 101, 77, 87 87	
	Emergency Pond	82, 78, 80, 65, 65, 49	
	Bottom Ash Sluice and pond	2.4, 1.9, 1.8, 2.4	
	FGD sludge	118	
	Collection and Holding Ponds	21, 22, 19	
	Ponds 1-10	33, 35, 18, 26, 17, 29, 36, 16, 33	
Power Plant Northern Texas	Fly Ash Pond	114	(EPRI 2004)
	FGD pond	96	
	Mill rejects and bottom ash sluice	0.057, <0.050, 0.087, 0.13	
	Basin water: pond and outfall	0.116, 0.090, 0.110, 0.099, 0.118	
	Leachate	<8.0, <0.080, <0.080, <0.095, <0.080, <10, <0.10, <0.50, 0.112, <0.10	
Metal cleaning basin	0.10, 0.08, 0.10		
Power Plant in north central PA	Coal Pile Runoff	0.08, 1.25, 0.19	(EPRI 2003)
	Waste basin	0.12, 0.19, 0.12	
	Ash landfill	0.38, 0.2	
Power Plant (subbituminous coal)	Landfill runoff	0.09, <0.05, 0.09, 0.09, <0.05, 0.2, 0.38	(EPRI 1998)
	Fly ash Sluice and Pond Water	<0.2, <0.2, <0.2, <0.2	
Power Plant (PRB subbituminous coal)	FGD liquor during bromide addition testing	35, 27 (baseline) 27, 41, 55, 55, 72, 102, 109, 145	(Benson, Holmes, McCollor, Mackenzie, Crocker, Kong, Galbreath, Dombrowski and Richardson 2007)
	FGD solids during bromide addition testing	13, <10 (baseline) 8, <10, 0, 0, <10, <10, 19, 13	
Power Plant SW PA	Blowdown Effluent	Average: 2.67 Maximum: 3.57	Permit Data Review
	Desilting Basin	Average: 2.763 Maximum: 3.040	
Power Plant SW PA	Blowdown Effluent	<2.5	
Power Plant SW PA	Blowdown Effluent	Average: 1.223 Maximum: 1.720	
Power Plant SW PA (bromide addition trial)	FGD Supernatant Baseline	109,113,113,114,96.4,125	(Frank 2011)
	FGD Supernatant Test Side	243,395,519,575,450,461	
	Outfalls	135,114,105,107,121,228,133, 114,105,107,123,219	
Power Plant	FGD Purge Bromide	28.1±14.73 (68 data points collected March 3, 2009 to July 30, 2009) raw data as follows: 16 17, 16,8.5,8.1,9.5,10,8.6,7.5, 8.8,15,18,18,14,16,19,14,13, 17,20,21,23,21,20,23,26,32, 40,59,67,52,40,26,23,26,24,	(USEPA 2009)

		23,2,18,17,10.0,26,31,31,40,47,43,36,22,31,43,41,41,38,37,44,45,59,34,40,43,27,26,27,30,30,49,56,55	
Power Plant in Newnan, GA	FGD Wastewater	7.42	(ERG 2007)

3.4 Bromide and Mercury Control

The fate of mercury in coal-fired power plants is beyond the scope of this report. The reviewer is referred to several excellent sources for review of this issue [e.g. (Meij, Vredenburg and teWinkel 2002; Wilcox, Rupp, Ying, Lim, Negreira, Kirchofer, Feng and Lee 2012)]. This section will deal only with the role of halogens, and specifically bromide, in mercury removal processes.

High bromide coals have been known to improve mercury control at power plants that have flue gas desulfurization units for many years [see excellent overview by (Kolker, Quick et al. 2012)]. Average removal efficiencies of subbituminous and lignite coal are always lower than that of bituminous, likely due to halogen content. Elemental Hg is a nonreactive, insoluble gas that is generally released in the flue gas after coal combustion. Halogens, when present in their gaseous elemental forms, are highly reactive with Hg^0 , oxidizing it to form the ionic Hg^{2+} , creating mercury-halogen salts ($HgBr_2$, $HgCl_2$), which are soluble, and therefore more easily captured in removal technologies. Chloride, which is abundant in coal, is an adequate oxidant when converted at high temperatures to chlorine; however, as noted above, additional reactions with sulfate can deplete chlorine levels. Bromine is a much better oxidant than chlorine, and it does not react with sulfate readily in the furnace, and thus, it is more available for oxidation of mercury. However, bromide is present at much lower levels in most coals; the bromide to chloride ratio of 0.02 means bromide is present at 2% of the chloride levels, on average. The issue is further complicated by the rate of the reactions, which are temperature dependent, with low halogen concentrations requiring higher temperatures for similar removals (Wilcox, Rupp et al. 2012). As noted by Kolker et al. (Kolker, Quick et al. 2012), “the actual proportion of Hg that conventional Air Pollution Control Devices (APCDs) capture depends on the type of coal that is burned, the type and set of APCDs, the halogen content of the coal, and the flue gas temperature.”

The addition of chloride has been demonstrated to improve mercury removal (Zhuang, Thompson, Zygarlicke and Pavlish 2007); however, bromide reacts faster and is effective at lower concentrations (Liu, Yan, Liu, Qu, Wang, Chang and Miller 2007; Cao, Zhengyang, Zhu, Wang, Huang, Chiu, Parker, Chu and Pan 2008). High concentrations of salts increase corrosion in the FGD system, and thus, bromide is preferred since it can be added at lower concentrations. Finally, $HgBr_2$ is more stable and less likely to convert back to Hg^0 . Thus, concentrations of halogens and sulfate are important for control of re-emission of mercury during FGD (Omine, Romero, Kikkawa, Wu and Eswaran 2012).

Bromine addition can take place at several points in the power plant: in the furnace (as bromine or bromide/chlorine) and in the flue gas prior to the FGD. Several patents exist for different bromine-addition technologies [For example: US 6,808,692 B2, Oct 26, 2004; US 6,878,358 B2, April 12, 2005]. Power plant pilot testing of bromide additions have been very successful for enhanced mercury removal [see for example: (Vosteen, Kanefke and Koser 2006; Benson,

Holmes et al. 2007; Berry, Dombrowski, Richardson, Chang, Borders and Vosteen 2007; Dombrowski, McDowell, Berry, Sibley, Chang and Vosteen 2008; GAO 2009)]. Research in this area has been similarly promising [see for example: [(Niksa and Fujiwara 2005; Eswaran and Stenger 2008)]. An alternative to direct bromide addition is the use of activated carbons (untreated, chlorinated or brominated) that oxidize and then sorb Hg onto the particle surface where downstream particle removal technologies capture these materials [See For example: US 6,953,494 B2, Oct 11, 2005]. Brominated activated carbons work better for this application (Chang, Dombrowski and Senior 2008; Krishnakumar, Naik, Niksa and Fujiwara 2013). However, use of activated carbon-based materials, which are captured in the fly ash rather than released in wastewaters, can reduce the resale value of the resultant fly ash (GAO 2009). The use of direct bromide addition, thus, is more likely based on its cost, its minimal effect on operations, and its non-negative impact on residuals sales (Fielding 2012).

When EPA promulgated the Clean Air Mercury Rule (CAMR) in 2006, which would have required mercury reductions of 70% by 2018, the agency stated that it expected significantly expanded use of bromide in coal plants (USEPA 2005; Mcilvaine 2013). The Mercury and Air Toxics Standard, which replaced CAMR, and requires mercury reductions of up to 90% by 2017, is also likely to promote bromide use in coal plants (USEPA 2012). Fielding (Fielding 2012) summarized the potential bromide demand associated with meeting targets for mercury control in coal-fired power plants by considering the volume of coal used, the average bromide in that coal, and the average bromide concentration needed for mercury removal; he reports 5,700-69,000 short tons of bromide would be needed annually. As Fielding notes, supply of this amount of bromide would not be a problem, as U.S. bromide capacity (via extraction from brines in the Smackover formation in Arkansas) is abundant. **However, discharge of this additional bromide to surface waters could lead to significant challenge for downstream drinking water plants.**

As detailed above (see Table 1), available data suggest FGD wastewaters contain significant bromide, while other wastewaters from coal-fired power plants are low in bromide. Based on existing knowledge of bromide fate in power plants with FGD systems, it seems very likely that any bromide added for mercury control will also be captured predominately in the FGD wastewater. For plants that do not operate FGD systems, added bromide is likely to end up where naturally-occurring bromide would (predominately in flue gas as bromine). Few full-scale tests of bromide additions have evaluated the fate of the added bromide. For example, Berry et al. (Berry, Dombrowski et al. 2007) report on a full-scale calcium bromide injection test at a power plant in Alabama, demonstrating significant mercury control. Only the source coal was measured for bromide; there was no evaluation of the concentration of bromide in any wastewater produced at the plant. Similarly, EPRI reports on a number of halogen addition tests, showing variable mercury removal, but does not discuss bromide fate (Vosteen, Chang, Rini, Berry and Dombrowski 2008). The U.S. DOE also conducted a series of studies, again focusing on mercury removal, where some analyses for bromide were conducted (Benson, Holmes et al. 2007). Lignite and PRB coal (both containing <10 µg/g bromide), were amended with various compounds, including bromide at different concentrations. Bromide was measured in fly ash (highest concentration reported at 6.98 µg/g) and the FGD liquor (highest concentration of 145 mg/L) and FGD solids (non-detectable). FGD liquor bromide concentrations increased with increasing bromide addition. However, the mass balance on bromide was missing 90% of the added bromide, calling into question the analytical methods in this study. A similar full-scale

addition test case included measurement of bromide before the FGD, providing insight into the fate of bromide in the absence of a FGD system (Dombrowski et al., 2008). The flue gas bromine concentration increased with increasing calcium bromide injection rate, as expected; without FGD, bromide is released as bromine in flue gas. However, the sum of bromine in the flue gas and the fly ash were below the theoretical levels predicted by mass balance. Thus, additional analysis to evaluate the fate of the injected bromide in the absence of FGD units is warranted. In 2011, a well-controlled performance trial of calcium bromide addition to coal at a plant with a wet FGD scrubber system was conducted in southwestern Pennsylvania (Frank 2011). To improve evaluation of the mass balance on bromide, sodium bromide addition in the cooling towers was discontinued ten days prior to the bromide addition evaluation. Bromide was measured in the FGD supernatant tanks prior to wastewater treatment. Baseline bromide in the effluent (prior to the trial) was 114 mg/L, while the maximum detected during the trial was 575mg/L. Outfall concentration maximums were 228 mg/L and 219 mg/L, below the maximum values reported for these outfalls in prior permit renewals. Bromide was detected at slightly increased levels in the fly ash, with an average concentration of 7.1 mg/kg. While this was a small trial at only a single plant, the data suggest approximately a four-fold increase in bromide concentration in FGD wastewater during calcium bromide addition for mercury control (from 112 ± 9 mg/L to 441 ± 115 mg/L)(Frank 2011).

3.5 Bromide use as a biocide in power plant cooling towers

Cooling towers create a concentrated wastewater (called blowdown) that typically reflects the original chemicals in the makeup water plus chemicals added for corrosion control or biological fouling control. While not the focus of the current analysis, the use of bromide in power plant cooling systems is discussed here to explain other, related sources of bromide in wastewater effluent. Bromine is used as a biocide, either alone or in conjunction with chlorine. Bromine (as HOBr) is generally more reactive than chlorine, and thus has stronger biocidal activity. Further, bromine appears to increase the rate of oxidation, leading to lower concentrations of oxidants in the effluent at discharge (Pinkey, Friday and Hochberg 1992). This is beneficial because discharging reactive disinfectant is detrimental to ecological health. Bromine can also be used at various stages in cooling water disinfection. For example, EPRI (EPRI 2007) report pre-treatment of lake water with sodium bromide and chlorine bleach to control iron and manganese and to manage biological growth prior to use for cooling water. The formation of disinfection by-products in cooling water has also been evaluated (EPRI 2004). Table 1 includes some data from cooling tower blowdown water, showing generally low bromide concentrations, on the order of a few milligrams/L.

4.0 Source Water Bromide and Drinking Water Disinfection By-Products

As noted above, bromide released into the environment can raise the concentration of bromide in surface waters. While bromide itself is not a risk to humans or ecosystems at the concentrations likely to be observed in the downstream environment of power plant discharges, elevated bromide source waters can alter the chemistry in drinking water produced from these sources. This section provides an overview of the formation of disinfection by-products and the role of bromide in the risk associated with these drinking water contaminants.

4.1. Drinking Water Treatment Disinfection and Disinfection By-Product Formation

Drinking water treatment involves a series of steps to remove contaminants of concern from the source water to make it safe for human consumption. Coagulation, settling and filtration are designed to chemically alter some dissolved contaminants (reducing their solubility and forming precipitates) and then to remove naturally-occurring or chemically-produced particulates of concern. Particles that are too small to be removed through the physical processes of settling and filtration and that do not react in the chemical process of coagulation are subjected to further chemical treatment to render them harmless. This is generally done through chemical oxidation (using a disinfectant) that inactivates living organisms (e.g., bacteria and viruses) that make it through the prior treatment steps.

Disinfection of drinking water is widely recognized as one of the major engineering accomplishments of the 20th century, reducing the rates of waterborne illness everywhere it is practiced. Disinfection techniques include ozonation, ultraviolet radiation (UV), and chlorine-based chemical processes. Chlorine is used extensively, as it not only provides a primary disinfectant to inactivate organisms in the water, but it also persists in water over the multiple days that water will travel in pipes to consumers, providing additional protection in case of microbial regrowth or re-entry into the pipe (called secondary disinfection). Ozone and UV methods do not provide this residual protection and thus are used as primary disinfectants only. In the U.S., the provision of a chemical residual disinfectant all the way to the consumer's drinking water tap is required by law. In addition to their use as a disinfectant, oxidants are also used to control nuisance metals in drinking water (e.g., Fe, Mn). Thus, oxidation steps can occur several times during drinking water treatment. Pre-oxidation, which occurs before coagulation, settling, and filtration, is often used for metals control, as the reaction of the oxidant with the metal makes it less soluble and, thus, metals are removed in the physical settling and filtration processes. Disinfection-based oxidation usually occurs at the end of the treatment process, as microbes attached to particles that have not yet been removed can be resistant to destruction by oxidants. A typical treatment process for drinking water, showing locations where chlorine-based oxidants may be used is shown in Figure 2. The amount and type of disinfectant and/or oxidant added in each stage is specific to the water being treated and the drinking water treatment plant capabilities.

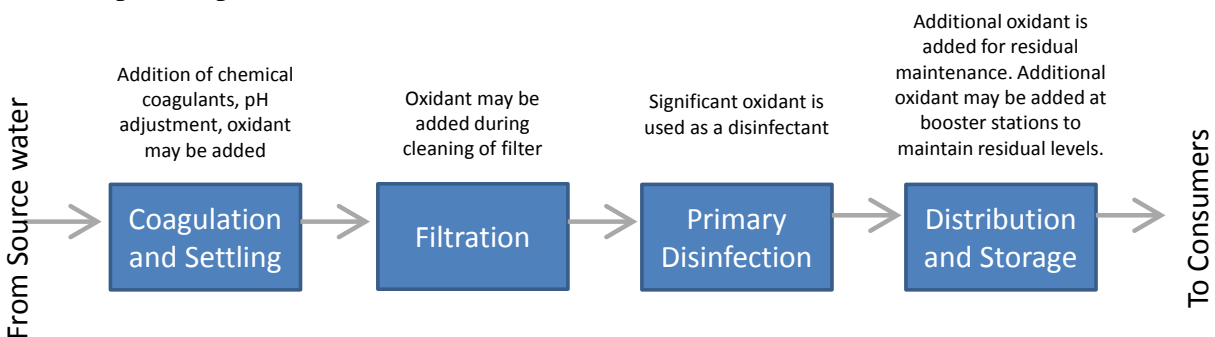
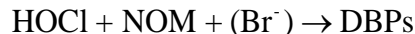


Figure 2. Schematic of Drinking Water Treatment Process with Oxidant/Disinfectant Addition Points Noted.

While drinking water disinfection is a triumph of engineering to protect human health, it does have an unintended consequence. During disinfection, chlorine (typically applied as hypochlorous acid, HOCl) reacts with organics present in the source water (natural organic matter or NOM) to form chlorinated disinfection by-products (DBPs). If bromide is present, the

free chlorine rapidly oxidizes the bromide to hypobromous acid, which then, along with the residual hypochlorous acid, reacts with the organic matter to form brominated and mixed chlorinated-brominated DBPs. The generalized reaction below illustrates the formation of disinfection by-products using chlorine as a disinfectant.



Hundreds of different halogenated organic compounds form during drinking water treatment (Richardson 2003; Richardson, Thruston, Rav-Acha, Groisman, Popilevsky, Juraev, Glezer, McKague, Plewa and Wagner 2003; Singer 2004; Richardson and Ternes 2005), and a very limited subset have been well studied (Krasner, Weinberg, Richardson, Pastor, Chinn, Scilimenti, DOnstad and Thruston 2006). For waters treated with chlorine, haloacetic acids (HAAs) and trihalomethanes (THMs) predominate. There are a total of nine HAA species (HAA_9) containing chlorine and/or bromine and there are a total of four THM species (THM_4) containing chlorine and/or bromine (see Figure 3). The regulation of only five of the HAA species (MCAA, DCAA, TCAA, MBAA, and DBAA) was based on available occurrence data and limitations in analytical method standards for the other four HAA species (DCAA, DBCAA, DCBAA, TBAA) (Singer 2004). Maximum Contaminant Level Goals (MCLGs) are listed in Table 2, along with the Maximum Contaminant Level (MCL) allowable in finished water, which is based on the sum of TTHM and HAA_5 , respectively. The regulation of these compounds as groups was based on the predominance of chlorinated forms over brominated forms in most source waters; only when bromide is high in source waters do brominated forms appear and present risk.

While THM_4 and HAA_5 are currently the most studied DBPs, additional DBPs and groups of DBPs have been evaluated in drinking water. For example, the use of chloramine instead of chlorine produces different DBPs (many of them containing nitrogen; all unregulated at present). The use of ozone produces fewer DBPs, with the exception of bromate, which forms when bromide is present in source water (Von Gunten 2003; Fan 2009); bromate is regulated.

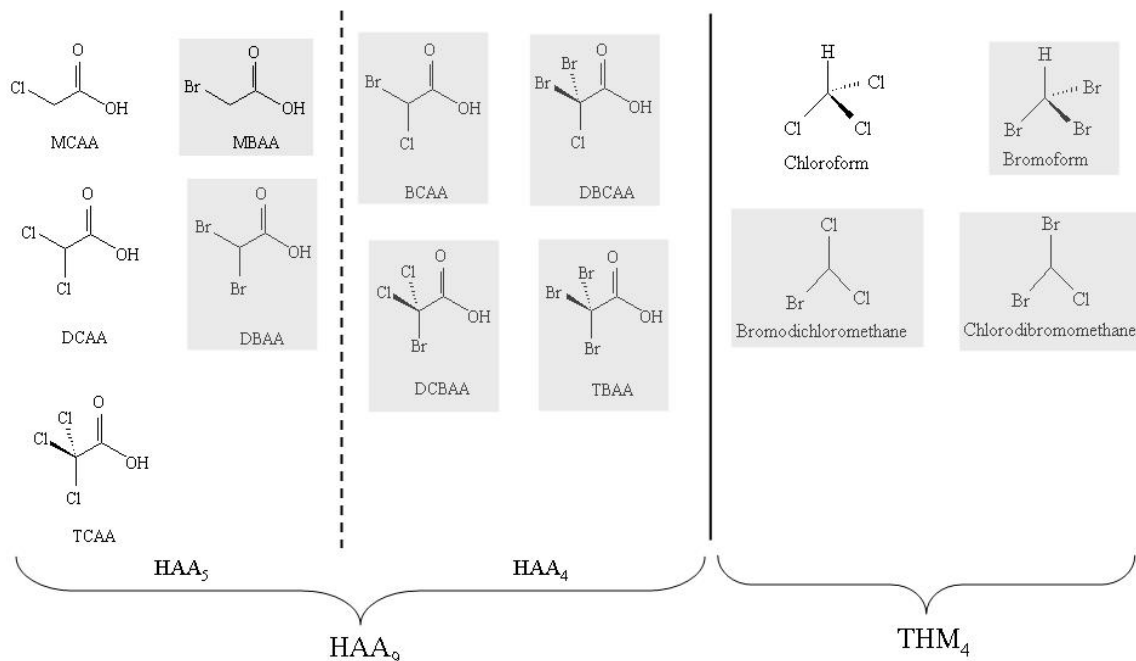


Figure 3. Structures for HAAs and THMs. Shaded DBPs contain bromide and can only be formed when source waters contain bromide

4.2 Drinking Water Disinfection By-Products and Human Health Risk

While disinfection has clearly made drinking water much safer by removing microbial risks, disinfection by-products are not without their own concerns (for a recent overview, see (EWG 2013)). In 1976, the National Cancer Institute identified chloroform as being carcinogenic to rodents (1976). Since it was known to be present in chlorinated drinking water, extensive research followed. Subsequent work challenged the contention that chloroform was carcinogenic in humans through consumption of drinking water, and well-controlled epidemiological studies have proven difficult due to the presence of mixtures of DBPs in drinking water (NIH 2011) and the multiple pathways of exposure (ingestion, inhalation, dermal). Toxicity and carcinogenicity of *individual* DBPs remains difficult to quantify. However, mixtures of DBPs present in drinking water have been well-studied.

Numerous epidemiological studies have established an association between the use of chlorinated drinking water and increased risk of bladder cancer and rectal cancer (see for example: (Cantor, Hoover, Hartge, Mason, Silverman, Altman, Austin, Child, Key, Marrett, Myers, Narayana, Levin, Sullivan, Swanson, Thomas and West 1987; King and Marrett 1996; Cantor, Lynch, Hildesheim, Dosemeci, Lubin, Alavanja and Craun 1998; Boorman, Dellarco, Dunnick, Chapin, Hunter, Hauchman, Gardner, Cox and Sills 1999; NIH 2011)). Other effects from exposure and use of chlorinated water that contains DBPs can include adverse reproductive outcomes (e.g., low birth weight, anemia, developmental anomalies, growth retardation, and urinary tract anomalies) (Boorman, Dellarco et al. 1999; Nieuwenhuijsen, Toledano, Eaton, Fawell and Elliott 2000; Graves, Matanoski and Tardiff 2001; Kumar, Forand, Babcock and Hwang 2013). Additional epidemiological work has focused on the inhalation and dermal exposures to DBPs in drinking water and in chlorinated recreational water (i.e., swimming

pools)(Liviak, Wagner, Mitch, Altonji and Plewa 2010; Basu, Gupta, Singh and Mukhopadhyay 2011; Richardson and Postigo 2012).

As EPA notes in most documents associated with DBP regulation, more than 200 million people in the United States use water that has been treated with a chemical disinfectant for consumption and bathing. Even small health risks present a serious concern, due to this very large exposed population. To reduce the risk to populations using disinfected water, the Stage 1 Disinfectants/Disinfection Byproducts (D/DBP) Rule was established in the U.S. in 1998 to regulate total Trihalomethanes (THMs) at a maximum contaminant level (MCL) of 80 µg/L and a group of five Haloacetic acids (HAAs) at an MCL of 60 µg/L (USEPA 1998). At that time, there was extensive discussion about the regulation of individual DBPs, the additional four HAAs, and other potential DBPs (e.g., NDMA). EPA continues to evaluate DBPs for health concerns, and several nitrosamines are on the Contaminant Candidate List (USEPA 2009). In 2006, the EPA published the Stage 2 D/DBP Rule, which alters the monitoring locations and reporting requirements for THM and HAA to increase public health protection. Basically, the change ensures that all locations in a drinking water distribution system will meet the MCLs, whereas previously, utilities could average high and low locations and still be considered in compliance. Large systems (those serving greater than 100,000 people) were required to be in compliance with Stage 2 of the D/DBP Rule in January 2013. Smaller systems have compliance dates over the next year, with final compliance at all public systems by July 2014.

There are two main issues related to the use of lumped surrogate terms (TTHM and HAA₅) for the protection of consumers from risks associated with disinfection by-products. First, TTHM and HAA₅ represent a small fraction of the total number of DBP chemicals that might form. While they may represent the most common chemicals, it is not clear that their control will also control other unregulated DBPs. Francis et al. used the ICR data to evaluate the suitability of TTHM and HAA₅ as surrogates for other halogenated organics measured during the ICR study (Francis et al. 2010). They found that the relationship between the regulated surrogates (TTHM and HAA₅) and other classes of halogenated organics present in drinking water is fairly strong when source water bromide concentrations are low, suggesting that the control of THM and HAA₅ will also provide protection from risks associated with unregulated DBPs. However, when source water bromide is high (>0.4 mg/L), TTHM and HAA₅ concentrations are not well correlated with other classes of DBPs, suggesting waters containing acceptable levels of TTHM and HAA₅ could contain unacceptably high levels of unregulated DBPs that pose human health risk (Francis, Vanbriesen et al. 2010).

The second concern with the use of TTHM and HAA₅ has to do with their regulation based on total concentration. The regulatory limit is on *total concentration* of these groups of chemicals, again because this grouping is believed to be a good surrogate for risk (USEPA 1992). However, the risk associated with DBPs is well-known to be *species-dependent*, with iodinated and brominated DBPs associated with negative outcomes at lower concentrations than their chlorinated analogs (Richardson, Thruston et al. 2003; Echigo, Itoh, Natsui, Araki and Ando 2004; Plewa, Wagner, Richardson, Thruston, Woo and McKague 2004; Berry, Dombrowski et al. 2007; Richardson, Fasano, Ellington, Crumley, Buettner, Evans, Blount, Silva, Waite, Luther, McKague, Miltner, Wagner and Plewa 2008). Thus, because brominated DBPs have higher health risks than chlorinated DBPs, the presence of bromide in source waters increases the risk

associated with use of chlorinated drinking water (Rook 1974; Richardson, Thruston et al. 2003; Berry, Dombrowski et al. 2007). When bromide is present, it is possible to have a finished drinking water that contains acceptable levels of TTHM and HAA₅, but which presents a greater risk to consumers than water with acceptable levels created solely by chlorinated DBPs.

The assessment of risk is complex and beyond the scope of the present work. Table 2 provides details on the four regulated THM, the five regulated HAA and the four unregulated HAA, as well as other regulated DBPs (chlorite from use of chlorine dioxide and bromate from use of ozone in waters that contain bromide). Toxicity data for the main THM and HAA forms has been developed, but for many unregulated disinfection by-products, little is known regarding toxicity. Using computational toxicity tools, estimates of the toxicity of unstudied chemicals detected in finished drinking water samples that have been disinfected have been developed (Woo, Lai, McLain, Manibusan and Dellarco 2002; USEPA 2008). **While specifics for each chemical remain largely unknown, in general, as noted above, brominated (and iodated) DBPs present higher risks than do chlorinated DBPs. Thus, shifting speciation from predominately chlorinated to predominately brominated forms of DBPs increases risks associated with exposure to chlorinated drinking waters.**

Table 2. Summary of Target Concentrations (MCLGs and MCLs) for Common Disinfection By-products in Water

	Maximum Contaminant Level Goal	Maximum Contaminant Level
Chloroform, CHCl ₃	70 µg/L	Sum of all four on a mass basis must be less than 80 µg/L (0.080mg/L) for an annual running average
Bromodichloromethane, CHCl ₂ Br	0	
Dibromochloromethane, CHClBr ₂	60 µg/L	
Bromoform, CHBr ₃	0	
Monochloroacetic acid (MCAA)	70 µg/L	Sum of HAA ₅ on a mass basis must be less than 60 µg/L (0.060 mg/L) for an annual running average
Dichloroacetic acid (DCAA)	0	
Trichloroacetic acid (TCAA)	20 µg/L	
Monobromoacetic acid (MBAA)	Not set	
Dibromoacetic acid (DBAA)	Not set	
Bromochloroacetic acid (BCAA)	Not set	
Bromodichloroacetic acid (BDCAA)	Not set	No MCL set for these compounds
Dibromochloroacetic acid (DBCAA)	Not set	
Tribromoacetic acid (TBAA)	No set	
Bromate	0	10µg/L (0.010 mg/L)
Chlorite	0.80 mg/L	1 mg/L

4.3 Disinfection By-Product Speciation and Bromine Incorporation

As noted above, while toxicity and carcinogenicity of *individual* DBPs remains difficult to quantify, mixtures of DBPs have been well studied, and brominated DBPs are consistently found

to be more toxic than chlorinated DBPs. Thus, there have been a number of studies focused on identifying the effect of source water bromide on finished water DBP levels and associated risk. A nationwide study by Krasner et al. found that in source waters containing 3 mg/L (3000 µg/L) bromide, the THM distribution shifted to the brominated species (Krasner, McGuire et al. 1989). Similarly, Heller-Grossman found that 85% of the HAAs were brominated in a lake with “high” bromide concentrations (1.9 mg/L; 1900 µg/L). Chlorination of water with elevated bromide concentrations has been observed to cause a shift from chlorinated to the mixed chloro-bromo and brominated haloacetic acids (Cowman and Singer 1996).

Extensive laboratory and field studies have explored the relationship between bromide concentrations in the source water and finished DBP concentrations in drinking water (Luong, Peters and Perry 1982; Hellergrossman, Manka, Limonirelis and Rebhun 1993; Pourmoghaddas, Stevens, Kinman, Dressman, Moore and Ireland 1993; Cowman and Singer 1996; Chang, Lin and Chiang 2001; Duong, Berg, Hoang, Pham, Gallard, Giger and von Gunten 2003; Liang and Singer 2003; Ates, Kitis and Yetis 2007; Cravotta 2008). Bromide field data available in the ICR database have also been evaluated (Obolensky, Singer and Shukairy 2007; Obolensky and Singer 2008; Francis, Vanbriesen et al. 2010). Much of the research conducted in the laboratory or field has identified relationships with high bromide concentrations (≥ 0.4 mg/L (400 µg/L), as classified in a nationwide EPA report on the occurrence of DBPs (Weinberg, Krasner, Richardson and Thruston 2002)). For example, in a laboratory study, a high bromide concentration of 412 µg/L resulted in the formation of 80% brominated HAAs (Cowman and Singer 1996). For water with low to moderate bromide concentrations (20 µg/L to 140 µg/L (Weinberg, Krasner et al. 2002)), the speciation of brominated HAAs and THMs is less clear. Duong et al. studied the formation of THMs after chlorination of groundwater samples containing low to moderate concentrations of bromide (50 – 140 µg/L) and found that greater than 80% of THMs formed were brominated (Duong, Berg et al. 2003). In the same study, source water with 20 – 30 µg/L bromide that was chlorinated resulted in 40% brominated THM formation (Duong, Berg et al. 2003). However, another laboratory study found that source water with a moderate bromide concentration of 100 µg/L resulted in only 10% formation of brominated HAAs (Cowman and Singer 1996). Research by Ates et al. found that waters with lower bromide concentrations (60–110 µg/L) did not see a formation shift of DBPs, and that non-brominated DBPs were being formed at greater concentrations at lower bromide concentrations (Ates, Kitis et al. 2007). In work using the ICR database, Obolensky et al. found that bromide was a significant predictor for all DBP species (Obolensky and Singer 2008), but also concluded that at lower bromide concentrations DBPs other than THMs and HAAs, such as the unregulated adsorbable organic halogens, were being formed, again calling into question the concept of using TTHM and HAA5 as surrogates for drinking water DBP risk.

While disinfection by-products have been widely studied and much is known about their formation and control, we know the least about systems where bromide is high *and* organic carbon is high. As noted above, the 1996 EPA information collection rule (ICR) database (USEPA 2000) and subsequent surveys (Weinberg, Krasner et al. 2002) identified two general classes of waters in the US: those with elevated bromide and low organic carbon (typically groundwaters in coastal states) and those with elevated organic carbon and low bromide (typically inland surface waters) (Francis, Vanbriesen et al. 2010). The significantly problematic case of elevated bromide and high organic carbon was not observed in surveys of US drinking

water in the 1990s and 2000 (Obolensky, Singer et al. 2007; Francis, Vanbriesen et al. 2010). High bromide in conjunction with high organic carbon is widely recognized to be a worst-case scenario for drinking water plants as typical DOC removal technologies cannot reduce DOC to levels that prevent significant DBP formation in the presence of even moderate bromide levels (Babcock and Singer 1979; Liang and Singer 2003; Archer and Singer 2006). **Thus, inland surface waters, which typically have elevated organic carbon (due to natural processes), are most susceptible to problems when bromide concentrations increase.**

Despite the well-known challenges associated with source water bromide, it is rarely considered within a regulatory framework, likely because most bromide is naturally-occurring and confined to systems with known problems. For example, bromide is a well-known concern in water systems dependent on water from deltas, where tidal excursions cause the mixing of seawater and river water. For this reason, the CALFED Drinking Water Quality Program in California has set a target of 50 µg/L (0.05 mg/L) to protect the public from the health effects of brominated disinfection by-products (Holm, Harader and Fernandez 2007). Source waters in areas of California with significant seawater intrusion (either through groundwater or in tidal areas) often exceed this level. For example, bromide levels in water used by CALFED had running annual averages of 42-424 µg/L (0.04-0.4mg/L) from 1990-2006 (Holm, Harader et al. 2007). Since these are natural sources and bromide removal is very difficult, control is managed via dilution with other water sources (median bromide concentrations unaffected by the ocean are 14µg/L (0.014 mg/L) in surface waters in this area, with concentrations below detection frequently). The effect of these elevated bromide concentrations on water produced from these sources has been extensively documented (Holm, Harader et al. 2007; Westerhoff 2008).

4.4 Drinking Water Treatment System DBP Control Options

The cost of reducing DBPs in drinking water has been evaluated by EPA as part of the multi-stage Disinfectants/Disinfectant By-Product (D/DBP) Rulemaking (see for example: (USEPA 1992; USEPA 2005)). There are several common methods to improve DBP control within the drinking water plant. First, drinking water systems can apply enhanced coagulation, settling and filtration systems to improve removal of organic carbon (which reacts to form DBPs)(Edzwald and Tobiason 1999; Volk, Bell, Ibrahim, Verges, Amy and LeChevallier 2000). This DBP-precursor control has been very successful at many drinking water plants, leading to systems that are optimized for organic carbon removal. Because this technical solution has been applied at many plants already in response to State 1 of the D/DBP rule, it is unlikely to have utility in addressing increased bromide concentrations.

A second option that is often selected is to change from free-chlorine-based disinfection to a non-chlorine based disinfectant or to combined chlorine (UV, ozone, chloramine). These other disinfectants also produce disinfection by-products (chlorite from chlorine dioxide, bromate from ozone, and unregulated nitrosamines from chloramine). The role of bromide in formation of DBPs from alternative disinfectants has also been studied (e.g., (Richardson, Thruston, Caughran, Chen, Collette and Floyd 1999)), although, as noted above, less is known about the risks associated with unregulated DBPs. Disinfection switching carries increased costs, as well as a need for additional training of operators. For example, the switch to chloramine requires the addition of phosphate to control lead releases that can be caused by the transition (e.g., see the case study of the transition in Washington D.C. (Edwards and Dudi 2004; Edwards,

Triantafyllidou and Best 2009)). EPA's most recent costs analyses suggest that the switch to chloramine is the most cost-effective method (USEPA 2005). **None of the national cost analyses specifically deal with the issue of increasing bromide, altering the level or speciation of DBPs, or interacting with process controls implemented to reduce TTHM and HAA₅.**

Due to the extensive challenge of bromide for the CALFED system, Chen et al assessed the cost of increasing bromide concentrations associated with projected increases in seawater intrusion and decreases in delta water export (Chen, Haunschild and Lund 2008). Their estimates are based on the 1.5 million acre-foot of water presently used from the Delta (providing water to 23 million Californians), and an increased cost of \$20-60 per acre foot associated with the current bromide levels, leading to \$30-90 million per year. They estimated an increase to \$200-1000 million per year as source water quality declines and water use increases. Further, they consider the residual public health risk associated with unregulated DBPs that may not be removed through treatment. "Bromide is particularly difficult and expensive to remove and its associated brominated DBPs are among the most harmful." (Chen, Haunschild et al. 2008) More recently, the California Urban Water Agencies (CUWA) completed an analysis of the operational and maintenance costs associated with bromide at various levels in the source water under current and potential future regulatory scenarios for DBPs (CUWA 2011). Absent an improvement in source water quality, they anticipate spending \$3-8 billion in capital improvements to meet future plausible³ drinking water standards (including those associated with DBPs) with the lower quality (higher bromide) water; added annual O&M costs are estimated at \$115-325 million.

DBP control in the distribution system after the water leaves the treatment plant can also be implemented. DBPs continue to form from the treatment plant to the consumer's tap due to the residual disinfectant and organic carbon. Several in-distribution system operations are often deployed to reduce DBP levels in the distribution system. First, reduced chlorine loading at the plant with subsequent additions through 'boosters' in the distribution system can reduce the contact time for chlorine with the organic carbon in the distribution system, reducing the DBPs in the consumed water (Carrico and Singer 2009; Kang and Lansey 2010; Behzadian, Alimohammadnejad, Ardeshir and Jalilsani 2012). DBP speciation changes within the distribution system have been evaluated (Elshorbagy 2000; Behzadian, Alimohammadnejad et al. 2012) and recent laboratory experiments (Clark 1998; Boccelli, Tryby, Uber and Summers 2003) and studies in real distribution systems (Chen and Weisel 1998; Elshorbagy 2000; Rodriguez, Serodes, Levallois and Proulx 2007; Behzadian, Alimohammadnejad et al. 2012) have considered the role of additional chlorine dosing in DBP formation. If staged disinfection is not effective, DBP can be removed from the distribution system at storage points. The most common removal technique is to mix and aerate water in tanks, which causes the THM to volatilize, reducing concentrations in the water sent to consumer taps (Sherant 2008; McDonnell and Boccelli 2012). Very little research has been done to evaluate the relative removal of different species of THM following aeration. Total THM decreases under aeration conditions—however,

³ The report selects "plausible" and "outer boundary" conditions for future regulatory conditions. For example, the authors state that it is plausible that monitoring for THM regulation will change to a single sample not to exceed from the current averaging. It is an outer boundary condition to assume that individual THM and HAA species will be regulated. See report for full details of the conditions represented by the cost values cited here.

simple partitioning calculations suggest that chloroform will volatilize to a greater extent than bromoform, leading to an increase in the percent bromination while overall THM is decreasing. Again, in waters that contain bromide this may lead to a drinking water that meets regulatory compliance levels, but represents an increased risk due to its high levels of brominated DBPs.

Finally, while not typically deployed at drinking water plants, there has been significant research on bromide removal technologies for source waters. In general, removal of bromide is very challenging since it is a highly soluble, small, monovalent ionic species. Removal of this type of contaminant is usually achieved through removal of all dissolved species during desalination. Both membrane and thermal demineralization processes are suitable for bromide removal, but since bromide comprises just a small fraction of the dissolved solids in a waste stream or source water, most of the energy invested in desalination is spent removing non-target salts (i.e., NaCl). Further, fully demineralized water is unsafe for consumption, so additional expense may be incurred for chemical addition for potability if TDS must be taken very low to remove adequate amounts of bromide.

While bromide ion removal generally requires desalination techniques (membrane or thermal), this is not the only known method. Anion exchange (Hsu and Singer 2010), electrochemical removal (Kimbrough and Suffet 2002; Kimbrough and Suffet 2006; Bo 2008; Kimbrough, Boulos, Surawanvijit, Zacheis and Cohen 2013), enhanced coagulation (Ge, Shu and Dai 2007; Ge and Zhu 2008), and sorption with reactive carbons (e.g., silver doped aerogels (Sanchez-Polo, Rivera-Utrilla, Salhi and von Gunten 2006; Sanchez-Polo, Rivera-Utrilla and Von Gunten 2007)) are all methods that have been evaluated and have varying removal efficiencies. These methods selectively target bromide, usually for removal from source waters undergoing disinfection to reduce brominated DBP formation. Few of these technologies have reached field scale deployment. However, Kimbrough et al. (2013) recently published results from pilot-testing an electrolysis method for use on California State Water Project water (as discussed above, this water has naturally-occurring bromide on the order of 42-424 $\mu\text{g/L}$ (0.04-0.4mg/L) (Holm, Harader et al. 2007), and costs estimated for its control are in the hundreds of millions per year (Chen, Haunschild et al. 2008)). Kimbrough et al. (2013) estimate that the capital cost of an electrolysis plant would exceed a similar reverse osmosis plant. Power consumption would be in the range of similar reverse osmosis plants, but disposal costs would be less because no residuals are produced.

5.0 Current and Potential Future Power Plant Bromide Discharge Impacts on Drinking Water

Assessing the impact of proposed treatment methods for power plant discharges on downstream drinking water plants would require considerably more information than is currently available or was used for environmental assessment of the proposed effluent limitations guidelines and standards for the steam electric power generating point source category (USEPA 2013).

For example, similar to the analysis presented in the modeling studies, receiving water analysis would have to be used to identify current bromide levels in surface waters. There are not extensive historical data for surface waters, however, drinking water plants experiencing DBP problems do frequently analyze source water bromide, and their results could be used for this

part of the model. Proximity analysis along the flow path of the surface water would need to be used to identify downstream drinking water plants that might be affected by current or altered bromide concentrations (this was done for drinking water plants in the current analysis with respect to metals, but it is not clear that plants beyond the mixing zone for metals discharges were evaluated (USEPA 2013)). Bromide does not settle out or complex as metals do, so increased bromide concentrations have impacts hundreds of miles downstream from discharge. Bromide declines only through dilution with surface runoff or rainfall. [See for example, analysis of the bromide concentrations in the Ohio River at Cincinnati associated with increased discharges of bromide into the Allegheny and Monongahela Rivers in 2008 and 2010 (Ziolkowski 2010).] Downstream drinking water plants would have to be characterized to determine (1) the current contribution of power plant discharges to drinking water risk, (2) the future effect of increased discharges associated with FGD or mercury removal technologies on drinking water risk, and (3) the potential effects of the implementation of ELG options under consideration on drinking water risk. The downstream plants would need to be evaluated for type of disinfectant used, treatment train DOC removal efficiency, current source water bromide levels, and current DBP concentrations and speciation.

Very little work has been done regarding the effect of increased bromide loads through anthropogenic discharges on drinking water plants. Much of the prior work on the effects of bromide on drinking water systems (summarized above) is associated with naturally-occurring bromide (e.g., CALFED's analysis; (Holm, Harader et al. 2007)). In the past few years, within the Monongahela and Allegheny basins in southwestern Pennsylvania, significantly increased bromide concentrations have been observed in source waters (States, Cyprych et al. 2013; Wilson, Wang et al. 2013; Ziemkiewicz 2013). This has largely been attributed to practices associated with disposal of oil and gas produced water from Marcellus shale development (Ferrari, Michanowicz, Christen, Mulcahy, Malone and Sharma 2013), however, several power plants in the region have recently installed FGD systems, and thus may be contributing to the bromide loads.

States and colleagues at the Pittsburgh Water and Sewer Authority and the University of Pittsburgh completed a multi-year study in the Allegheny River and its upstream tributaries that evaluated source water (at the plant in Pittsburgh) and finished water (after disinfection), as well as water from locations above and below various discharges that were suspected to contain bromide (States, Cyprych et al. 2013). Source water bromide concentration was linearly correlated with finished water bromination; at 50 µg/L bromide in the source water, 62% of the THM consisted of bromoform, dibromochloromethane and bromodichloromethane, while at 150 µg/L bromide in the source water, 83% of the THM was comprised of these brominated species. Oil and gas brine treatment plants added significant bromide to the watershed, as expected. Some coal fired-power plants intermittently added bromide loads, while others seemed to have very low bromide discharges. It was not clear from the States et al. (2013) study which power plants had FGD scrubbers installed. It was clear that increasing bromide loads (through discharges from various sources) affected the finished drinking water at the treatment plant. Higher TTHM and increased bromination (up to 88%) was observed in response to increased bromide concentrations. Conventional drinking water processes were ineffective at removing bromide, as expected, with bromide only removed during oxidation to form brominated DBPs. TDS was not a reliable indicator or surrogate of bromide concentrations, and thus, TDS standards for the river

or for point source discharges are not likely to adequately control bromide discharges. They identified anthropogenic loads of bromide in the basin of 1622 lbs/day (735.7 kg/day).

VanBriesen and colleagues at Carnegie Mellon University, with collaborators at seven drinking water plants in the region, completed a three year field study in the Monongahela River that evaluated source water (from drinking water plant intakes) and finished water (after disinfection) to ascertain the effect of increasing bromide loads on DBP formation and speciation. Wilson and VanBriesen (2013) calculated the increased bromide load associated with surface water discharge practices in the oil and gas industry in 2008-2011 in the state of Pennsylvania. They report a six fold increase in bromide load (from 1150 kg/day to 8000 kg/day) between 2006 and 2008, with a subsequent decline to 1750kg/day in 2011, after Marcellus-associated produced water stopped being treated at surface discharging plants not subject to TDS effluent limits (Kraner 2011). VanBriesen and colleagues report significant increases in TTHM and percent bromination at the surface water treatment plants during this time period (VanBriesen and Wilson 2012; Wilson and VanBriesen 2013), as would be expected based on the extensive literature supporting the relationship between higher source water bromide and higher bromination of DBPs in the finished water.

While no direct analysis has been done on the effect of coal-fired power plant bromide discharges on downstream potable water supply disinfection by-product formation, there is no reason to suspect that bromide released from FGD scrubber wastewater discharged to surface waters will react in any way differently than other sources of bromide. Increased bromide loads translate into increased bromide concentrations, subject to dilution effects controlled by river flows, rainfall, and the input of other waste streams with varying bromide concentration. A complete assessment of all inputs of bromide to a drinking water source area could easily be made with adequate monitoring data. The relative contribution of coal-fired power plant discharges to the overall bromide load could then be ascertained. Regardless of the source of bromide, however, it is clear that relatively small amounts of bromide in source waters have the potential to create significant quantities of brominated disinfection by-products. Drinking water treatment plants will require modification and will incur additional costs if bromide concentrations in source waters rise to unacceptable levels. Because of the structure of DBP regulation (as lumped TTHM and HAA5) and the relative risk associated with brominated versus chlorinated DBPs, drinking water plants that meet MCLs for TTHM and HAA₅, while treating high bromide source waters, may distribute water that presents increased risk to consumers. Quantification of this increased risk will be difficult, but should be undertaken if bromide levels are permitted to rise in source waters due to increased discharges from power plants.

6.0 Summary and Conclusions

Current coal-fired power plant activities produce a variety of wastewaters, including those that contain elevated total dissolved solids (TDS or salts). These salts often contain high levels of chloride and moderate levels of bromide. Current levels of bromide in coal-fired power plant wastewater are highly variable. Bromide levels in coal vary, producing variable amounts of bromide during combustion. In a conventional coal-fired power plant, bromide is generally converted to bromine and exits in the flue gas. However, pollution control units, especially wet flue-gas desulfurization (FGD) treatment designed to reduce sulfur dioxide emissions, converts bromine back to bromide, which is then collected in the FGD wastewater and discharged to

surface waters. Thus, plants operating wet FGD systems currently, or those that will install them in the future, discharge higher amounts of bromide to surface waters. Also, a successful technology associated with mercury control is based on bromide addition, which further increases bromide concentrations in FGD wastewater. It is not clear, based on regulatory uncertainty and industry options, how many power plants in the US will install wet FGD systems and/or wet FGD with bromide addition for optimal control of sulfur dioxide and mercury emissions to air. **It is reasonable to expect that bromide loads from coal-fired power plants will increase in the coming years unless FGD wastewater is treated to remove bromide.**

Discharge of bromide to surface waters, even from wastewaters at low concentration, can increase concentrations of bromide in waters that are used as sources for drinking water treatment plants. Bromide concentrations that affect potable drinking water systems are generally very low. While more information and study is needed to understand fully the role of bromide in DBP formation and risk, source water levels above 0.05-0.1 mg/L are associated with significant bromination and often lead to concentrations of TTHM and HAA₅ that exceed regulatory compliance levels. Drinking water plants cannot easily remove bromide, and when bromide reacts with disinfectants, it can form brominated disinfection by-products. Exposure to these DBPs (through consumption of treated water and through dermal and inhalation exposure during bathing) is associated with increased cancer risk (especially bladder and rectal) and with increased negative reproductive outcomes (i.e., low birth weight, developmental anomalies). Control of DBPs through process changes is often expensive, requiring plant upgrades and increased annual operation and maintenance costs. DBP control targets regulated TTHM and HAA₅, but other DBPs formed during disinfection of bromide-containing water may present higher risks and may persist even in waters that have been modified to meet compliance requirements. Thus, while it is possible to manage bromide-associated risks within the drinking water system, the technologies involved are complex and expensive and may not significantly reduce the risk associated with source water bromide. **Managing bromide in source waters is preferred as it avoids the expensive and possibly ineffective treatment options used within drinking water systems, providing protection for the hundreds of millions of people who use disinfected water in the U.S. every day.**

Bromide was inadequately considered in the review of technologies for the proposed Effluent Limitations Guidelines and Standards for the Steam Electric Power Generating Point Source Category. Extensive receiving water analyses did not include current bromide levels in these waters. Analysis of current bromide levels in power plant discharges was insufficient to adequately characterize the breadth of current risk or the potential for increased risk with expanded pollution control for sulfur dioxide and mercury. Proximity analysis to downstream drinking water plants was considered for potential effect of metals, but not for bromide. Downstream drinking water plants were also inadequately characterized to determine the current contribution of power plant discharges to drinking water risk, the future potential effect of increased discharges, and the effects of the implementation of the proposed ELG options on drinking water risk. While Option 5 would be expected to remove bromide (as it removes chloride), other options, which do not appreciably remove chloride are unlikely to remove bromide. **Significant additional analysis is needed to understand the human health and economic impacts of steam electric power plant discharges of bromide now, in the future, and under different possible treatment options proposed in the new standards.**

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